
 BOSCH 		CR pump CP4 - Diagnosis report		Report no.	19420
				Date	12/4/2007
Department:	Person responsible:	Telephone:	Use	internal	
Non-responsive content removed			external		x
Pump type:	Customer:	Project:	Project/ design sample version		
CP4.1XX_298_2x5,25_REC_3,3_1,95_MT4,2	VW	R4 2.0 EU5	D / C2		
Item number (Part no.) :	Date of manufacture:	Serial number:	Plant - line		
0445B21058	010207	0045	0110 FeP - 1		
SAP-No.:	Samos no.:	Customer order no.:	Engine/Vehicle number		
DS-164763	578256		AU 481-8-8008		
Customer part number	ER type [customer]:	Endurance run conditions:	DSBFD no.:		
	Q endurance run		19420		
Mileage:	Received by DS-PC/EDI on:	Process no.	Confidentiality note		
80000 km	10/22/2007	2007 - CP4 / 0006	Confidential		
Complaint:	None. Endurance run end.				

1. Subject

CP4 customer return
Q-ER; CAG 0000 067; AU 481-8-8008

2. Conclusion

The results of the residual soiling test lie within the tolerance of new parts. Only light traces of wear can be seen.

The pump has passed the test.

3. Results of diagnosis (visual findings)

Legend rating stages

OK	x		
non-critical		x	
Critical			x

3.1 Drive

No wear visible

x		
---	--	--

3.2 Drivetrain

Only very slight wear visible (Fig. 1 and 2)

x		
---	--	--

3.3 High pressure

Only very slight wear visible

x		
---	--	--

3.4 Bearing

No striking feature (Fig. 3)

x		
---	--	--

3.5 Shaft seal

Minor embedding of the shaft seal

x		
---	--	--

3.6 Bore holes

Only very minor cavitation erosion in the tappet bore (Fig. 4)

x		
---	--	--

3.7 Attached components (MU, OV, GP)



No striking feature


x		
---	--	--

3.8 Other

No striking feature

x		
---	--	--

 BOSCH 	CR pump CP4 - Diagnosis report			Report no.	19420	
				Date	12/4/2007	
Department:	Person responsible:	Telephone:	Use	internal		
Non-responsive content removed				external		x
4. Hydraulic function						
				Delivery rate [l/h] New part	Delivery rate [l/h] after testing	
	n [rpm]	p_rail [bar]	Metering unit [A]	2/6/2007	11/5/2007	
ST	200	200	0.4	4.0	3.9	<input checked="" type="checkbox"/>
Running limit	1000	1800	0.4	17.5	17.7	<input checked="" type="checkbox"/>
KL1-S	3375	500	0.4	67.6	66.7	<input checked="" type="checkbox"/>
OK						

		CR pump CP4 - Diagnosis report		Report no.	19420
				Date	12/4/2007
Department:	Person responsible:	Phone	Use	internal	<input type="checkbox"/>
Non-responsive content removed			external	<input checked="" type="checkbox"/>	<input type="checkbox"/>
5. Parts storage The parts will be stored at RB until 06/2008 6. Attachments Figure					
Tested:	Non-responsive content removed	Telephone:	Non-responsive content removed	Date:	14.12.07
Department:		Telephone:		Date:	19.12.07
Department:		Telephone:		Date:	07.01.08
				Signature:	Non-responsive content removed



 BOSCH 	CR pump CP4 - Diagnosis report		Report no.	19420
			date	12/4/2007
Department:	Person responsible:	Telephone:	Use	internal
Non-responsive content removed			external	<input checked="" type="checkbox"/>



Fig. 1 010207-0045_cam track_running surface

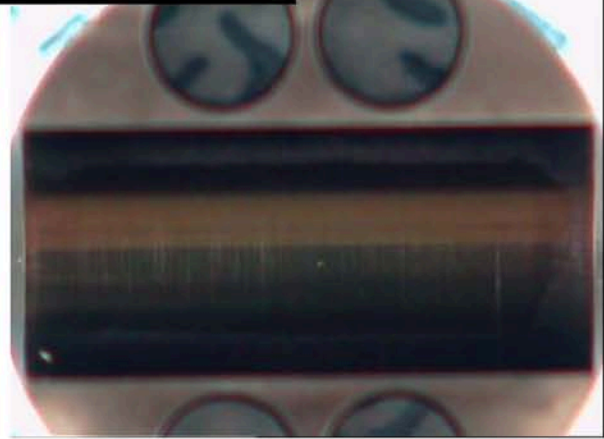


Fig. 2 010207-0045_roller support running surface

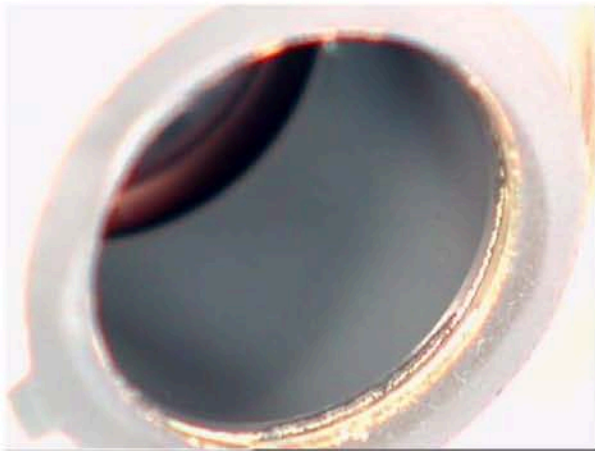


Fig. 3 010207-0045_flange bearing bushing



Fig. 4 010207-0045_housing tappet bore

From: Non-responsive content removed
To:

CC:

Date: 9/19/2008 12:50:04 PM

Subject: Teleconference 9/18/2008, Production measures to reduce drivetrain damage

Hello,

Attached are the minutes for today's teleconference on the above topic:

Participants:

Audj: Non-responsive content removed

RB: Non-responsive content removed

1) Metal splashes (roller support)

1.1) Avoidance of metal splashes

- Testing of new system is completed
- 2-day production to be decided (scheduling in progress), fix date, info to Audi in Wk 39 -> Non-responsive content removed
- Proposal: Carry out large-scale test (3 months of production) for VW/Audi, then series release if evaluation is positive

- Discussion of proposal in change meeting on 9/25 -> Non-responsive content removed

1.2) Identification of metal splashes

- 2 quotations (external, internal) submitted
- Large-scale test under series conditions required for evaluation purposes to be sure of avoiding "pseudo scrap" e.g. due to washing residues.
- 2 x visual inspections used at present (after finishing process and after friction coefficient test)
- Objective: 1st step: Implementation of optimized measurement method + assessment by employees, 2nd step: Implementation of assessment using calculation algorithm (longer term)
- From present perspective, implementation of step 1 by Wk 44 achievable for 1st line (FeP)

3) Avoidance of C layer removal

- Completion of transport frame modification scheduled by Wk 42

3.1) Avoidance of C layer removal during pressing-in process of roller support in tappet body (new)

- Flaking C layer particles from roller support during pressing-in process (supporting surface of roller support) are transferred during frictional coefficient test and can lead to preliminary damage in contact with roller/roller support

- Possible improvements (optimization of C layer adhesion, avoidance of C coating in area mentioned) under discussion

- Submission of schedule for further procedure Wk 39 -> Non-responsive content removed

4) Avoidance of fusing on roller

- Currently 2 possible solutions are being considered

- 1. Improvement of roller contact through resilient contact plate

- 2. Direct stacking of the rollers ("stack of wood") -> contact through components themselves

- Variant 2 currently prioritized. If this works, implementation by Wk 48 appears to be feasible

- Currently there are 2 x straightedge tests in use Estimation of effectiveness positive, since 2nd test has not yet found any faulty parts.

Failure statistics update (flow chart, etc.) requested by 9/19/2008, and in future each Friday so that presentation the following Monday is possible) -> Non-responsive content removed

Best regards / Mit freundlichen Grüßen

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Robert Bosch GmbH

Non-responsive content removed

Domicile/Sitz: Stuttgart

Court of Registry/Registergericht: Local District Court Stuttgart Commercial

Register No. 14000 Chairman of the Supervisory Board: Hermann Scholl;

Management: Franz Fehrenbach, Siegfried Dais;

Bernd Bohr, Rudolf Colm, Gerhard Kümmel, Wolfgang Malchow, Peter Marks; Volk-mar Denner, Uwe Raschke, Peter Tyroller

C3: Avoidance of metal splashes

Status

- Graphite coverings for metal holders in the main power range
 - ⇒ 0.2% (1 of 480) metal splashes discovered directly on the adhesive layer, series: 0.2 - 0.4%

Derived hypothesis: Shielding plate between source and component is the cause of the metal splashes while the C3 source is being conditioned

- Influence of shielding plate while conditioning the source reduced, metallic holders used:
 - ⇒ One affected striking feature is currently under examination; result available on 4/10

1

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C3: Avoidance of Metal Splashes

Further work

- Combine the use of graphite coverings + reduce the influence of the shielding plate while conditioning the source
 - Try out process 4/4/2008
 - Coat roller support for testing (480 RS) 4/7/2008
 - Inspection after finishing 4/9/2008
 - Presentation of results 4/11/2008
- Alternative approach for avoiding metal splashes in preparation:
 - Optimized connection of the electrical potential to the components during process 5/9/2008

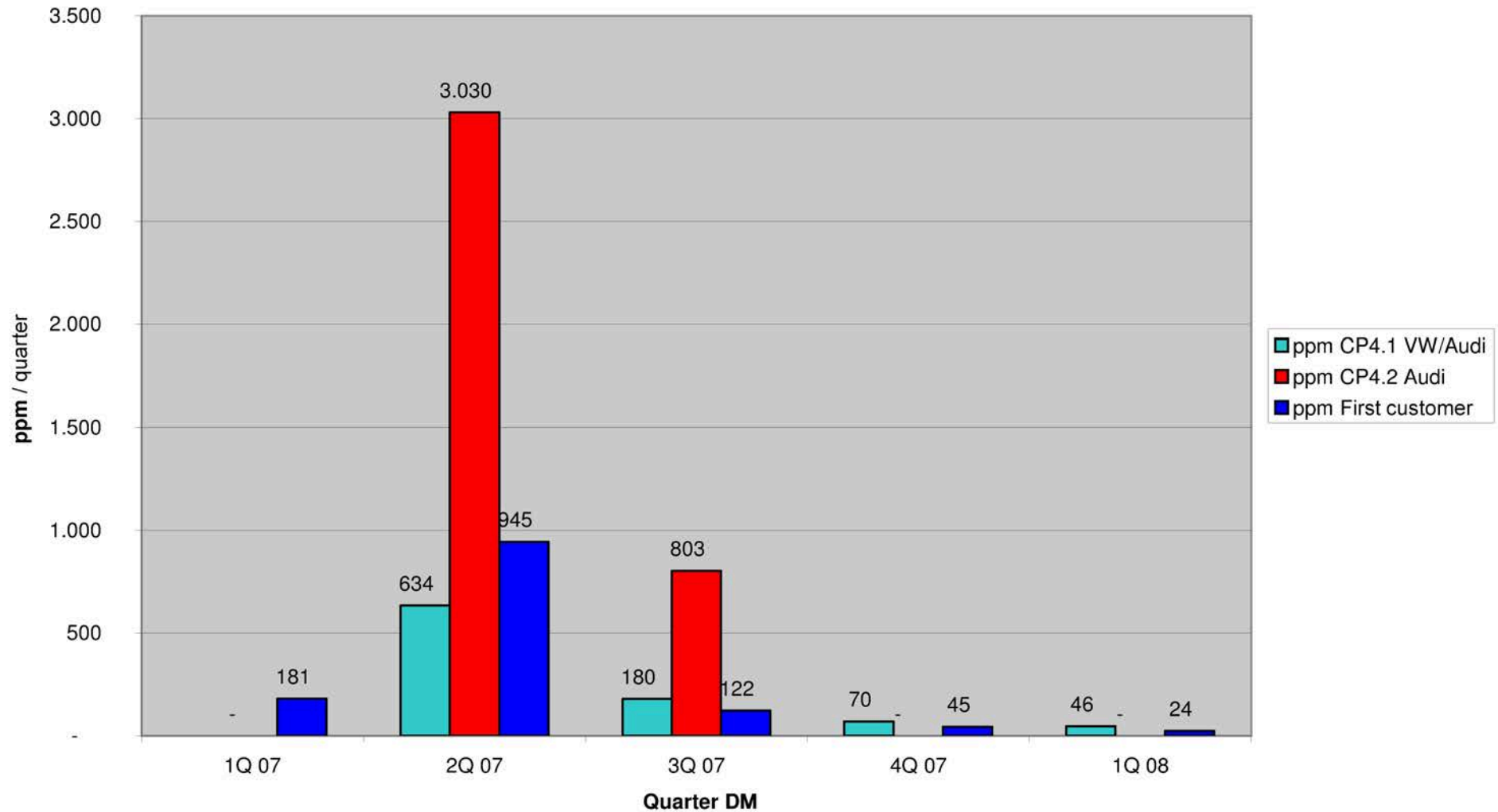
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Failure statistics 0 km / Field All customers

Drivetrain damage CP4 0 km and field



Traceability and controlling of not OK pumps

- Exclusion of pumps with turned tappets / drivetrain damage
 - Traceability and control of CP4 pumps carried out by central computer.
 - Transponder on the pump is read in each station
 - With not OK processes, the pump is excluded - information to employee via station monitor
 - Pumps with not OK status will be rejected in the following stations



CP4, Tappet anti-turning lock, Status 3/2008



Contents

- Motivation
- Design
- Testing
- Schedule
- Summary of results



CP4, Tappet anti-turning lock, Status 3/2008



Motivation

Following occurrence of the initial CP4 drivetrain damage during internal testing or the first start-up of the engine at the customer's, various failure hypotheses were developed.

One hypothesis was that turned tappets are the cause for subsequent drivetrain damage. To counter this, development on the tappet anti-turning lock was started.

The hypothesis established at that time can no longer be upheld with today's information. The cause for the occurring drivetrain damage is either a stiff and/or stuck roller. The subsequent turning of the tappet is therefore a consequence of the stiff / stuck roller. If turning were to be prevented by an anti-turning lock, this would simply delay the failure and not prevent it. Through the introduction of suitable measures in the assembly process (laser scanning of the tappet position), turned installation of the tappet was effectively excluded.

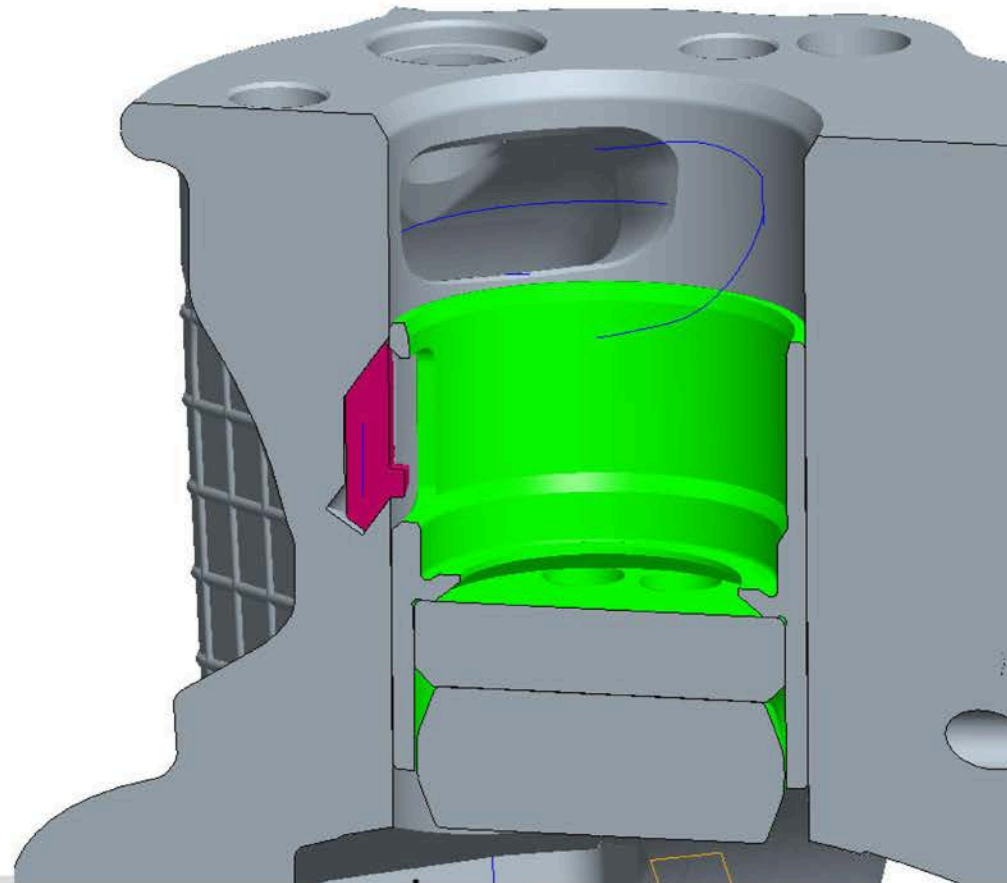
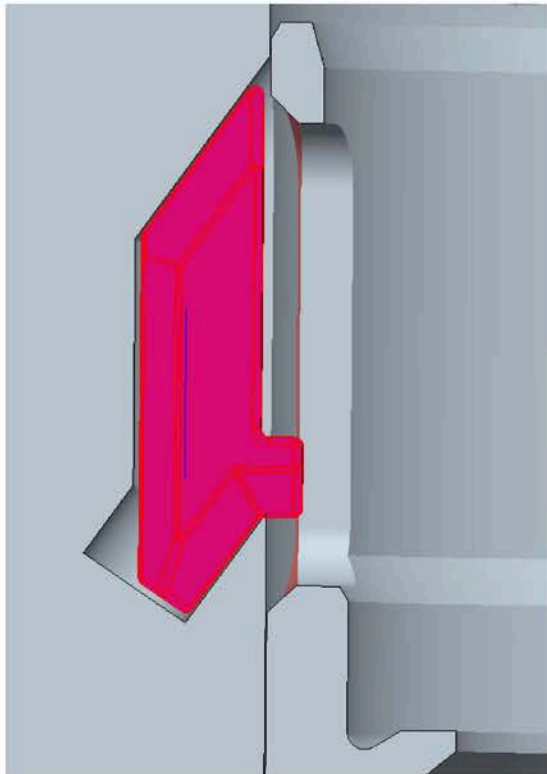


CP4, Tappet anti-turning lock, Status 3/2008



Design

- Preferred solution: Variant with fitted key as insert



Diesel Systems

3

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CP4, Tappet anti-turning lock, Status 3/2008



Testing:

- First 2 pumps after approx. 500h ER indicate a good result.
- Parts from near-series production process show tappet breakages (deformation, internal stresses in tappet body)



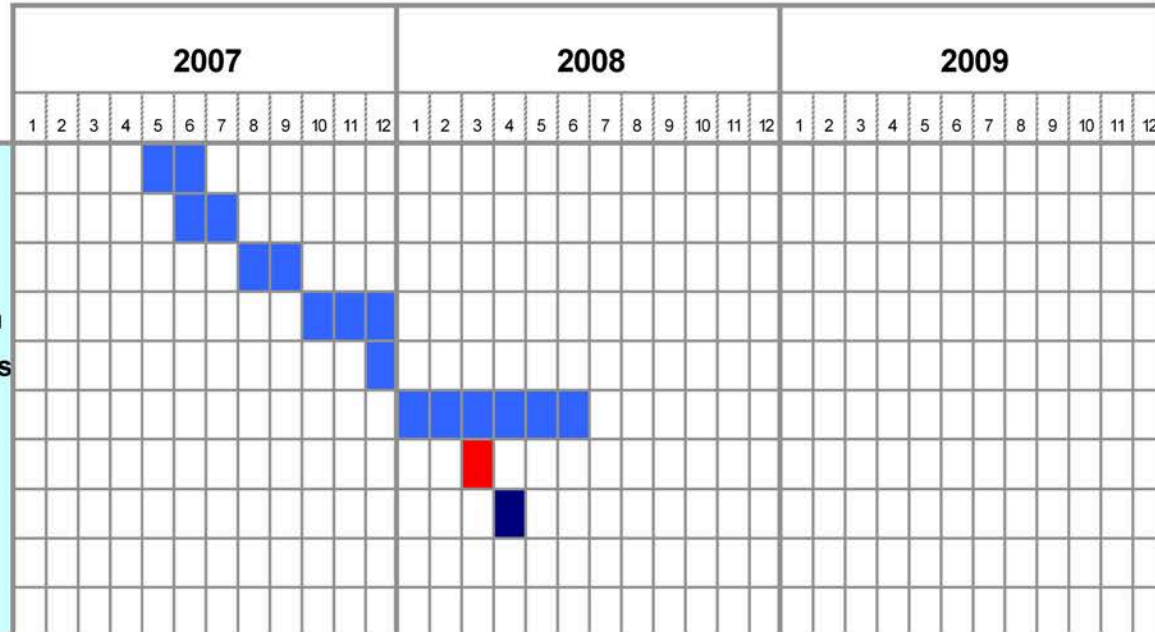
CP4, Tappet anti-turning lock, Status 3/2008



Schedule

CP4 Tappet anti-turning lock

Concept phase
Design/sampling
ER 2 x 500h (first verification)
Revision/series production preparation
Sample availability of pre-production parts
ER 2 x 2,000h (validation)
Development stop
Pump findings after approx. 250h



CP4, Tappet anti-turning lock, Status 3/2008



Summary of results

- Initial ER results are positive with respect to potential durability of the anti-turning lock described
- Near-series parts produced show weaknesses with regard to durability
- Today's findings on drivetrain damage show that turned tappet is a consequence and not the cause of the drivetrain damage. Stiff rollers are the cause of drivetrain damage. Anti-turning lock is not a corrective measure or does not increase robustness of this.
- Head of development decides to stop development on 3/2008
- Remaining ER pumps are stopped and final findings recorded



Detecting turned tappets, drivetrain damage

- Detecting turned tappets in the assembly
 - 100% laser scan of the alignment of the roller support after installation of the tappet body/roller support/roller assembly immediately before joining and bolting on the cylinder head
 - 100% click-clack test after helium leak test before functional inspection - since introduction of the laser query (11/15/2007 L1; 12/21/2007 L2) no further pumps have shown any striking features in the click-clack test

- Detecting drivetrain damage / turned tappets in the functional inspection
 - 100% test
 - Detecting by monitoring the temperature difference between the supply and return temperature

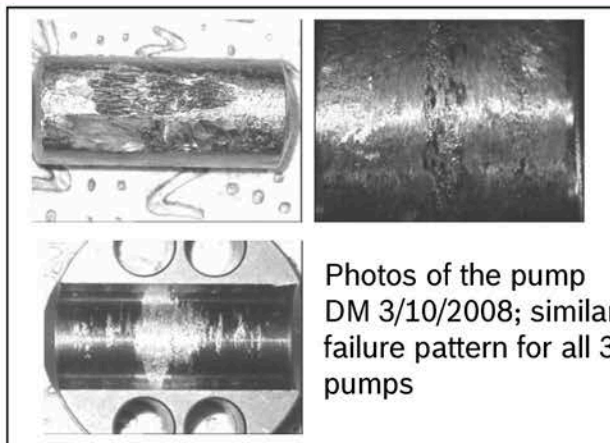


CRP CP4.1 and 4.2 - AUDI 0km complaint FeP

Drivetrain damage

Scope of defect

- 0 km: 3x pump 0445010507/ 03L130755
- Pump DM
 - 1x 3/5/2008
 - 1x 3/10/2008
 - 1x 3/11/2008
- Failure DM: 3/14 3/17 3/18/2008
- GR Bosch: 3/25/2008



Photos of the pump DM 3/10/2008; similar failure pattern for all 3 pumps

Description of problem

- Failure on Audi final function test bench (cold test) with noise and rail pressure variances

Cause analysis

- Heavy wear of the cam and roller
- Possible assessment of the damage: Increased friction between roller and roller support leads to slippage between roller and cam. This leads to damage of the cam, roller and roller support and to turning of the tappet.

1

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CRP CP4.1 and 4.2 - AUDI 0km complaint FeP

Measures

- PHA carried out in [REDACTED] on 7/12/2007
Result: Commissioning conditions do not comply with specification. Commissioning of the pump was changed
- Optimization of RB test bench sequence
D: 7/9/2007 completed
- CH assembly with 5° torsion allowance
D: 7/23/2007 completed
- Dry pressing in of roller support
D: 7/23/2007 completed
- Introduction of dwell time during assembly of roller support
D: 8/28/2007 completed
- Extension of high-load testing point
D: 10/12/2007 completed

2

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CRP CP4.1 and 4.2 - AUDI 0 km Complaint Feuerbach Plant

Measures

- Improved visual inspection of roller support according to provisional new visual inspection catalog
D: 12/13/2007 completed
 - Friction coefficient test +/- 10° to improve checking of main load range of roller support
D: 12/13/2008 completed
 - Introduction of laser scanning of tappet for the safe positioning of the tappet during assembly
D: 12/21/2008 completed
 - Introduction of final visual inspection catalog
D: 1/2/2008 completed
- Introduction of new inspection program for CP4.1 VW with more stringent test conditions
D: 1/11/2008 completed
- Introduction of visual inspection of roller support using technoscope instead of illuminated magnifier to improve detection of metal splashes
D: 2/4/2008 completed



CRP CP4.1 and 4.2 - AUDI 0 km Complaint Feuerbach Plant

Measures

- Introduction of new inspection program for CP4.2 Audi with more stringent test conditions
D: 2/5/2008 completed
- 100% straightedge test on roller to identify elevations on the roller. Since introduction of the test parts have been found. Parts will be used for large-scale test.
D: In parts manufacturing since 4/1/2008, in pump as of 4/7/2008
- Tests with 480 parts each to avoid metal splashes in C coating process of roller support
 1. With new electrode cover and optimized conditioning D: 4/11/2008
 2. Optimized electrical potentials for the components during the process D: 5/9/2008
if large-scale test successful with full batch



Causes and measures

→ Elevations on the roller

- Impact of elevations on the roller
 - Assessment through large trial
 - Documentation of the failure potential of the elevations on roller fault pattern in the short-term area (functional test) and as medium/long-term failure (0-km/field).
 - Set-up of 50 pumps (if possible) with documented elevations (WLI measurement + EDX analysis).
 - Documentation of tappet assemblies before and after friction coefficient check
 - Installation of tappet assemblies in pumps. Documentation of tappet assemblies after functional test – Evaluation of failures
 - Definition of selected pumps for a short ER



Causes and measures

- Elevations on the roller
 - Identification of elevations on the roller
 - Current identification of elevations: The identification of rollers with elevations is very difficult. The visual inspection is very error-prone.
 - Currently no failures in the visual inspection
 - Measures to improve identification of elevations
 - Set up a simple device in which the roller is rolled manually against a sharp edge (blade).



Causes and measures

→ Elevations on the roller

- Schedule to improve identification of elevations
- Set up simple testing device D: 04/04
- Test the device on the current series D: 04/04
- Selection of striking rollers from the current series D: 05/02
(Prerequisite: The device works and a sufficient number of parts is found)
- Documentation + measurement + EDX analysis of striking parts (parallel to 3) D: 05/09
- Assemble tappet assemblies, Friction coefficient check and before/after documentation D: 05/09
- Installation of tappet assemblies in pumps. Execution of functional test D: 05/15

Causes and measures

→ Elevations on the roller

- Schedule to improve identification of elevations
 - Assessment of results + decision D: 5/16
 - End of short ER test (100h) D: 5/26
 - Complete major trial D: 5/27

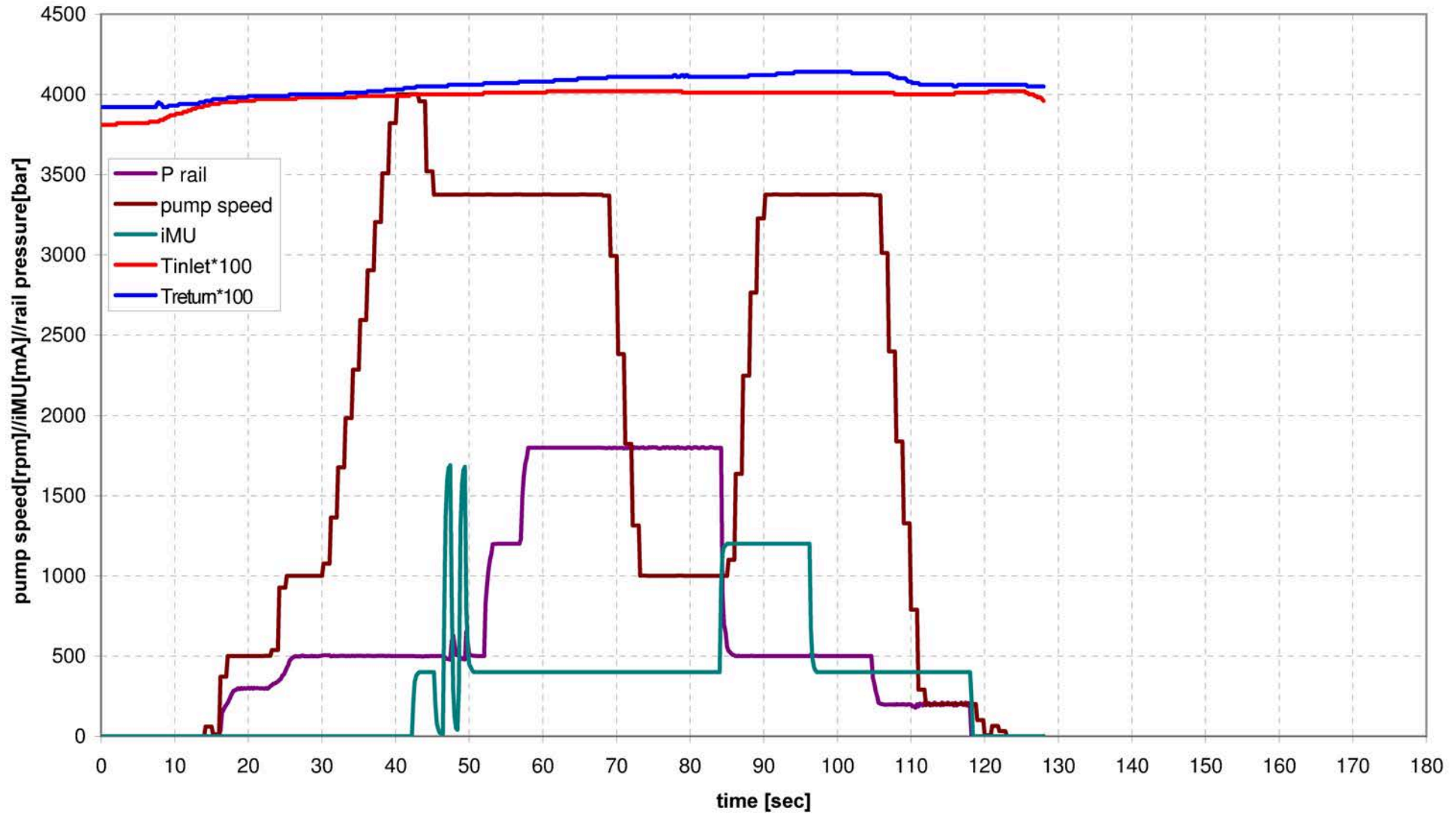
Remark

The above schedule always indicates the end of an activity for all 50 pumps. Many of the activities will run in parallel, which means interim results will be possible. A prerequisite for a successful trial is the functioning detection of elevations and the identification of a sufficient number of elevated rollers



CP4.1 - VW 0445010507 - Time sequence of the values (Current test sequence)

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Identification of turned tappet, drivetrain damage

- Click-clack testing
 - Click-clack testing is a manual test to identify turned tappet assemblies at the assembled pump.
 - Identification takes place by manually rotating the camshaft. In pumps with a turned tapped an increased variable resistance is noticeable
 - Current scope of test
 - 100% after completion – since 5/2007
 - No faulty pump identified up to now
 - 100% before/after assembly, function test - since 7/2007
 - No faulty pump identified since 12/1/2007 Note: Introduction of laser scanning (11/15/2007 L1; 12/21/2007 L2)
 - Planned scope of test:
 - Elimination of click-clack testing



From: Non-responsive content removed

To:

CC:

Date: 7/19/2007 6:27:25 PM

Subject: Re: Minutes from OEM meeting on CP4.x turned tappet from 7/13/2007 - Item 4
Inspection oil quality CP4

Dear Non-responsive content removed

Regarding your question relating to the HFRR value, please consider the following:

- Inspection oil contains anti scuff additives. The effect is specified and must be proven by the supplier in a FBBD (Four Ball Bearing) test.
 - HFRR is a standardized test used to determine wear (ball on plate). In other words, it is a measure of the amount of wear. The test runs in the mixed friction area.
 - It is possible to measure wear and friction in the HFRR test. However, a correlation of these parameters cannot be proven. This is partly due to the wide dispersion of the HFRR results in the test per se and also to the fact that different wear mechanisms (tribochemical wear/abrasive wear/adhesive wear) are involved here.
 - This means that the HFRR value is not a suitable parameter with which to assess friction behavior.
 - The HFRR value is relatively high for the inspection oil used in order to ensure a certain running in (abrasion/ smoothing of the surface tips of the parts).
- Friction is affected by the following parameters:
- For the hydrodynamic element of friction: f (viscosity of the inspection oil) --> viscosity is specified and is tested (per delivery batch)
 - Impurities in the inspection oil:
 1. Caused by particles: --> inspection oil is filtered or tested with regard to contamination in the circuit (on a weekly basis).
 2. Chemicals in the inspection oil: --> The chemical composition is tested using the FTIR (Fourier Transform Infrared Spectrometry) spectrum (per delivery batch)
 - In our opinion therefore, the key parameters that influence the friction properties of the inspection oil are monitored.

Best regards / Mit freundlichen Grüßen / Cordiali saluti

Non-responsive content removed

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Commercial Register No. 14000

Chairman of the Supervisory Board: Hermann Scholl; Management: Franz Fehrenbach, Siegfried
Dais; Bernd Bohr, Wolfgang Chur, Rudolf Colm, Gerhard Kümmel, Wolfgang Malchow, Peter Marks;
Volkmarr Denner, Peter Tyroller

From: Non-responsive content removed
Sent: Thursday, July 19, 2007 12:54 PM
To: Non-responsive content removed
Subject: Re: Minutes from OEM meeting on CP4.x turned tappet from 7/13/2007 - Item 4 Inspection oil quality CP4

As discussed, please reply.

Best regards / Mit freundlichen Grüßen

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From: Non-responsive content removed
Sent: Thursday, July 19, 2007 8:08 AM
To: Non-responsive content removed
Cc: ed
Subject: ANS: Minutes from OEM meeting on CP4.x turned tappet from 7/13/2007 - Item 4 Inspection oil quality CP4

Hello Non-responsive content removed

Why is the lubrication not being monitored? I thought that was the whole idea?

-----Original message-----

From: Non-responsive content removed
Sent: Wednesday, July 18, 2007 6:26 PM

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Subject: Minutes from OEM meeting on CP4.x turned tappet from 7/13/2007 - Item 4 Inspection oil quality CP4

Hello,

In the meeting on 7/13/2007, a presentation on the monitoring of the inspection oil quality at RB was requested.

1) Inspection oil used: Shell V-Oil 1404 (trade name)

2) The following parameters are monitored: appearance, viscosity, color, density. These are verified by the supplier by means of a certificate.

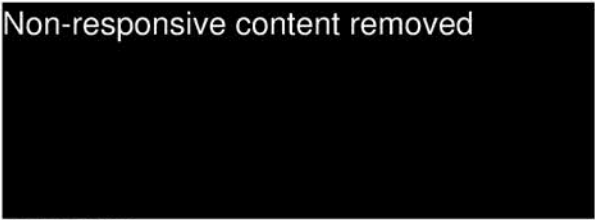
In the goods receiving inspection at RB, these parameters and the water content and the FTIR spectrum are determined.

Attached are the results of the goods receiving inspection in 2007

<<V1404_AnfrageCP4_VW.pdf>>

Best regards / Mit freundlichen Grüßen

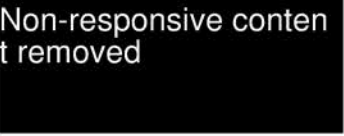
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Bernd Bohr, Wolfgang Chur, Rudolf Colm, Gerhard Kümmel, Wolfgang Malchow, Peter Marks;
Volkmar Denner, Peter Tyroller

KT analysis of lateral roller start-up

Hypotheses

- 1) Dimensional deviation of parallelism of cam to axle A-B (bearings) Oblique position camshaft due to concentricity error between the flange bearing and the housing bearing; axial play
- 2) Fuel change intervals unfavorable in the failed pumps
- 3) DT before ER -> pump not filled, therefore fuel deposits with unfavorable
a) μ (roller/roller support) have caused considerable turning of the tappet assembly in the housing
b) μ (tappet/housing) has a negative effect on back-turning



KT analysis of lateral roller start-up

Hypotheses

- 4a) Micro movement between roller support & TB -> alternating perpendicularity error
- 4b) Roller runs turned over TDC -> Load due to high pressure in TDC -> Remaining perpendicularity error
- 5) Missing 5° turning with CH assembly (combined with H4 this is problematic for the drivetrain)
- 6) Press-in strength of RS too low -> RS loose -> RS turns -> No running in of the C layer



KT analysis of lateral roller start-up

Hypotheses

- 7) Mutual influencing of tappet twin pistons; Axial movement of the camshaft restricted
- 8) Elastic resilience camshaft/housing has a alternating effect on the sucking tappet
- 9) Axial movement influenced by hydraulic axial forces (influence GP)



KT analysis of lateral roller start-up

		Hypotheses										
		1	2	3a	3b	4a	4b	5	6	7	8	9
Facts	1	A1	A4	t	t	A4, A5				✓	✓	
		A2	✓			✓				✓	✓	
	2	✓	✓			✓				✓	✓	
	3	A3	✓			✓				✓	✓	
	4											
	5	✓	A4			A6				✓	✓	
	6	✓	✓							✓	✓	
	7	A4	✓			A6				A7	A7	
	8											
	9											
10												

A1: Frequent dimensional deviations in the cam form (bathtub); parallelism measured

A2: Only plausible with Sittlinger slide

A3: Axial bearing wear tends to be worse

A4: During operation, single piston behaves different to the twin pistons in terms of angle deviation (series production)

A5: Greater press-in forces for single piston

A6: Press-in forces are not process-secure for a tight fit of the RS (perpendicularity error)
-> Plausibility test with measured diameters

A7: Geometrical tolerances have an amplifying effect





From | Processor | Tel | Fax

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4/11/2008
No. 884107

Log

Recipients

For Info
Host

Participants
Management

Log
Organiz.

Date/location **04/09/2008, 2:30 – 5:30 PM, NeckarsulmSU, B12, middle Conf. Room**

Topic **CP4 technical discussion**

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1. Complete overview RB ER test

Bosch presented the latest results from their component endurance runs and the system test. When testing the component using US fuel BDF 570, it is intended at Bosch to allow 2 endurance run pumps to continue up to 2,700 hours. With 2 further pumps, the endurance runs will be repeated on account of the lateral roller start-up.

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2. Current status of the gear pump

Bosch has established that only left-rotating pumps with an Eloxal layer on the cover show signs of wear. The cover wear has no influence on the function and the durability.

As a possible measure, Bosch would like to increase the robustness of the gear pump, in the form of a nickel coating on the cover and a reduction in the pressure between the coupling piece and the cover. Bosch is planning further tests to this end. The results will be presented at the next technical meeting.

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3. Current status regarding lateral roller start-up

In the component testing at Bosch, 3 pump endurance runs did not pass on account of the lateral roller start-up (rating ≥ 7). In the vehicle test, so far no pump has failed on account of lateral roller start-up. The cause for the failure is an impermissibly high friction between the roller end and the tappet interior surface. This brings about an overload or failure of the C layer on the roller end.



From | Processor | Tel | Fax

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4/11/2008
No. 884107

Log

CP4 technical discussion

Bosch has been documenting the press-out forces for 3 weeks now. The tests and the evaluations for the press-in and press-out forces are not yet concluded. The aim is to achieve a clean contact pattern in the roller support and tappet assembly or to optimize the press assembly (increase the press-in forces!).

Audi would like to know in this regard whether the press-in speed has changed in the last 4 - 5 months?

Furthermore, Audi would like to have a graphic evaluation for the press-in forces on the roller support, for the perpendicularity and for the friction coefficient for the series production and an evaluation in view of the "drill test".

Bosch presented the current status with the KT analysis. 9 hypotheses have been issued within the scope of the KT analysis. The main hypotheses are in the area of the press assembly. Bosch will evaluate / prioritize the hypotheses and present the results at the next technical meeting.

Bosch and Audi have agreed that other W19EU5 pumps from long running vehicles will be assessed in order to obtain further informations regarding the lateral roller start-up. In addition, Audi will verify the choice of fuel in future assessment documentation.

4. Current status of the low-pressure verification

Compared with measurements which were already carried out in August 2007 in the B8 2.7l (EU5 project), considerably greater pressures were measured, which Bosch was unable to explain at first. In the 3rd quarter of 2007, Audi introduced an acoustic measure in the B8 rail, which changed the correlation of PCV, FRL and pump returns. This measure involved inserting a T-piece that combined the return from the PCV and the fuel return line on the hollow screw remote from the return from the CP4. The testing (as well as the LP verification in the B8 2.7l) took place using a T-piece made of metal with an internal diameter of 6 mm. Since WK 34/07 a T-piece made of plastic with an internal diameter of 4 mm has been used in series production.

The circumstances will be discussed again and the further procedure stated at the next technical meeting.

Audi and Bosch have agreed that the topic of start/stop will be presented in a separate meeting by the Bosch System Development department.

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CP4 technical discussion Audi 4/9/2008

Hypothesis for GP clutch run-in

Aggravated axial play compensation between shaft dihedron - clutch - gear in conjunction with the warping on the “left” gear supporting surface leads to an axial force on the GP clutch in the direction of the GP cover.

Notes:

- Warping only on the left gear supporting surface (-> therefore no influence in the case of right-runners)
- Warping not found on current new parts, but in the case of used right-runners on the left supporting surface (i.e. must exist in new parts)
- During the ER the warping wears away

Basic tests to confirm the damage theory

Gears will be measured for warping prior to the test

Shaft dihedron measured

- Short PER(7h) with left-runner & without warping

D. 04/09/2008

compl. / no warping

compl. / OK

-> **Wear**



CP4 technical discussion Audi 4/9/2008

Estimation

- GP clutch run-in with R.B. testing occurred 100%
 - only on left-rotating pumps
 - only pumps with an Eloxal coating on the cover (not nickel)
- No functional impairment
- No indication of an effect on the durability
- No customer testing, (1 failed pump from W26 showed GP clutch run-in)

Development objective

- Eloxal coating must be present after target running time.

Possibilities to increase robustness

- Cover with nickel coating
- Reduce pressure between the coupling piece and & cover (analog to GP40)

Activities

- Short ER with nickel coated cover (basic test) 4/11/2008
- Short ER with GP 38 cover with 1 mm reduced through bore 4/12/2008
- List differences between the right / left & Assess influences 4/18/2008



Major test - Seizure provocation by metal splashes

Test description:

- > 50 roller supports with metal splashes in various magnitudes were chosen from the total quantity. In doing so it was ensured that the largest splashes and, above all, those in the area of the main load direction, were sought out.
- > The selected metal splashes were subjected to a WLI measurement, documented with photographs and then assembled into assemblies
- > The tappet assemblies were subjected to a friction coefficient testing prior to installation of the pump, the achieved values were documented
- > After the friction coefficient testing, the rollers were documented with photographs.
- > After a successful functional inspection with the standard program, the tappet assemblies were dismantled and the rollers documented again.

1

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**BOSCH**

Major test - Seizure provocation by metal splashes

- > The tappet assemblies were not dismantled yet

-> **Result:**

Out of the 50 tested pumps, one pump (no. 46) had drivetrain damage. It showed complete roller wear with a final 90° rotation. The point of failure was whilst slowing down from 3375 to 1000 rpm at 1800 bar, as is always the case in series production.

The error-causing metal splashes were approx. 7-8µm high and were located in the main load direction

Summary:

Metal splashes are clearly **a** proven cause for the drivetrain damage in the CP4

2

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**BOSCH**

Documentation metal splashes short ER

4 tappet assemblies were chosen from the metal splashes major test on 50 parts. These 4 assemblies were to be subjected to a 2x 50h ER.

After 50 h, the ER was interrupted, the roller documented and then the tappet body turned by 180 degrees. Then a further 50 h ER was driven.

Test parts were:	no. 4 = RS 1259
	no. 19 = RS 9633
	no. 35 = RS 4664
	no. 37 = RS 0275
+ extra part	no. 32 = RS 3898



Documentation metal splashes short ER

Summary of short ER metal splashes

Test part	After 50 h *	After 100 h *	Remarks:
No. 4, RS 1259	OK	OK	
No. 19, RS 9633	OK	OK	
No. 35, RS 4664	OK	OK	
No. 37, RS 0275	OK with considerable striking features	Pump not operated any further as parts required for further analysis	Dependency of metal splashes open
Extra part, no. 32, RS 3898	OK	C layer delamination in the area of the metal splashes	Failure at greater running time possible

* Relating to drivetrain damage



Documentation metal splashes short ER

Result of major test metal splashes:

1. Short-term failures (internal/ Okm)

Metal splashes could cause drivetrain damage in the short-term range. However, due to the major test, this could be explained only in the magnitude of 10 ppm. **I.e. there must be further causes for the failure.**

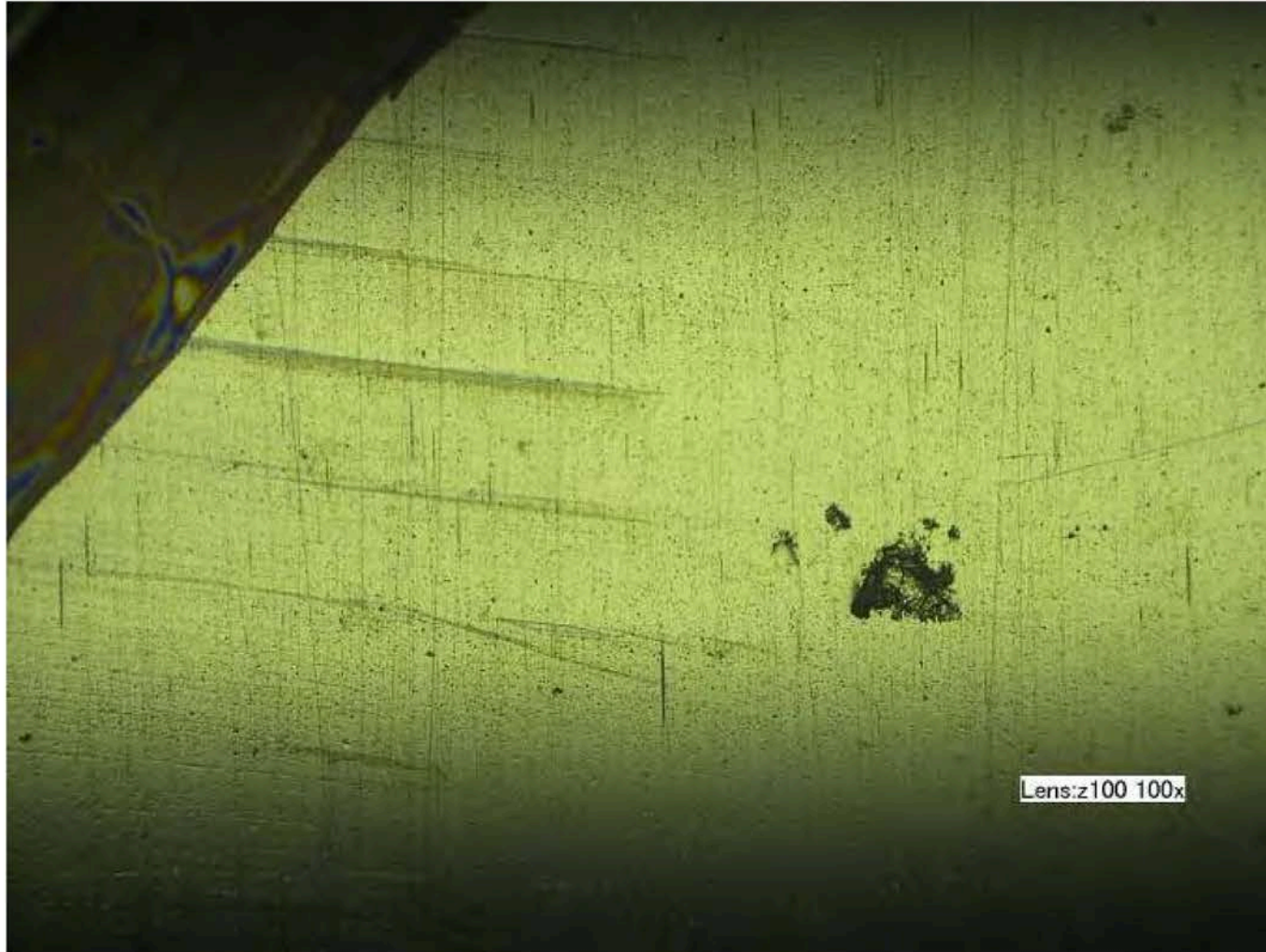
2. Long-term failure (field)

3 of the 5 pumps tested in the ER had no striking features. One pump showed striking features which have not yet been analyzed in full. A connection with the metal splashes is possible, however has not yet been proven. After 50 h an additional pump showed no striking features. After 100 h and dismantling, the C layer of the roller showed a considerable delamination in the RS.



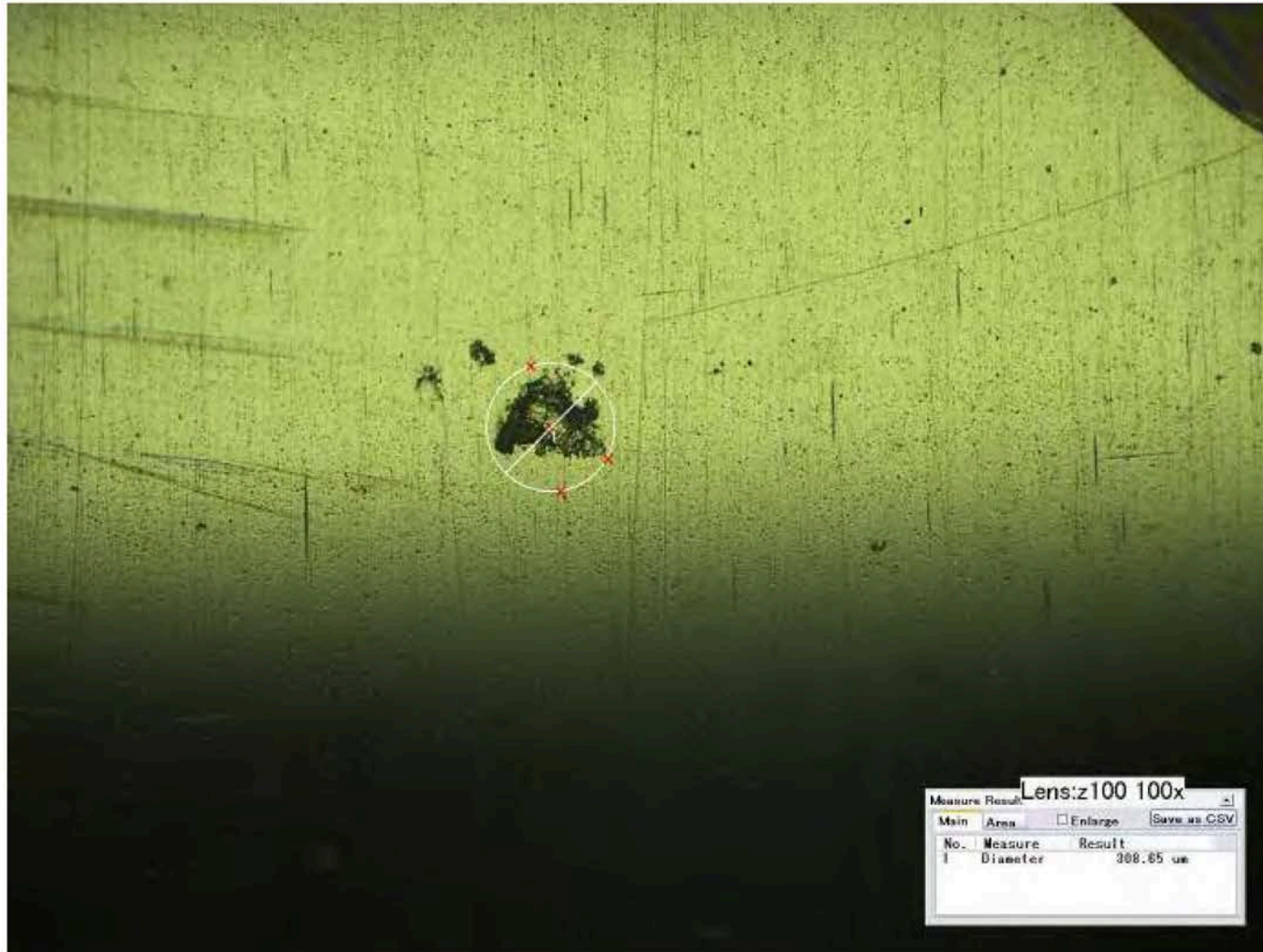
Roller_test

Roller no. 14



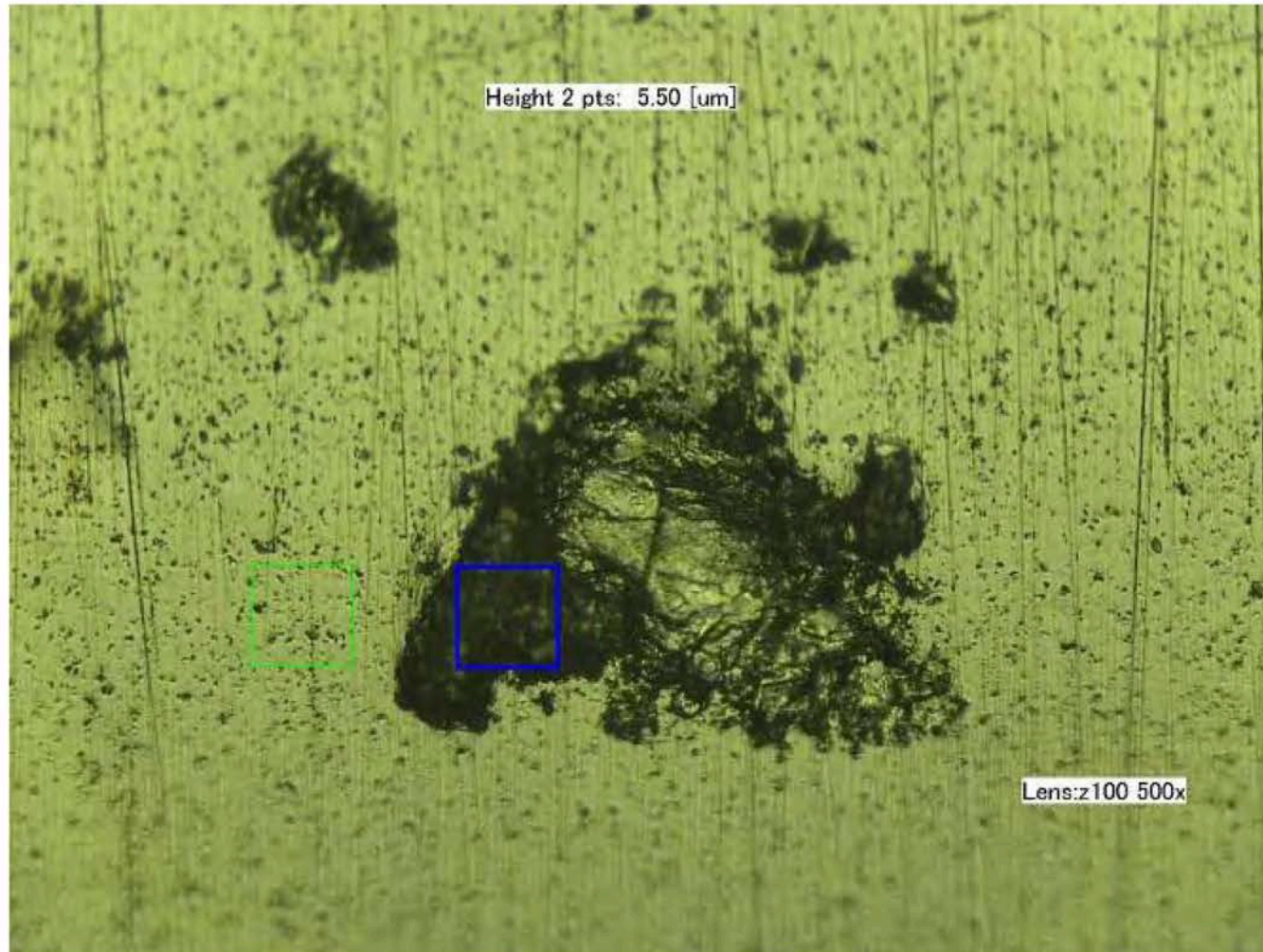
Roller_test

Roller no. 14



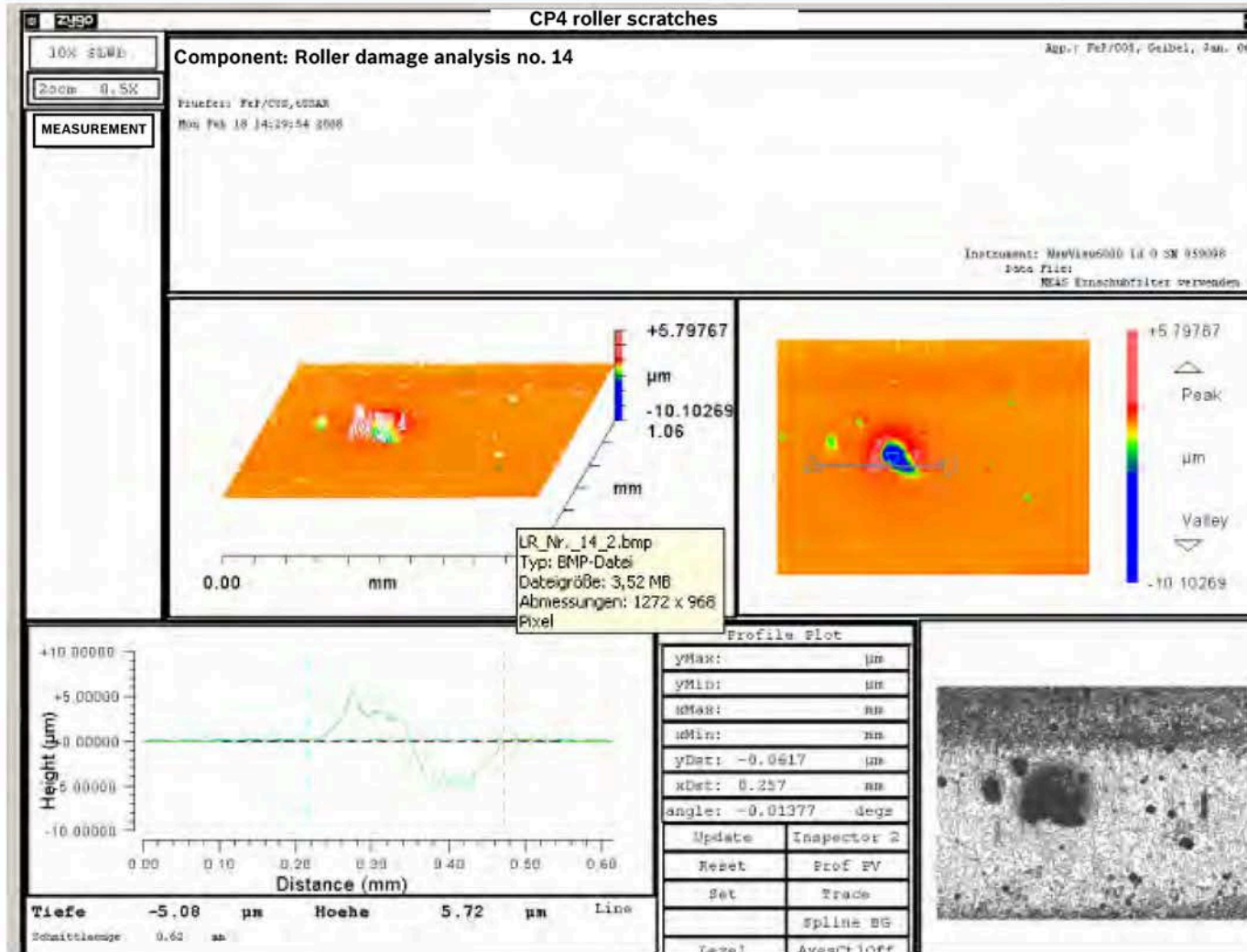
Roller_test

Roller no. 14



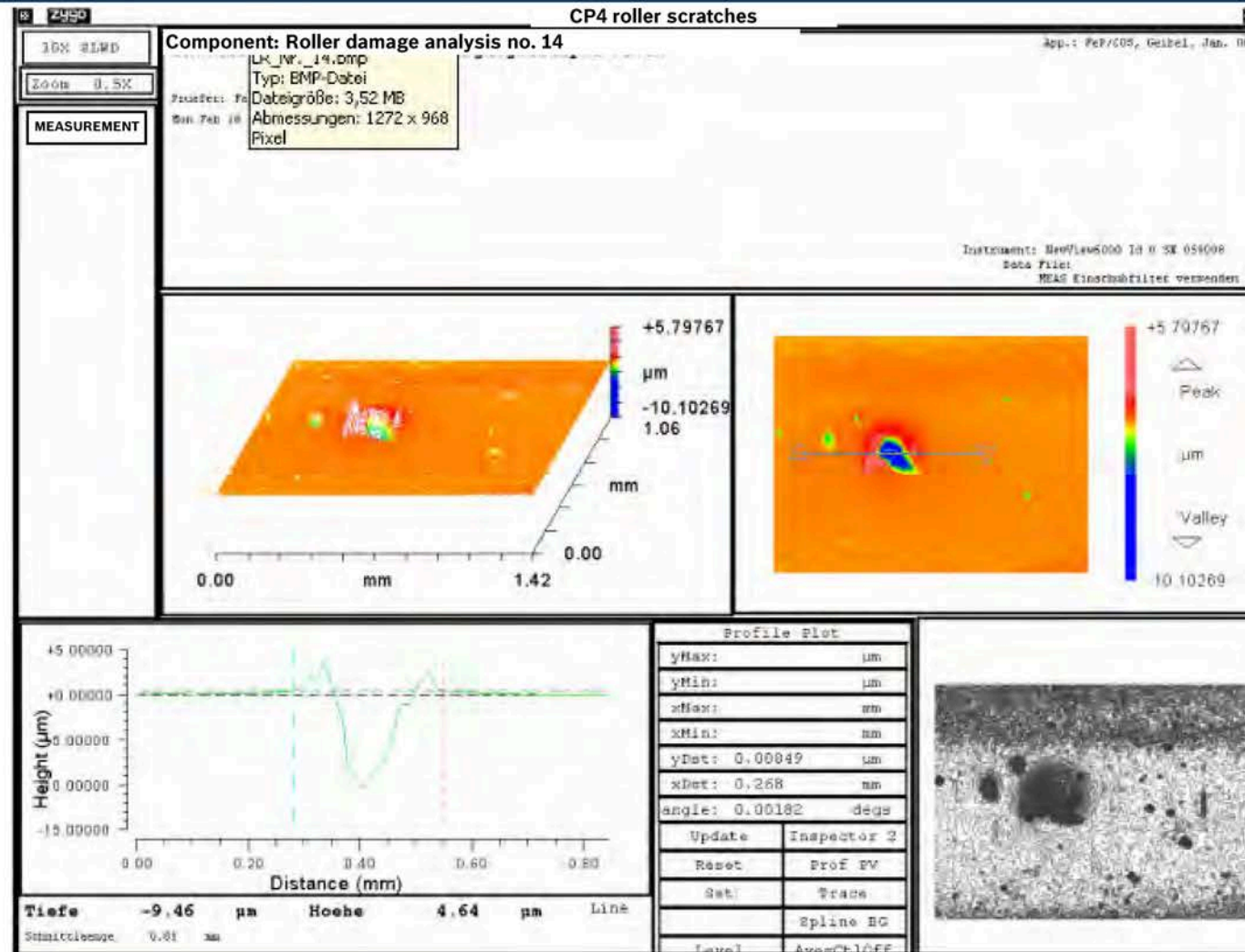
Roller_test

Roller no. 14



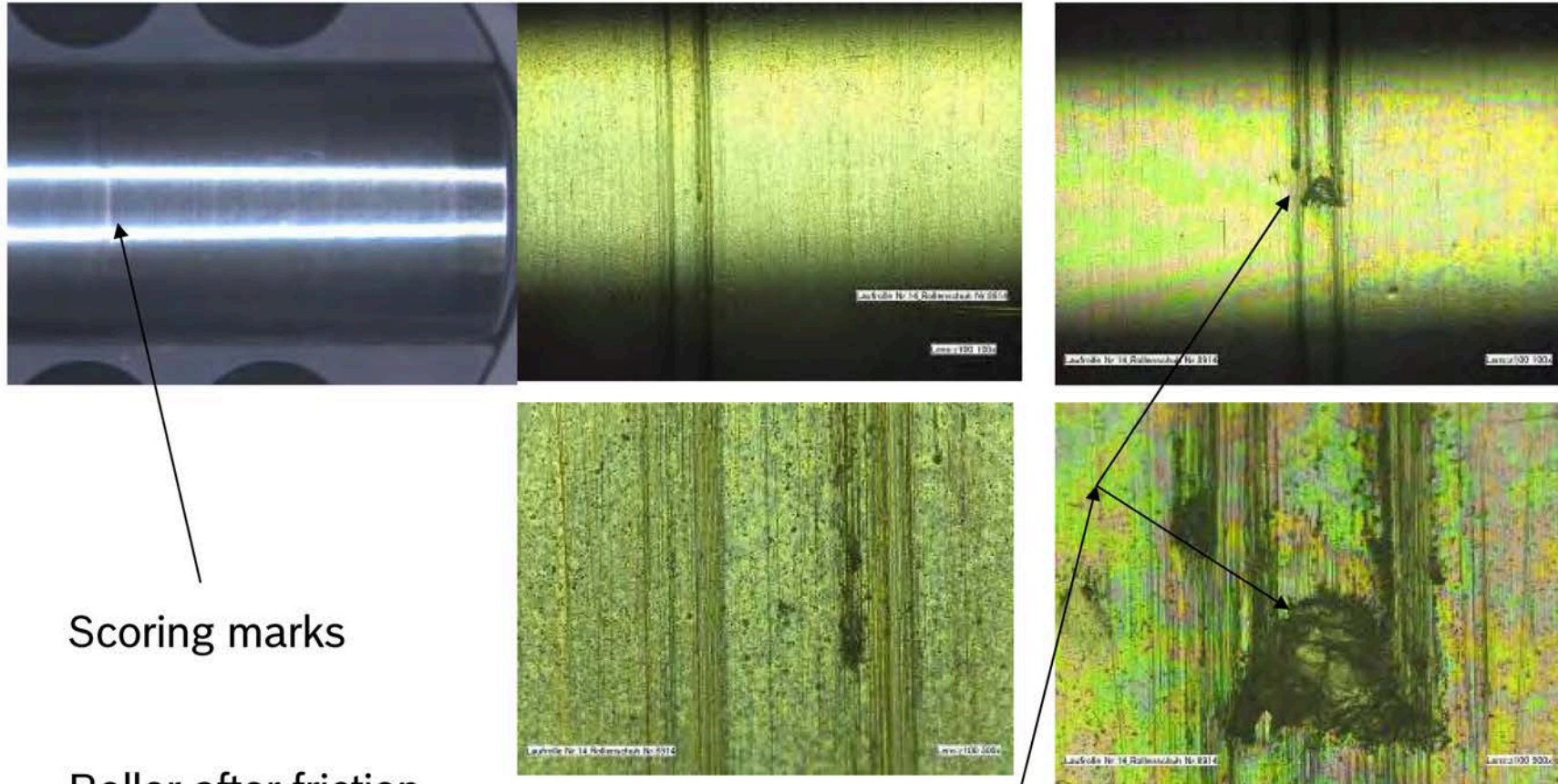
Roller_test

Roller no. 14



Roller_test

Roller no. 14



Scoring marks

Roller after friction coefficient test

Original position

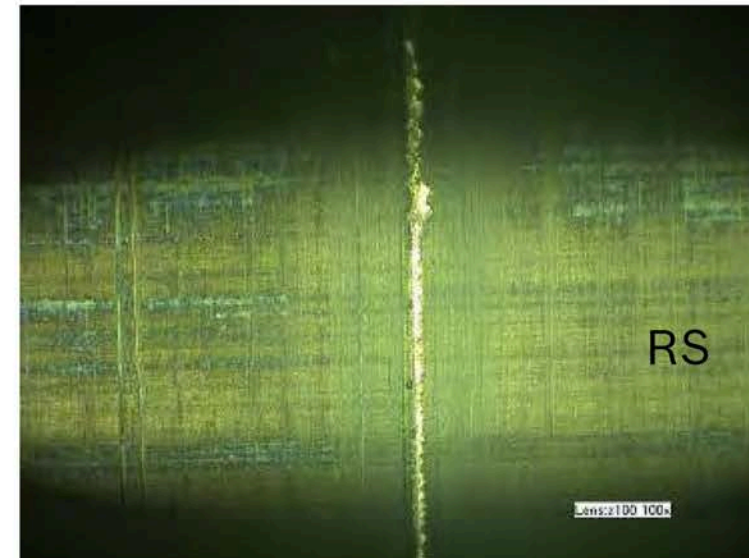
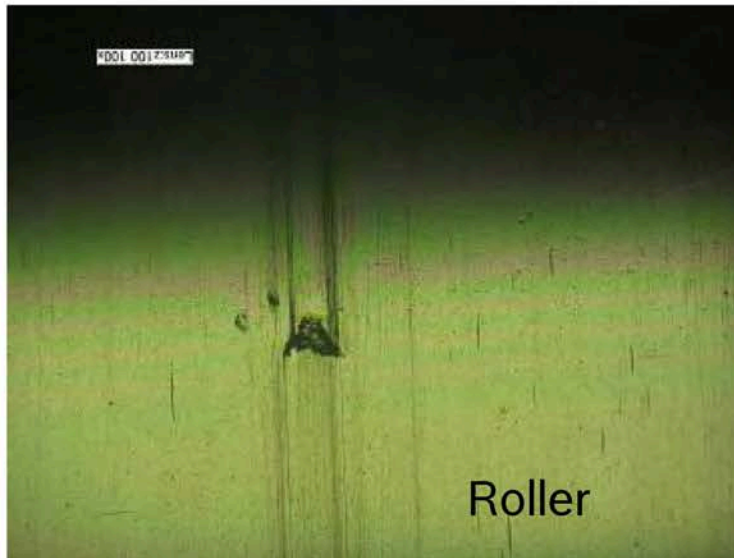


Roller_test

Roller no. 14

Seizure challenge test:

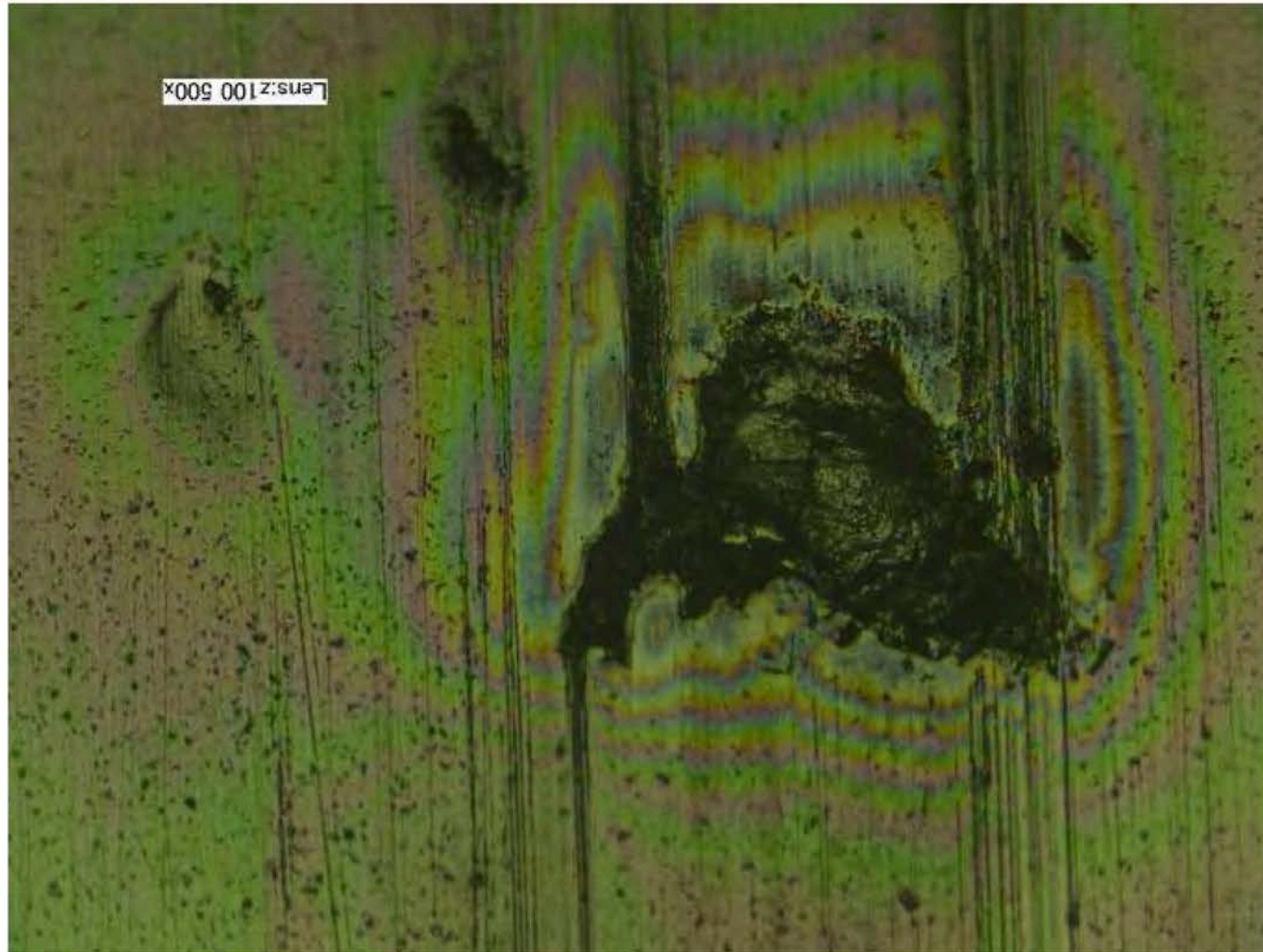
Roller no . 14 (friction coefficient OK) was installed in a pump and allowed to run with a standard program.



Result: no change to the original status

Roller_test

Roller no. 14



Roller_test

Roller no. 14



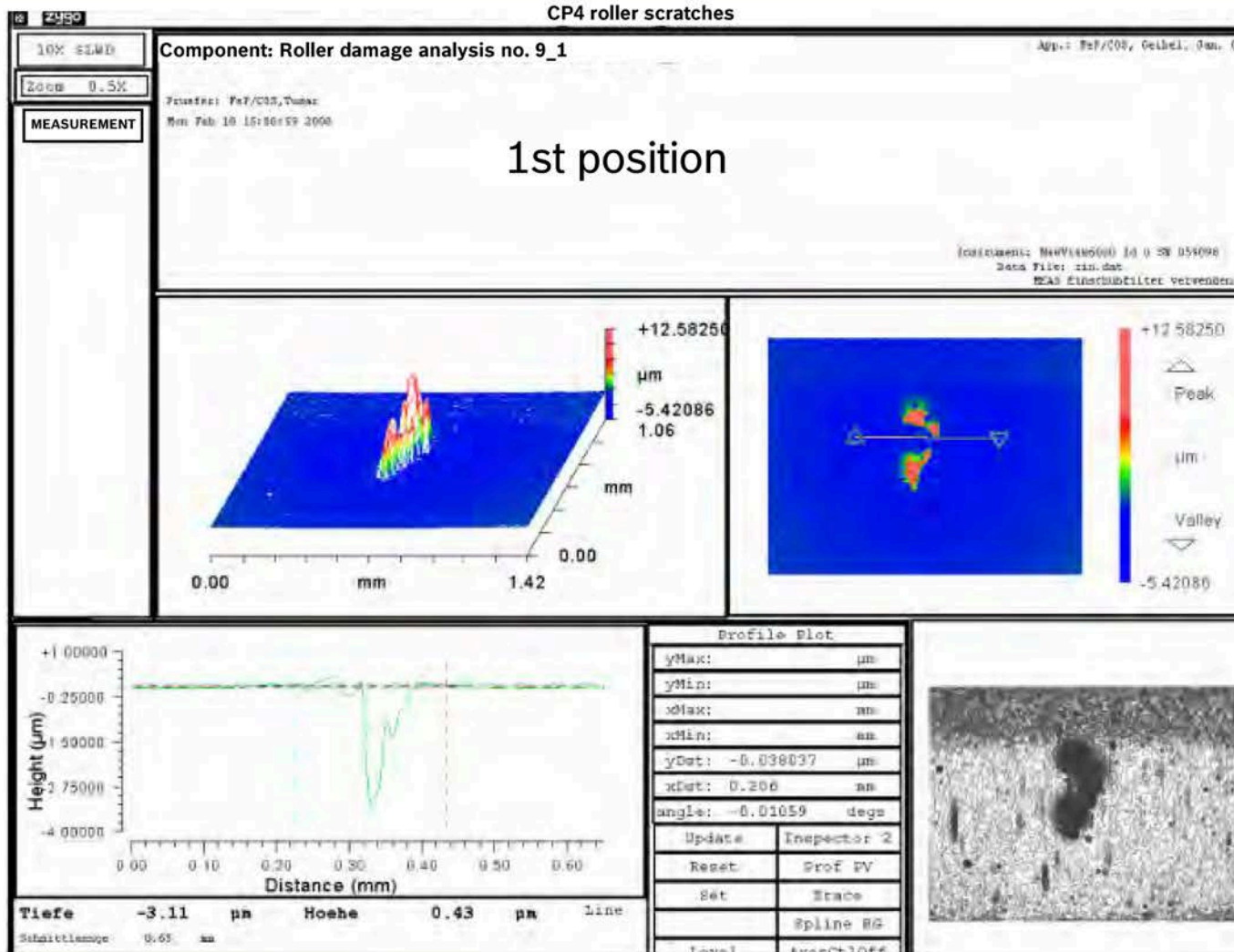
Roller_test

Roller no. 9



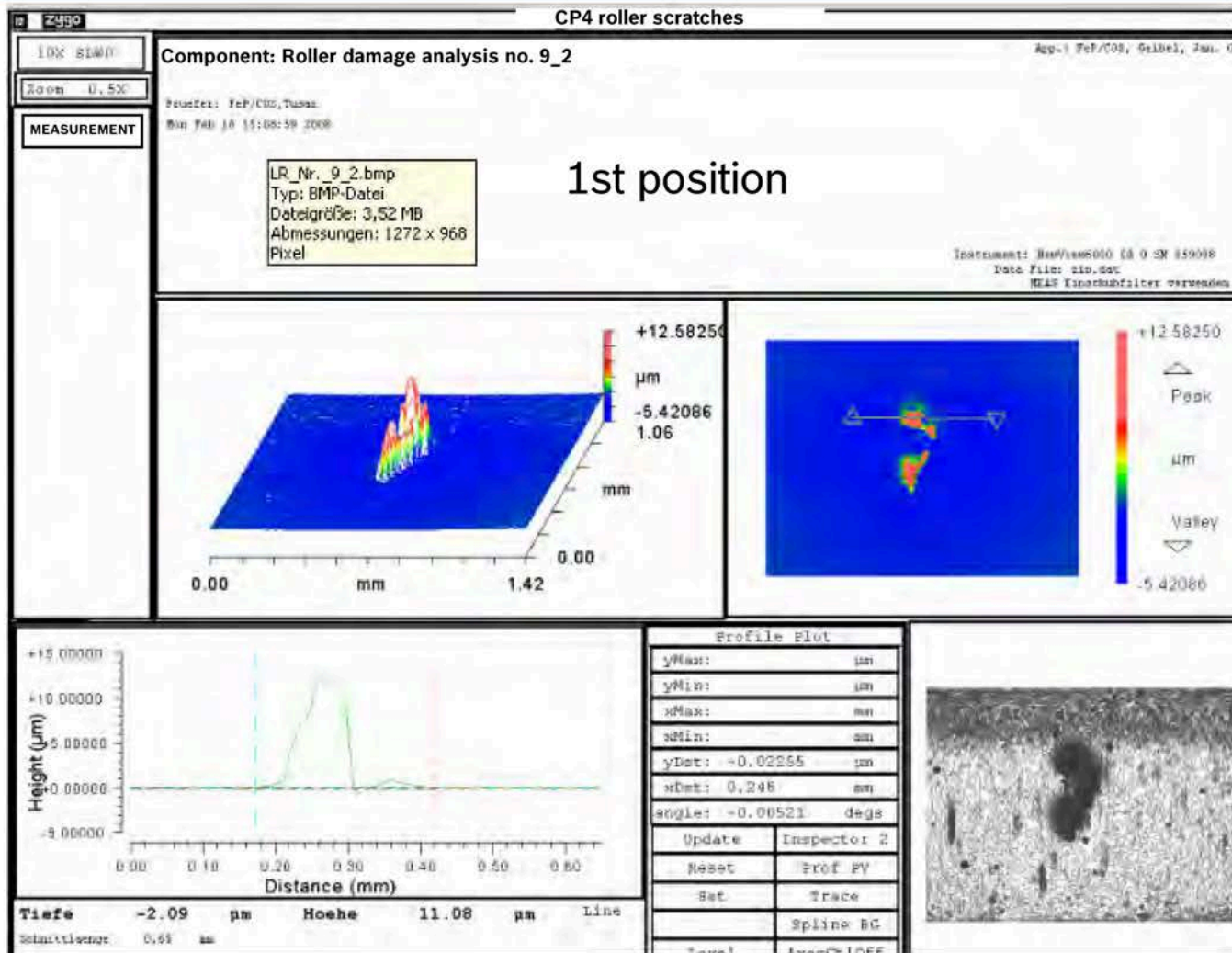
Roller_test

Roller no. 9



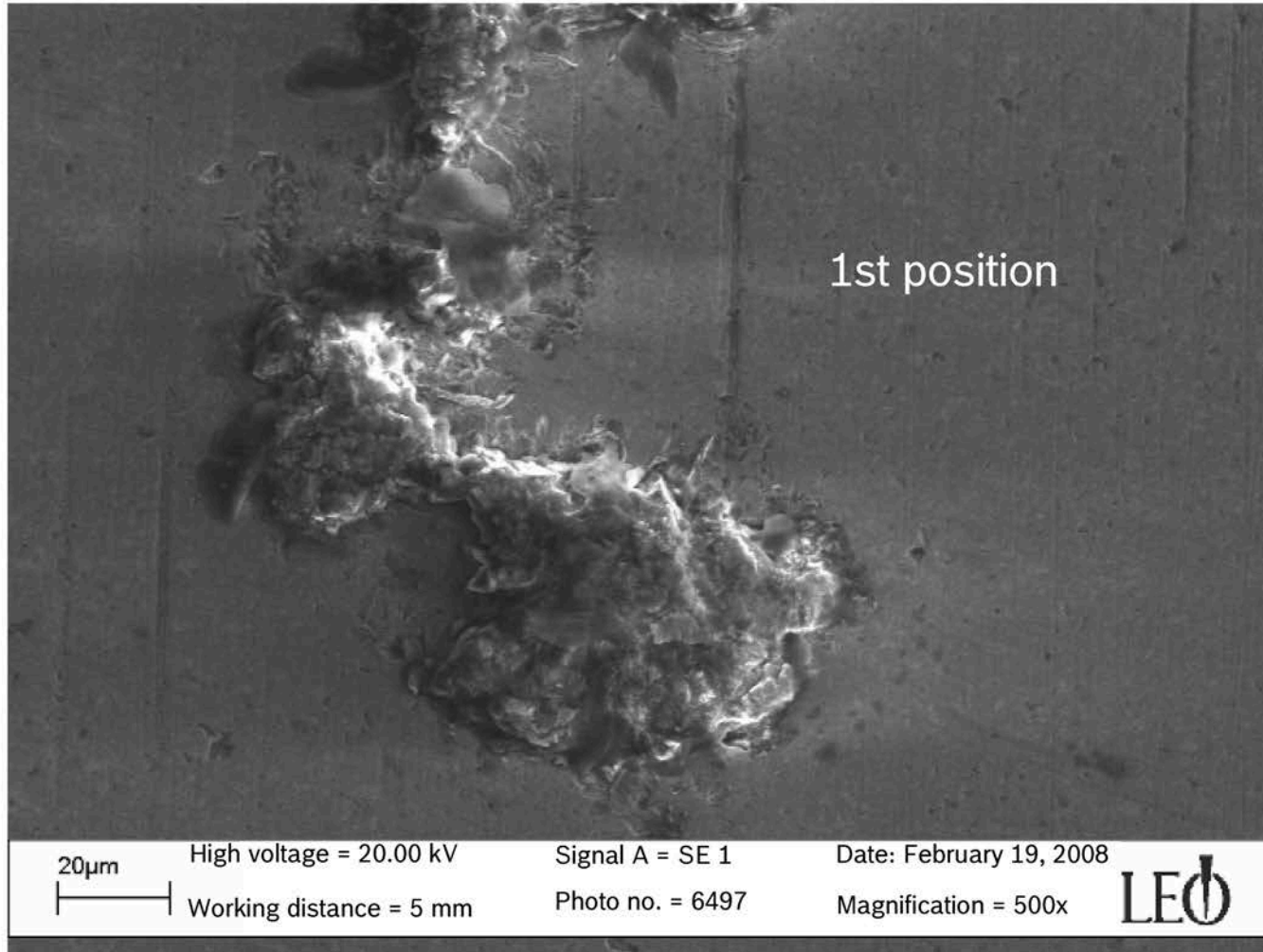
Roller_test

Roller no. 9



Roller_test

Roller no. 9



Roller_test

Roller no. 9

Spectrum processing:
Peaks omitted where possible: 0266,1039,2649,321,46 keV

Processing option: All elements analyzed (standardized)
Number of iterations = 4

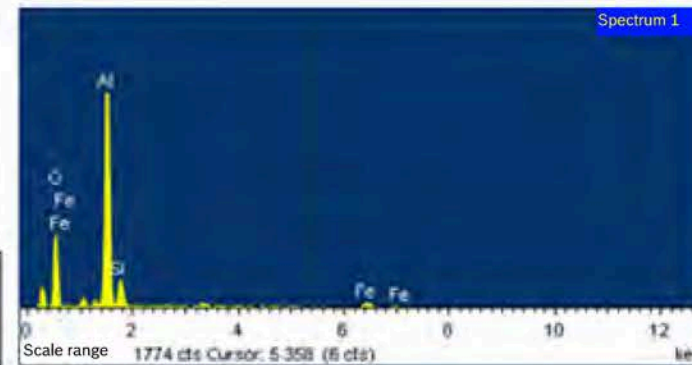
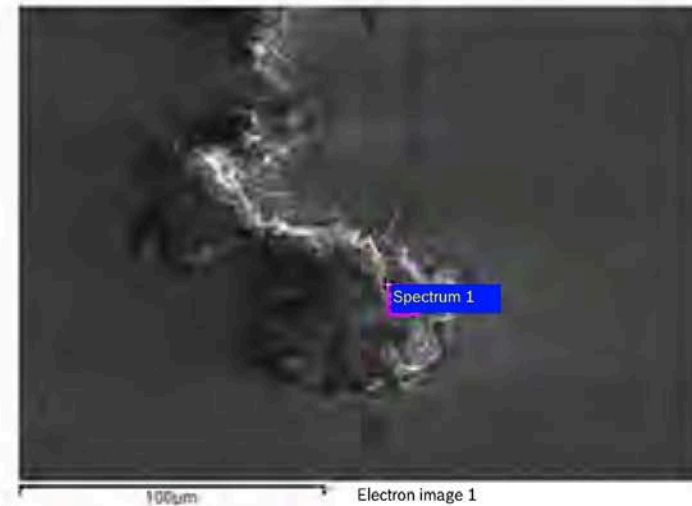
Standard :
O SiO2 1-Jun-1999 12:00 AM
Al Al2O3 1-Jun-1999 12:00 AM
Si SiO2 1-Jun-1999 12:00 AM
Fe Fe 1-Jun-1999 12:00 AM

Element	dimensions %	atom %
OK	45.57	59.67
AlK	41.61	52.30
SiK	8.70	6.49
FeK	4.12	1.55
Total	100.00	

1st position

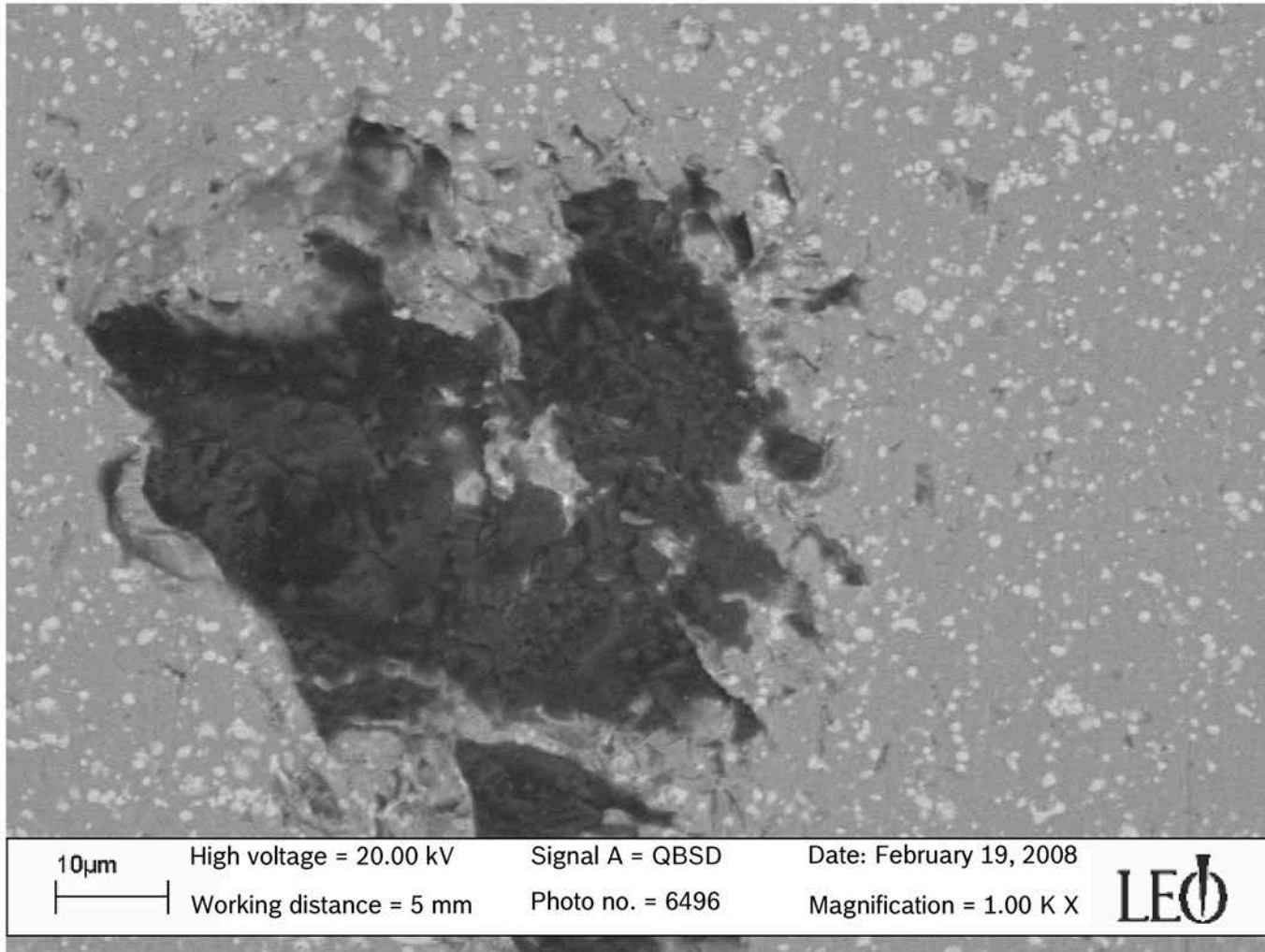
Sample comments:
Part no. 9

Comments:



Roller_test

Roller no. 9



Roller_test

Roller no. 9

Spectrum processing:
Peaks omitted where possible: 0268,1795,2291,4976,5424 keV
Processing option: All elements analyzed (standardized)
Number of iterations = 4

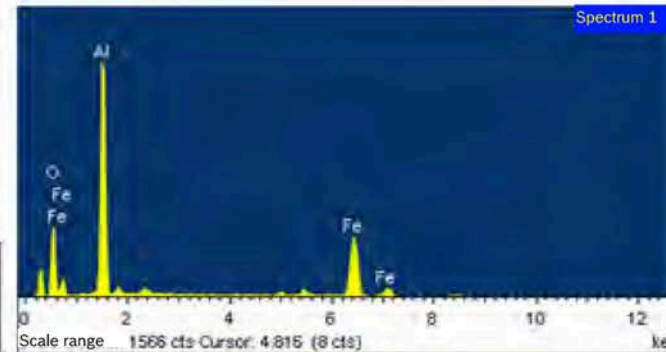
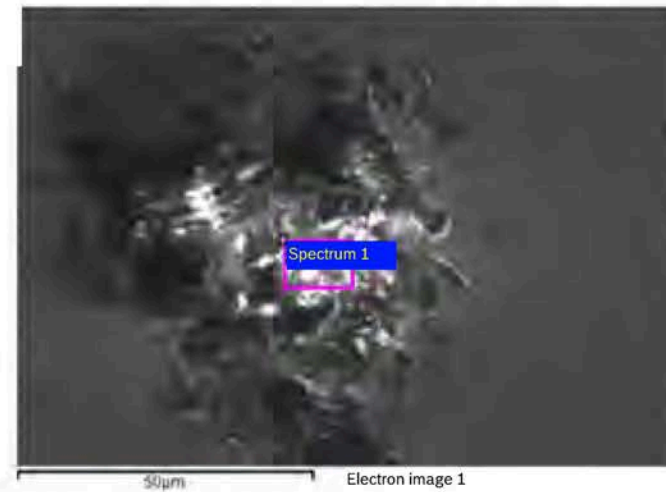
Standard:
O SiO2 1-Jan-1999 12:00 AM
Al Al2O3 1-Jan-1999 12:00 AM
Fe Fe 1-Jan-1999 12:00 AM

Element	dimensions %	atom %
O K	25.81	44.01
Al K	37.78	38.20
Fe K	36.41	17.79
Total	100.00	

2nd position

Sample comments:
Part no. 9

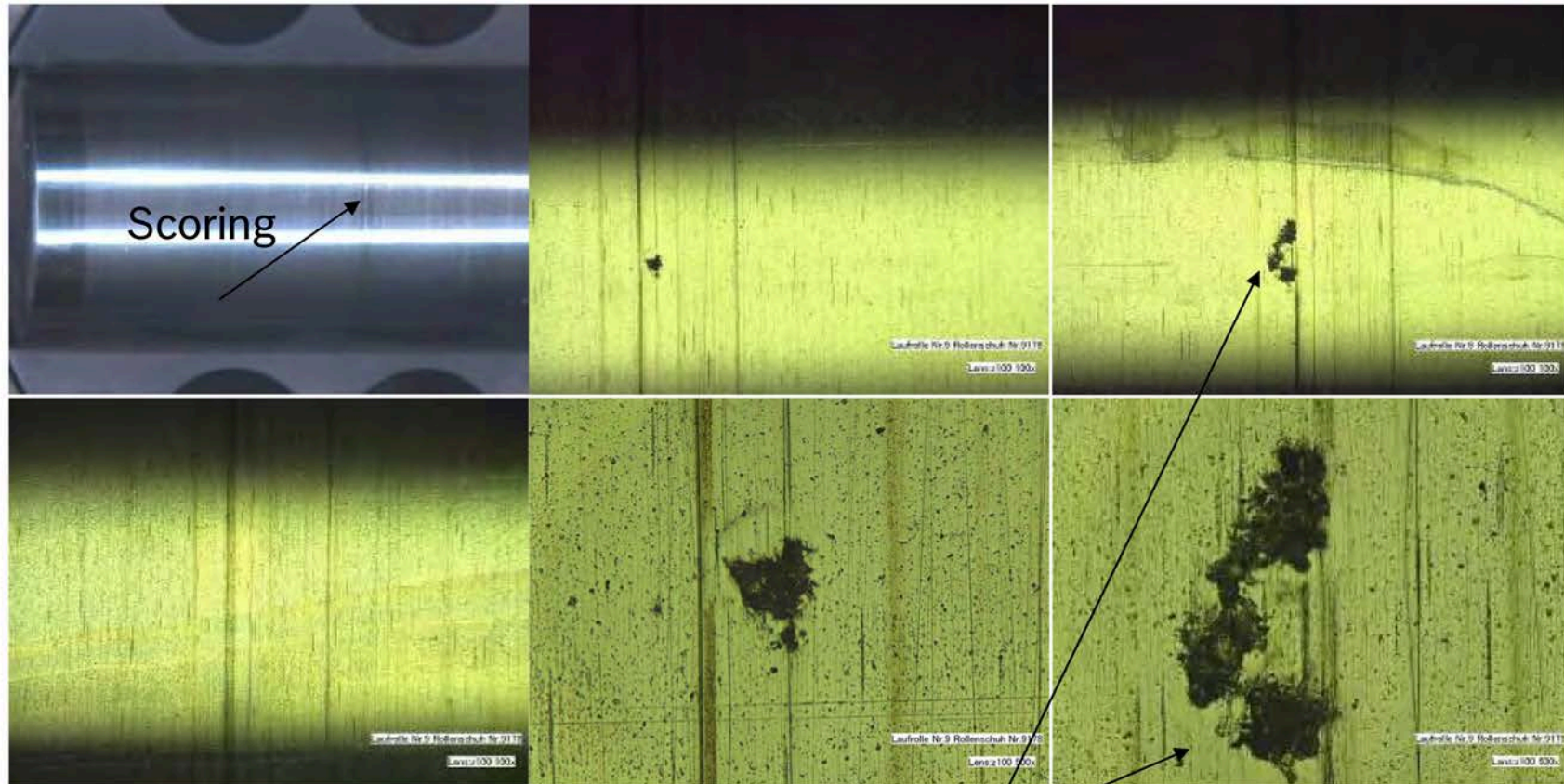
Comments:



Roller_test

Roller no. 9

Roller after friction coefficient test:



Original position

Roller_test

Roller no. 9



Roller_test

Roller no. 9

Seizure challenge test:

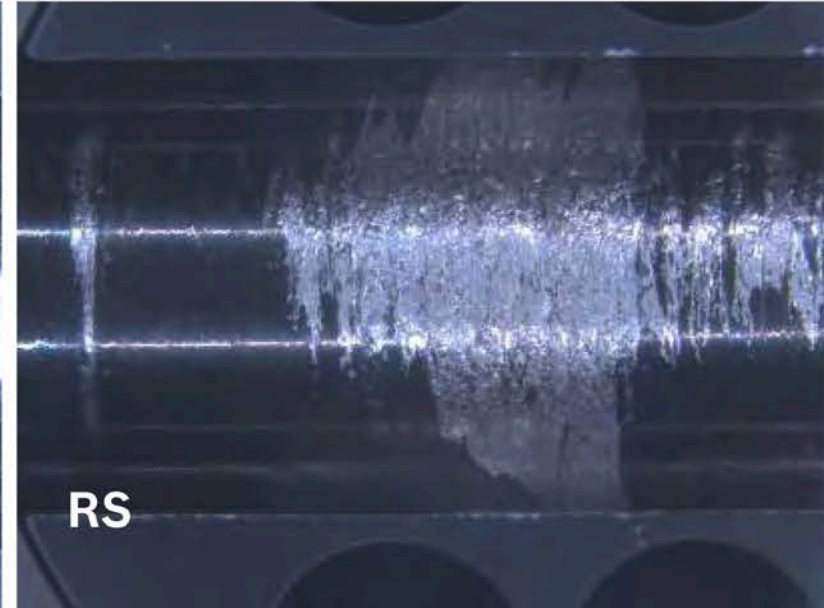
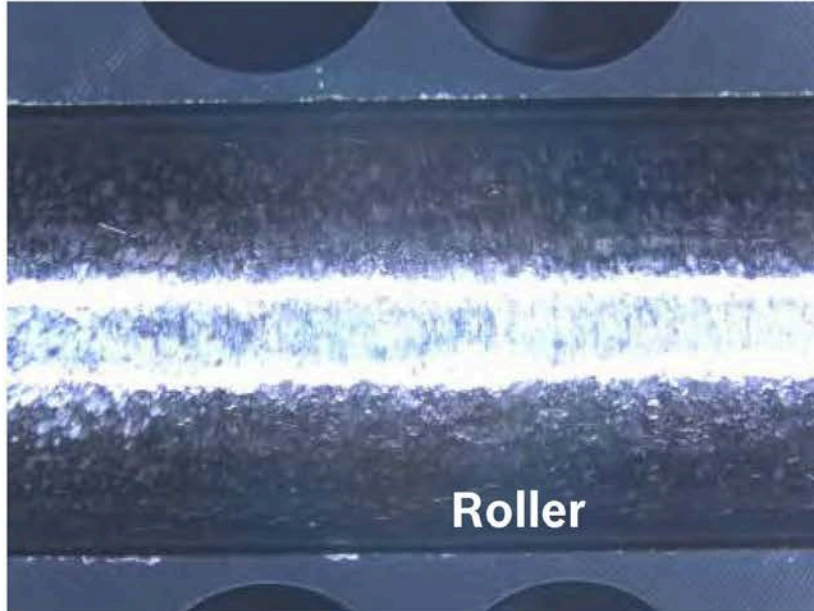
Roller no . 9 (friction coefficient not OK) was installed in a pump and allowed to run in a standard program.

Result: Failure of the pump in TP9 at 3,375 rpm and 1800 bar, complete roller wear



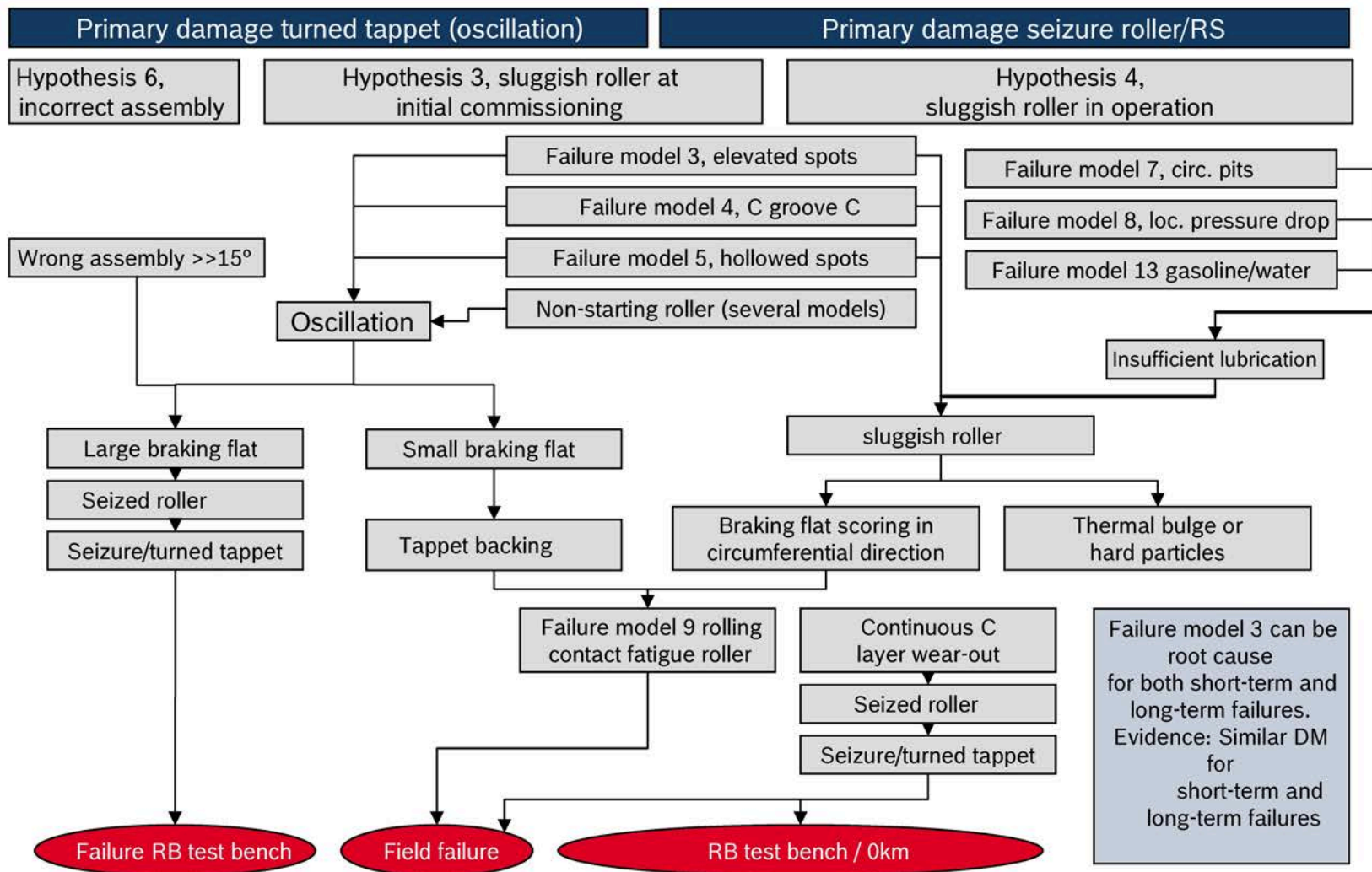
Roller_test

Roller no. 9



Circumferential roller wear, no 90° turning evident

Status drivetrain damage SC 3/19/2008



C3: Avoiding metal splashes

Status

- Graphite covers on metal brackets in the main power area
 - ⇒ 0.2% (1 of 480) metal splashes discovered directly on the adhesive layer, standard: 0.2 – 0.4%

Hypothesis derived: Shielding plate between the source and the component is the cause for metal splashes during the conditioning of the C3 source

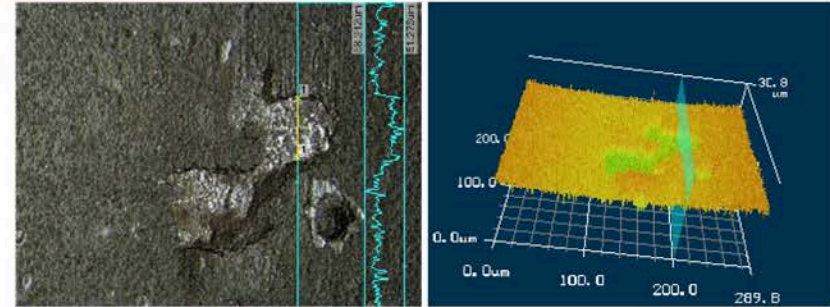
- Influence of the shielding plate reduced during conditioning, metal bracket used
 - ⇒ A striking feature



C3: Avoiding metal splashes

Status

Reduced influence of the shielding plate: Status of the analysis of the striking features:



→ SEM analysis - NMI:
both the topography as well as the EDX analysis (element analysis)
suggest that the striking feature is not metal splashes

→ FIB section follows

Result:

→ Probable relevant mechanisms for metal splash generation and
successful avoidance measure found

C3: Avoiding metal splashes

Proposed further work

Statistical verification of the result: One process with 2880 roller supports

- Additional verifications already carried out in the run-up (model wear)
- Recommendation for a positive test: Immediate conversion to optimized process



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Sent: Monday, April 07, 2008 1:44 PM
Subject: Agenda for 3. Audi CP4 zero-fault meeting on 04/10/2008 with a focus on drivetrain damage

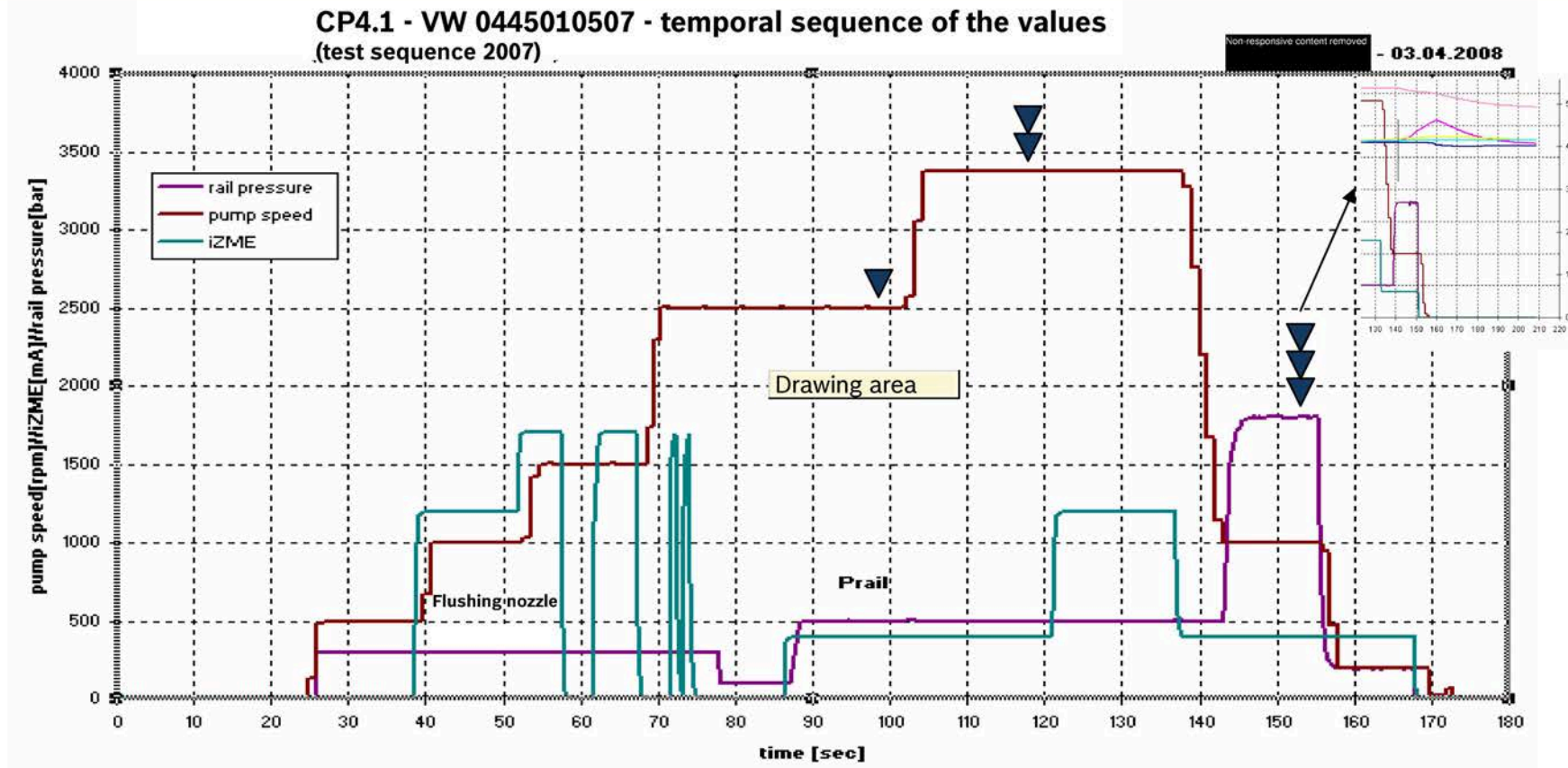
Agenda for 3. Audi CP4 zero-fault meeting on 04/10/2008 with a focus on drivetrain damage

PN: Audi: Non-responsive content removed
 VW:
 Bosch:

1. 08:00 - 08:15 AM CP4-Q situation 0km/field Audi/VW, Non-responsive content removed
 R: [REDACTED]
 CP4-Q-situation 0km/field Audi/VW, Non-responsive content removed
 R: [REDACTED]
2. 08:15 - 11:00 AM Status of drivetrain damage, OPL fr. telco from 03/05/2008,
 - 2.1 08:15 - 08:25 AM Failure hypotheses for drivetrain damage (if required)
 [REDACTED]
 - 2.2 08:25 - 09:00 AM Major test on metal splashes io the roller support (RS)
 R: [REDACTED]
 - 2.3 9:00 - 9:20 AM Avoid metal splashes on the roller support (RS)
 R: [REDACTED]
 - 2.4 09:20 - 09:45 AM Avoid elevations on roller
 R: [REDACTED]
 - 2.5 09:45 - 09:55 AM Presentation of Bosch CP4.1 and CP4.2 functional test sequence old/new with indication of internal drivetrain failures old/new
 R: Non-responsive content removed
 - 2.6 09:55 - 10:05 AM Recording actual sequence of the cold and hot test benches Audi Györ, VW Chemnitz, and Salzgitter Skoda
 R: Non-responsive content removed
 - 2.7 10:05 - 10:30 AM Appraisal of 3 CP4.1 from R4, 2.0l engine Audi Györ
 R: [REDACTED]
 Appraisal of 1 CP4.1 from VW Jetta (US07), verification vehicle
 R: [REDACTED]
 - 2.8 10:30 - 10:40 AM Question from [REDACTED] regarding set cold test run in Györ: Can/should the time be retained with speed 1000 and rail pressure ZERO???
 Please compare the two target curves; in my opinion, they are different (one is 9 sec, one is 2 sec). Which applies?
 R: [REDACTED]
 - 2.9 10:40 - 10:45 AM Audi/VW cold test process differences - why
 R: Non-responsive content removed
 - 2.10 10:45 - 10:55 AM Checking the production, assembly and testing data of failed CP4.1 for striking features
 R: [REDACTED]
 - 2.11 10:55 - 11:00 AM How can a turned tappet be reliably detected at RB? Description click-clack test (production tour)
 R: Non-responsive content removed
3. 11:00 AM - 12:30 PM Production inspection
 - 3.1 Handling of CP4 reworking, not OK Function test (DNA table)
 R: [REDACTED]
 - 3.2 Acceptance of module 4
 R: [REDACTED]
4. 12:30 - 1:15 PM Lunch (canteen)

5. 1:15 - 1:25 PM Comparison of the relative properties Bosch
test oil with diesel
R: Non-responsive content removed
6. 1:25 - 1:45 PM Statement by Bosch concerning the topic of anti-turning locks
R: Non-responsive content removed
7. 1:45 - 2:00 PM Inspection 4. module, Feuerbach plant
1.1 Change notification - Module 4. Parts production
1.2 Verification sheet FeP/QMM3
R: Non-responsive content removed
8. 2:00 - 2:10 PM Status of MU O-ring leak, pump verification vehicle
R: Non-responsive content removed
9. 2:10 - 2:15 PM Coordination 2DP date, GP38 Hallein
R: Non-responsive content removed
10. 2:15 - 2:30 PM Audi requirement 250µm, status test
R: Non-responsive content removed
11. 2:30 - 3:00 PM Final meeting
R: all

VW_Drivetrain damage_Failure overview

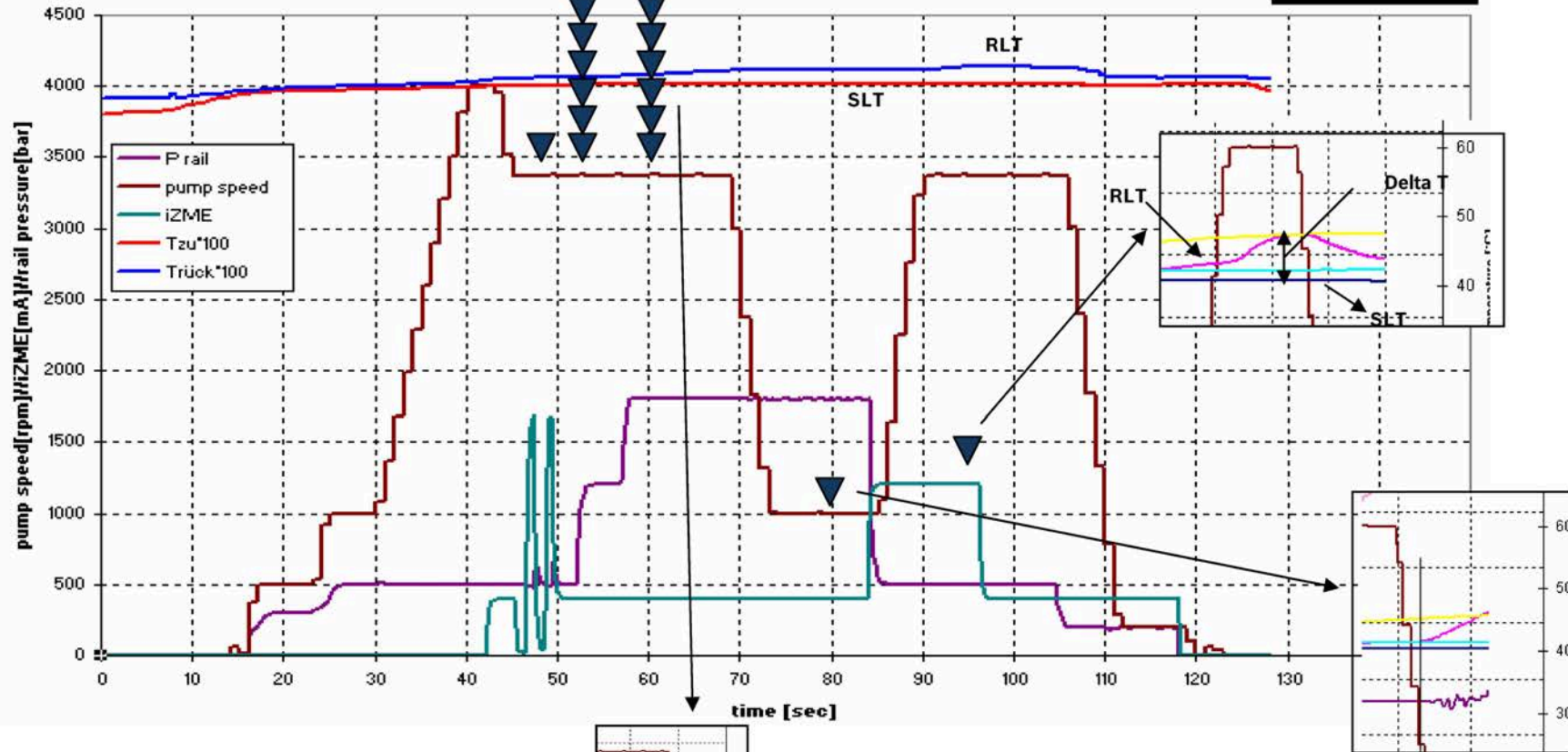


▼ Point of failure via rail pressure, Delta T, etc.



VW_Drivetrain damage_Failure overview

CP4.1 - VW 0445010507 - temporal sequence of the values
(current test sequence),



▼ Point of failure via Delta T, rail pressure



CP4, Tappet anti-turning lock, Status 3/2008



Contents

- Motivation
- Design
- Testing
- Schedule
- Summary of results



CP4, Tappet anti-turning lock, Status 3/2008



Motivation

Following occurrence of the initial CP4 drivetrain damage during internal testing or the first start-up of the engine at the customer's, various failure hypotheses were developed.

One hypothesis was that turned tappets are the cause for subsequent drivetrain damage. To counter this, development on the tappet anti-turning lock was started.

The hypothesis established at that time can no longer be upheld with today's information. The cause for the occurring drivetrain damage is either a stiff and/or stuck roller. The subsequent turning of the tappet is therefore a consequence of the stiff / stuck roller. If turning were to be prevented by an anti-turning lock, this would simply delay the failure and not prevent it. Through the introduction of suitable measures in the assembly process (laser scanning of the tappet position), turned installation of the tappet was effectively excluded.

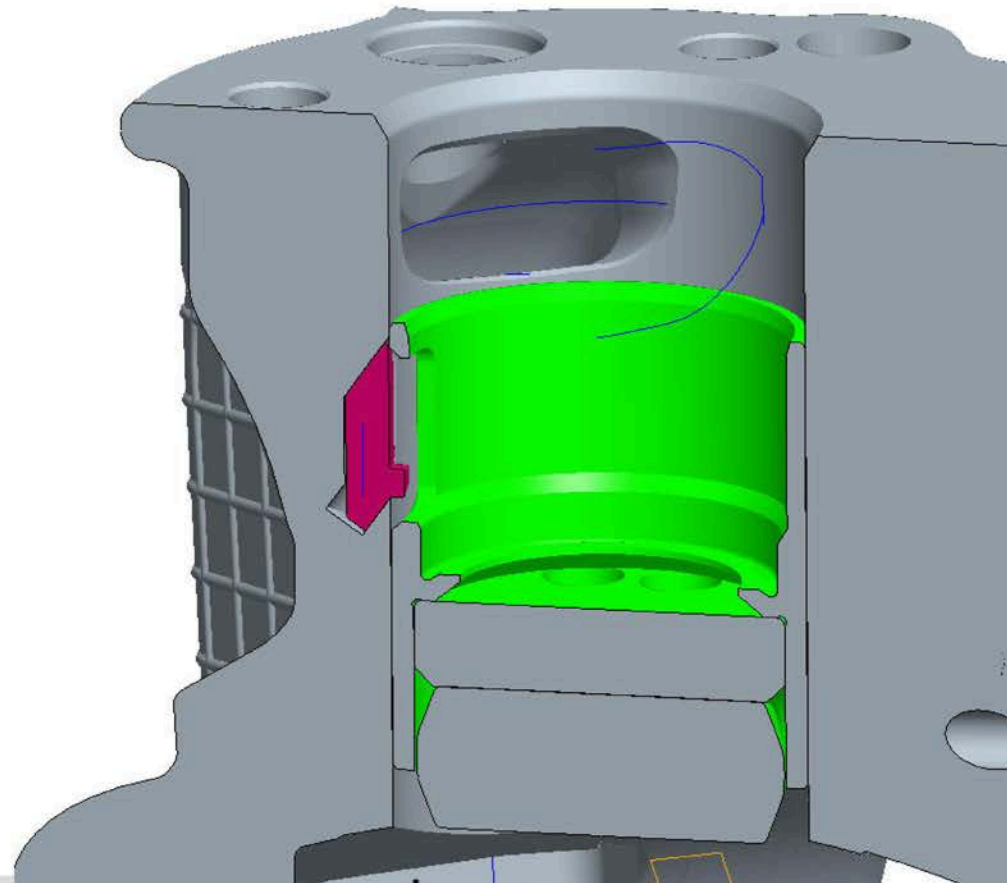
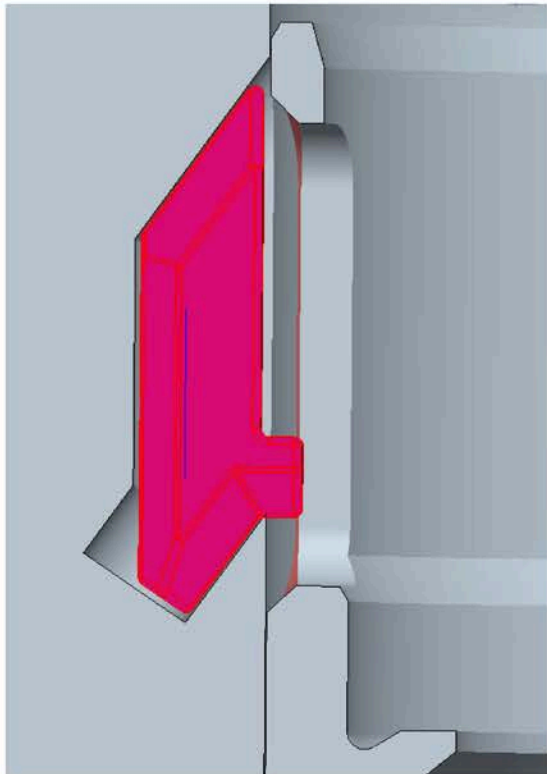


CP4, Tappet anti-turning lock, Status 3/2008



Design

- Preferred solution: Variant with fitted key as insert



CP4, Tappet anti-turning lock, Status 3/2008



Testing:

- First 2 pumps after approx. 500h ER indicate a good result.
- Parts from near-series production process show tappet break-ages (deformation, internal stresses in tappet body)



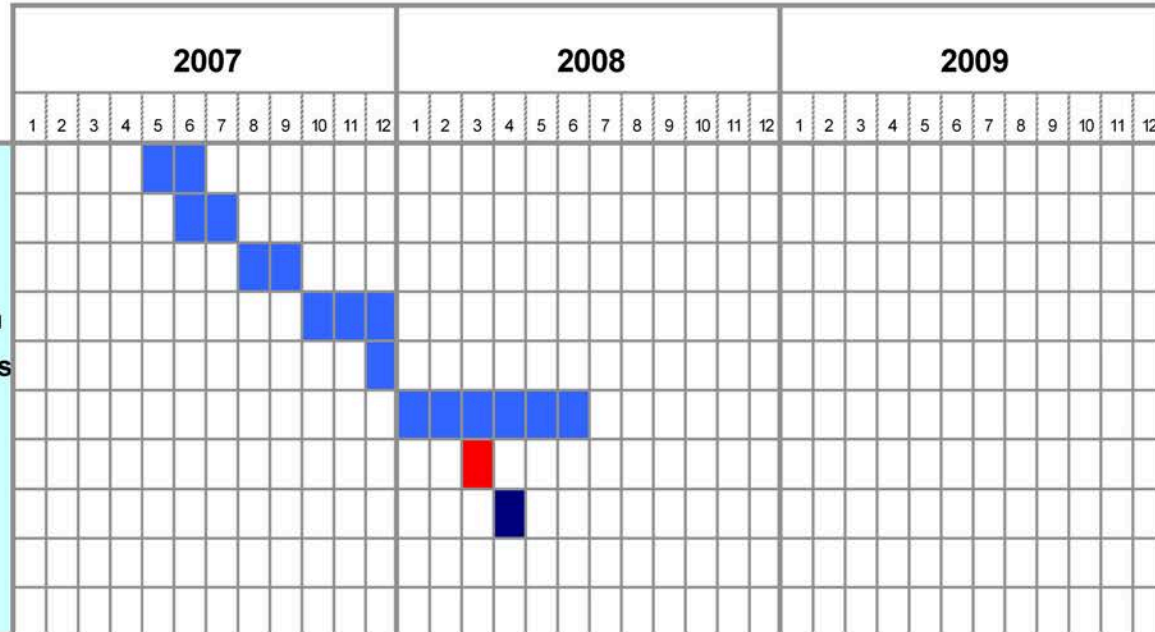
CP4, Tappet anti-turning lock, Status 3/2008



Schedule

CP4 Tappet anti-turning lock

- Concept phase
- Design/sampling
- ER 2 x 500h (first verification)
- Revision/series production preparation
- Sample availability of pre-production parts
- ER 2 x 2,000h (validation)
- Development stop
- Pump findings after approx. 250h



CP4, Tappet anti-turning lock, Status 3/2008



Summary of results

- Initial ER results are positive with respect to potential durability of the anti-turning lock described
- Near-series parts produced show weaknesses with regard to durability
- Today's findings on drivetrain damage show that turned tappet is a consequence and not the cause of the drivetrain damage. Stiff rollers are the cause of drivetrain damage. Anti-turning lock is not a corrective measure or does not increase robustness of this.
- Head of development decides to stop development on 3/2008
- Remaining ER pumps are stopped and final findings recorded



Straightedge test on roller

Objective of test:

Identify rollers with various types of elevations (fusing, pushed-in particles, etc.).



Straightedge test on roller

Procedure:

1. Remove roller from frame and place in front of blade of test equipment.
2. With one finger, press the roller against the blade slightly and cautiously turn the roller 2-3 revolutions with one finger.
3. If slight scratching is noticed, the roller can be rotated more often; if the roller can then be turned without scratching, it is OK.
4. If the roller snags noticeably or juts out while turning, the roller should be removed immediately.
5. Failed rollers should be placed by part no. and documented in the list.



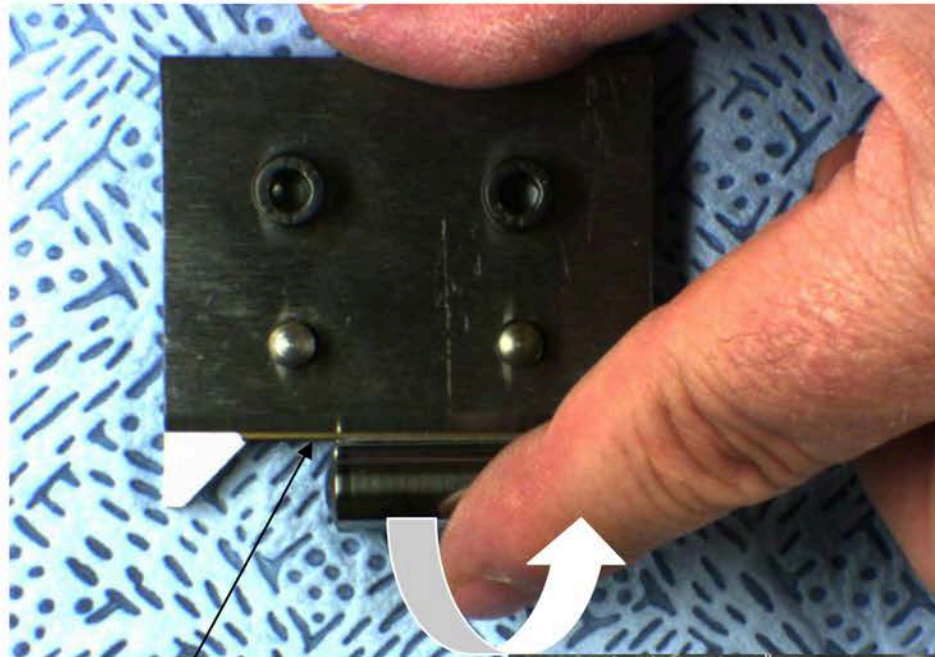
Straightedge test on roller

Remarks:

- Make sure the blade is sharp; turn or swap out the blade every 4 frames. If necessary, the blade can also be replaced earlier. Only the 2 opposite blade sides can be used.
- Wipe the blade regularly with a lint-free cloth, **be careful! The blade is very sharp.**
- Use the entire width of the blade for turning when possible, so the blade is worn evenly



Straightedge test on roller



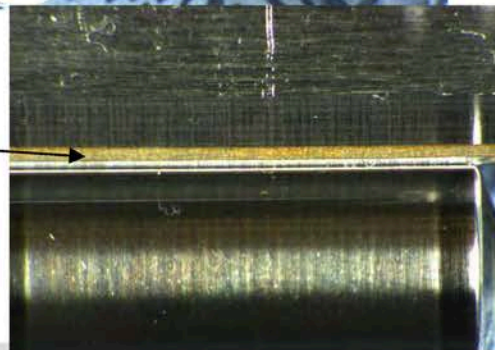
Straightedge test on roller

Roller is turned manually with a finger **against** an inserted sharp blade.

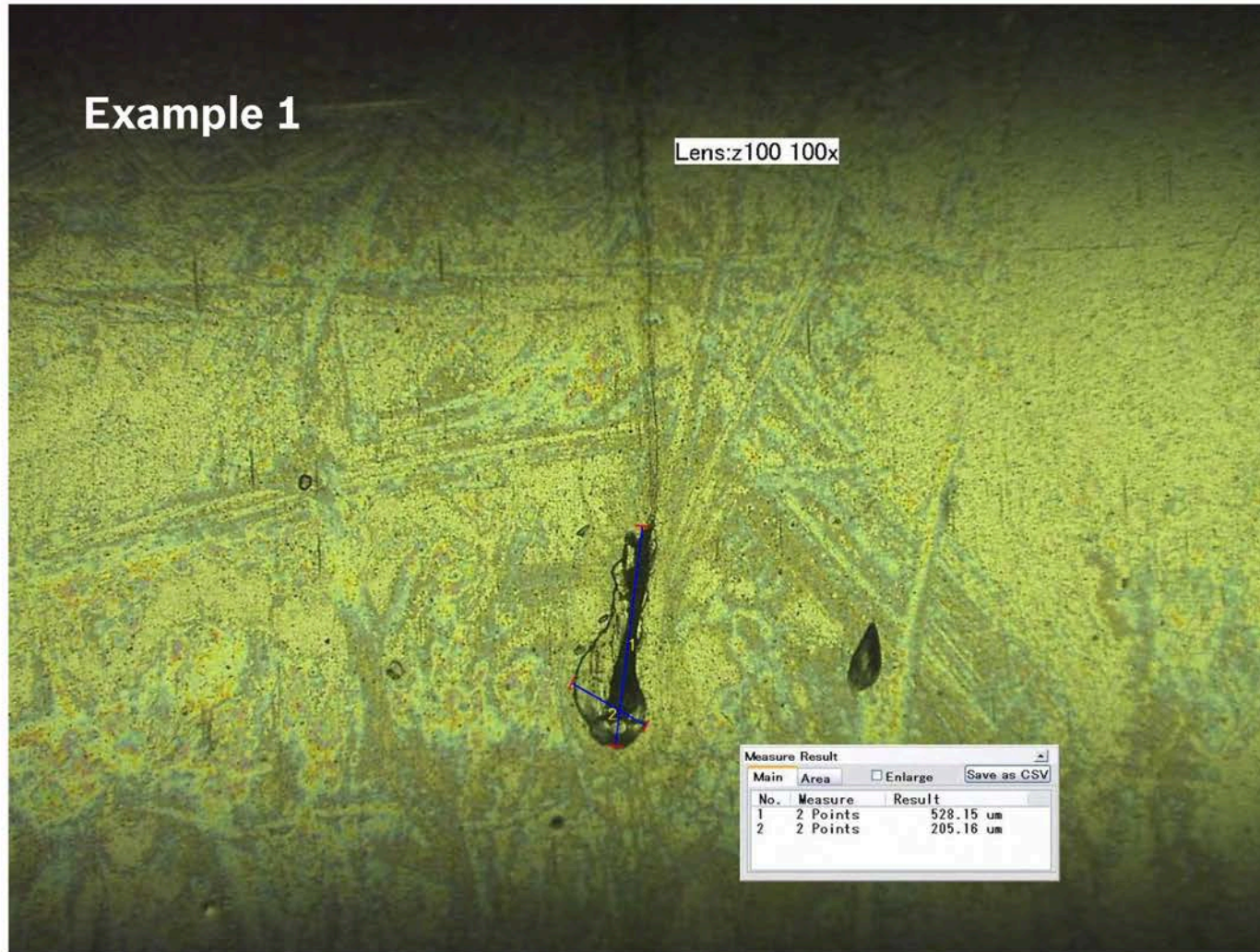
→ Approx. 2-3 revolutions

→ Elevations are detected through scratching or lifting of the roller

Inserted sharp blade

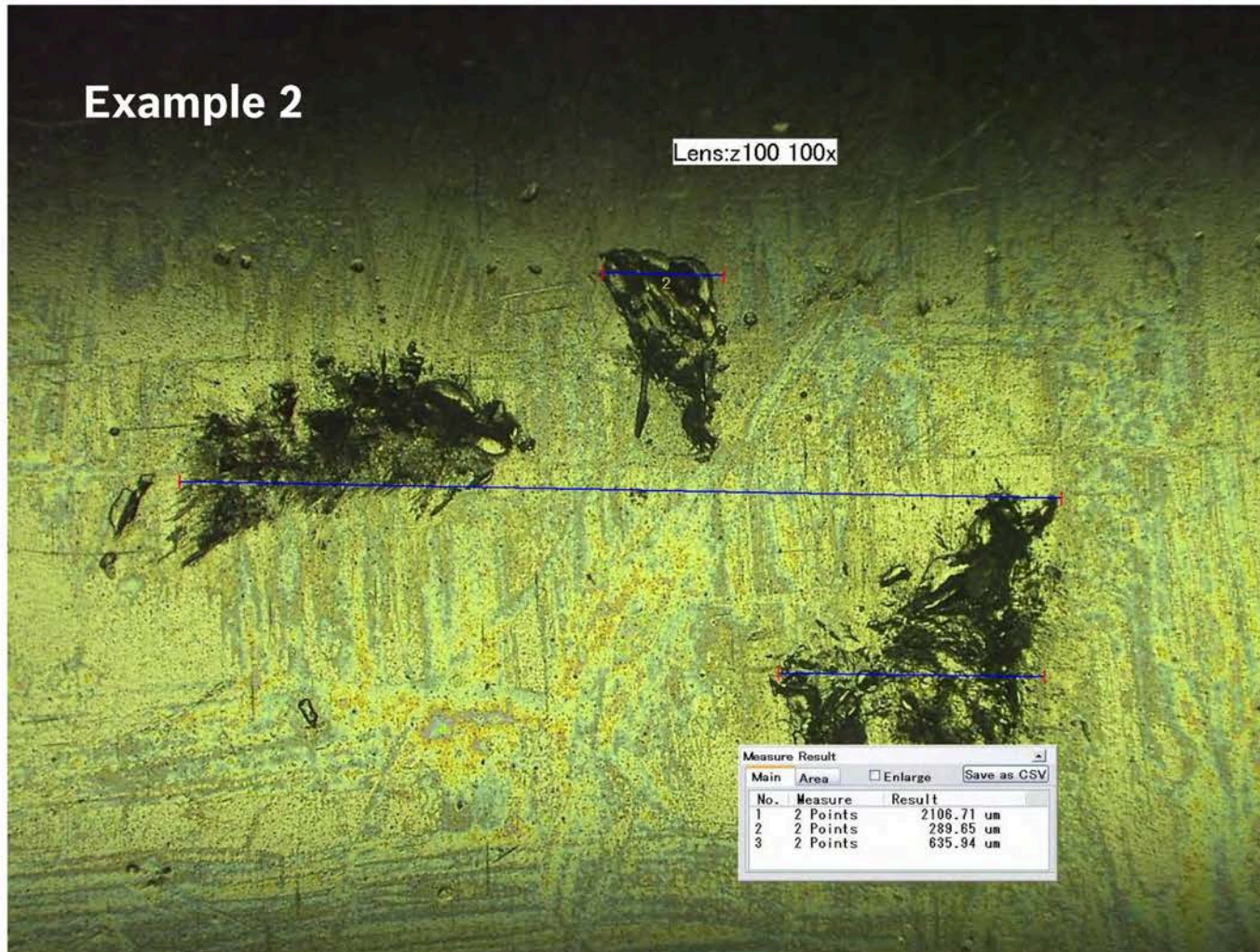


Straightedge test on roller

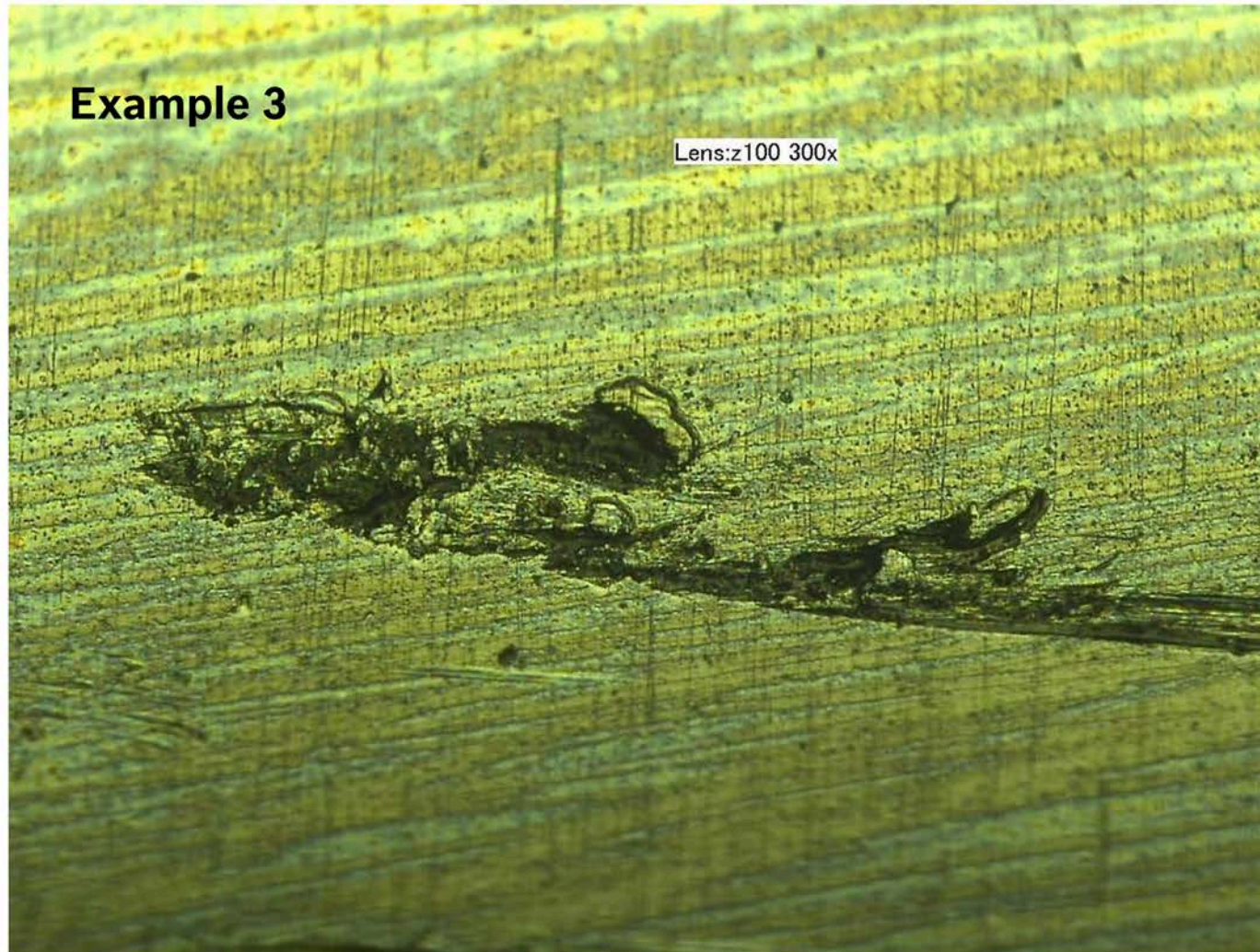


Straightedge test on roller

Example 2



Straightedge test on roller



CP4.1 (R4) and CP4.2 (V6-V8-V12) VW / AUDI Status of drivetrain damage

0km complaint

Scope of defect (current failures - March)

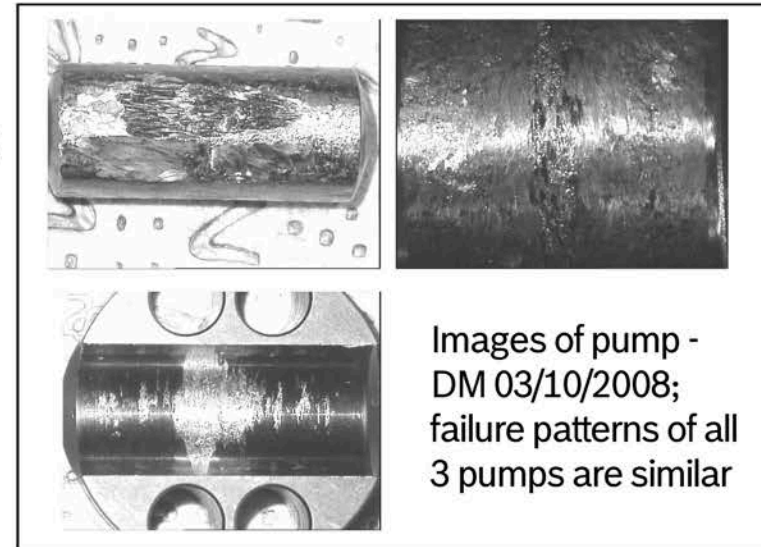
- 0km: 3 x pumps 0445010507/ 03L130755
- Pump DM 1x 03/05/2008
1x 03/10/2008
1x 03/11/2008
- Failure DM: 14.3., 17.03. 3/18/2008
- GR Bosch: 3/25/2008

Description of problem

- Failure on Audi final function test rig (cold test) with noise and rail pressure fluctuations

Cause analysis

- Considerable wear on the cam and the roller
- Possible damage profile: Increased friction between roller and roller support leads to slippage between roller and cam. This leads to damage of the cam, roller and roller support and to turning of the tappet.



CRP CP4.1 and 4.2 - AUDI 0km complaints - FeP

Total measures since SOP:

- Analysis of the assembly and handling processes carried out in Dresden on 07/12/2007. Result: Commissioning conditions not according to specification. Commissioning of the vehicles has been changed immediately
- Optimization of test bench process of Bosch by raising the start-up speed from 200 rpm to 500 rpm
D: 7/9/2007 compl.
- Cylinder head assembly with 5° torsion allowance
D: 07/23/2007 compl.
- Dry pressing in of roller support
D: 07/23/2007 compl.
- Introduction of dwell time during mounting of tappet assembly
D: 8/28/2007 compl.
- Extension of high-load testing point
D: 10/12/2007 compl.



CRP CP4.1 and 4.2 - AUDI 0km complaints - FeP

Measures

- Improved visual inspection of the roller support according to new visual inspection catalog D: 12/13/2007 compl.
- Friction coefficient test +/- 10° for an improved checking of the main load area of the roller support
D: 12/13/2008 compl.
- Introduce tappet position query by means of laser to ensure the tappet is fitted in the correct place during assembly
12/21/2008 compl.
- Introduction of a new test program for CP4.1 VW with intensified test conditions i.e.
 - Start-up with steeper speed ramp in order to cause drivetrain damage internally and not at the customer
 - Critical load points (1,800 bar) moved from end of test process to start of test process, so that drivetrain damage can be better detected.
 - Elimination of the flushing nozzle, thus detection of not OK rail pressures even during flushing of the pump and omission of the critical switching procedure from flushing to measuring.
 - Flush operation of 300 bar and 2,500 rpm to 1,800 bar and 3,375 rpm - revolutions intensifiedD: 1/11/2008 compl.



CRP CP4.1 and 4.2 - AUDI 0km complaints - FeP

Measures

- Introduction of visual inspection of the roller support using a technoscope instead of a magnifying glass for a better detection of the metal splashes
D: 2/4/2008 compl.
- Introduction of a new test program for CP4.2 Audi with intensified testing conditions analog to VW for CP4.1, T: 2/5/2008 compl.
- 100% straightedge test on the roller to detect elevations on the roller. Parts have been found since the introduction of the test. Parts will be used for major test.
D: since 04/01/2008 in parts production, as of 04/07/2008 in the pump
- Measures currently in testing C coating:
Roller support (RS):
 1. Reduction of the influence of the shielding plate, test with 480 RS batch; first result positive, FIB section still open; if FIB section positive - step 2.
 2. Reduction of the influence of the shielding plate, test with 2,800 RS batch; is result positive then Audi will authorize the changeover of the C coating process;
planned date of introduction: 4/18/2008



CRP CP4.1 and 4.2 - AUDI 0km complaints - FeP

Measures

Measures currently in testing C coating:

Roller:

Optimized holder concept for roller to avoid fusing

D: currently being clarified as the change to the holder is quite intensive



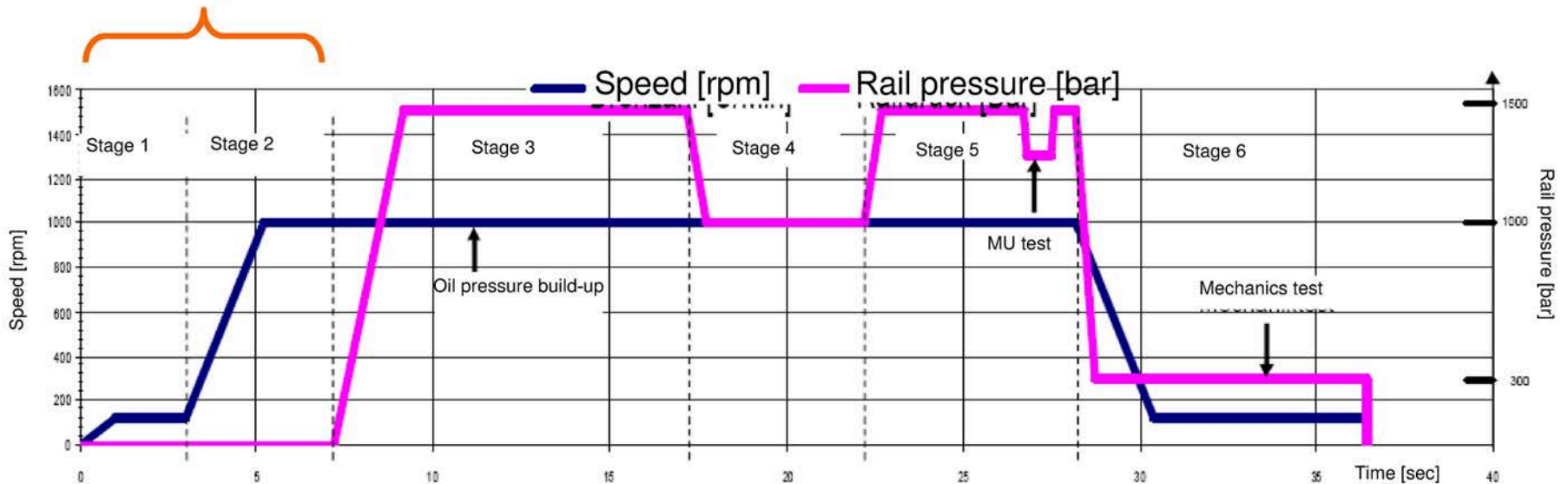
R4 CR TDI

High-pressure fuel pump seized, noisy

Detection of fault in the cold test curves

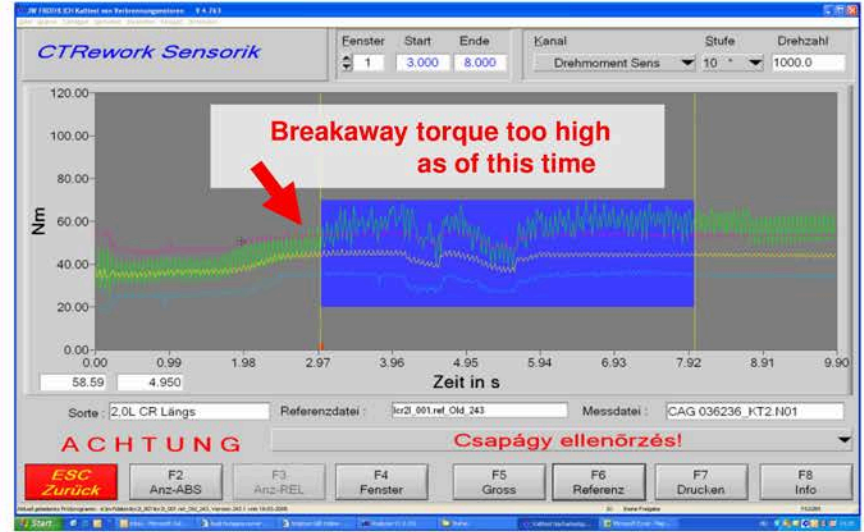
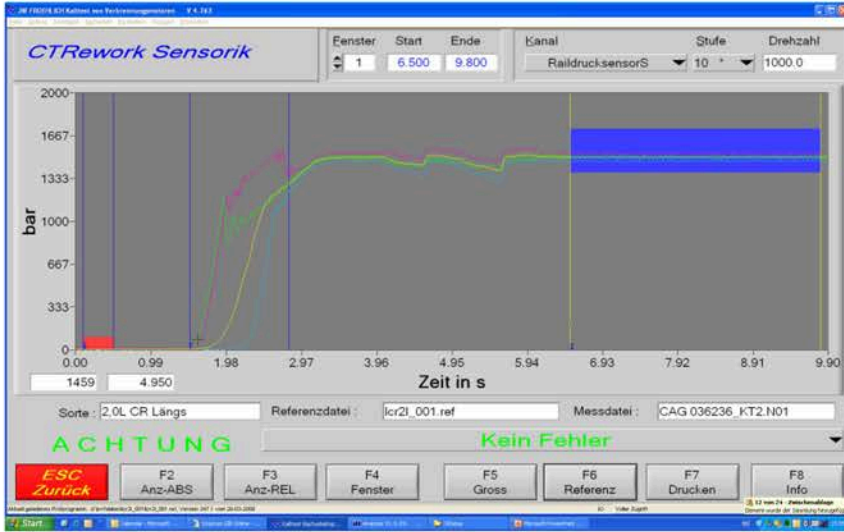
(e.g. on the engine Motor CAG 036236, but it manifests in the same manner in the other two failures)

No striking features

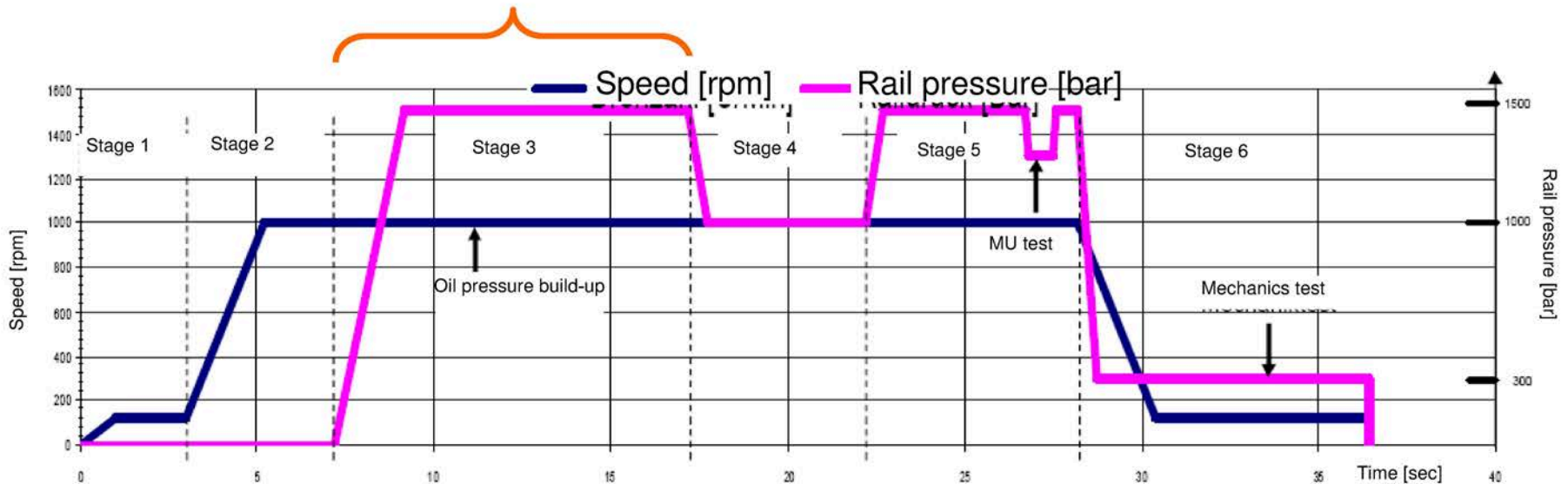


ACTUAL rail pressure

ACTUAL breakaway torque of the engine

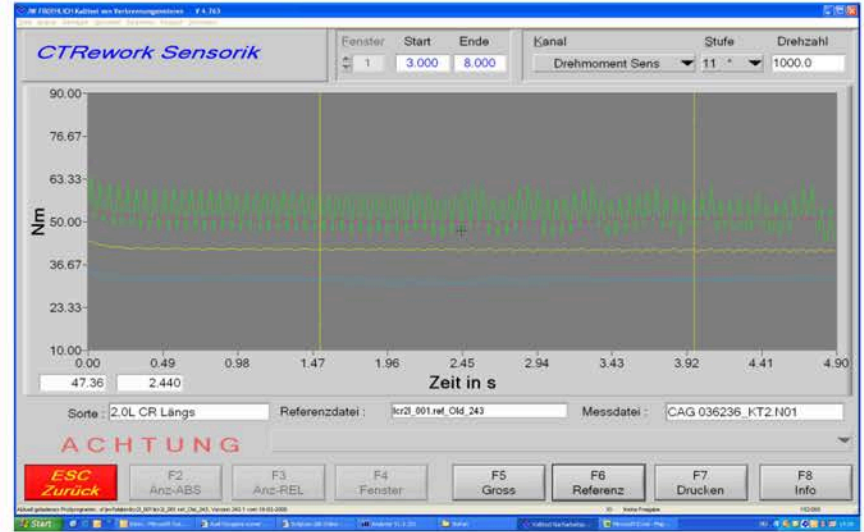
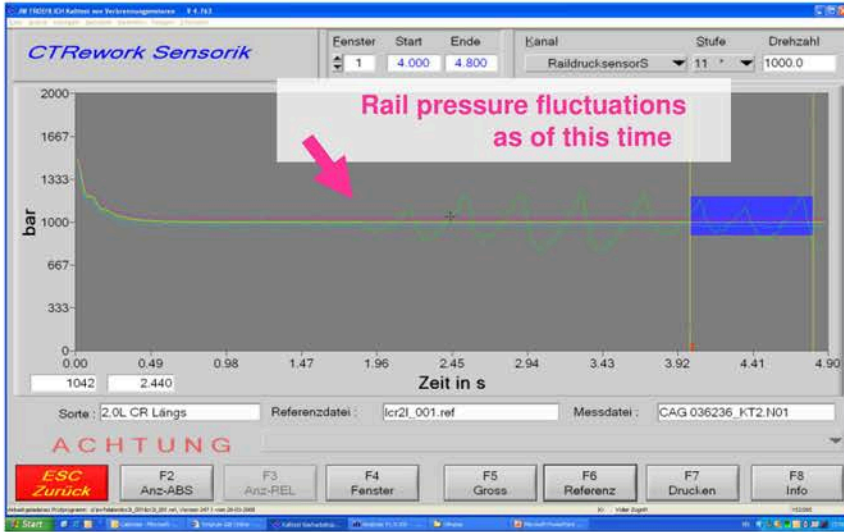


Rail pressure build-up and kept stable, but the torque curve has run up since approx. the second third to a level that is greater than the reference curves

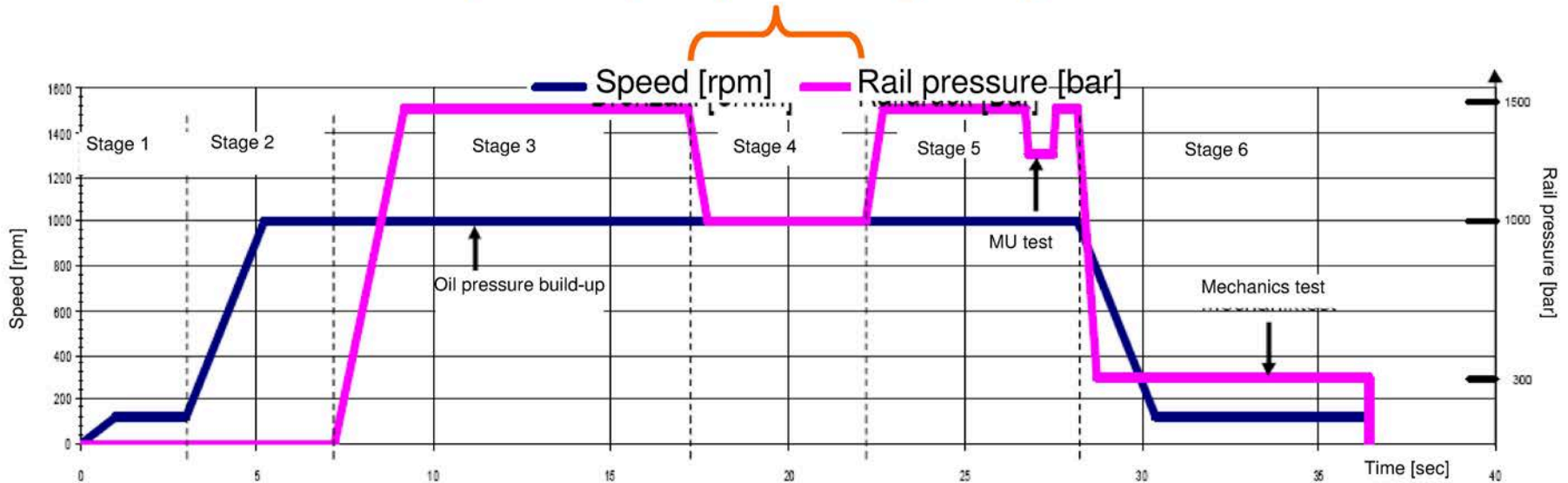


ACTUAL rail pressure

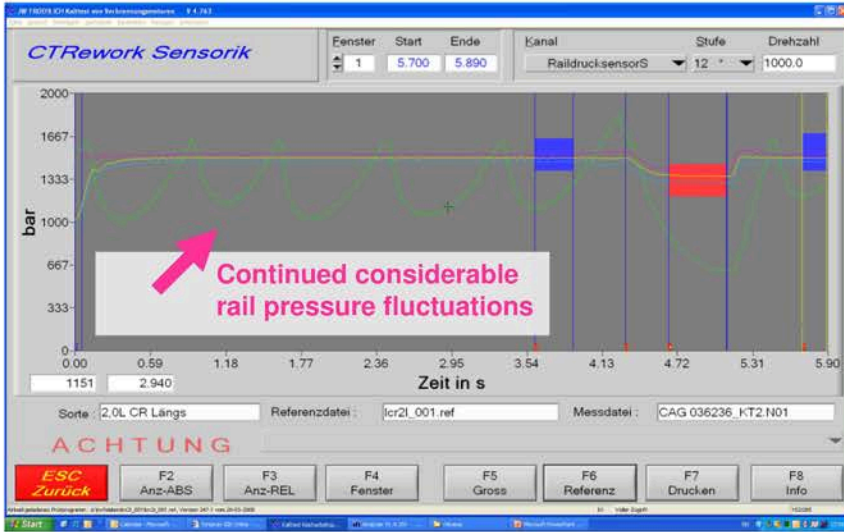
ACTUAL breakaway torque of the engine



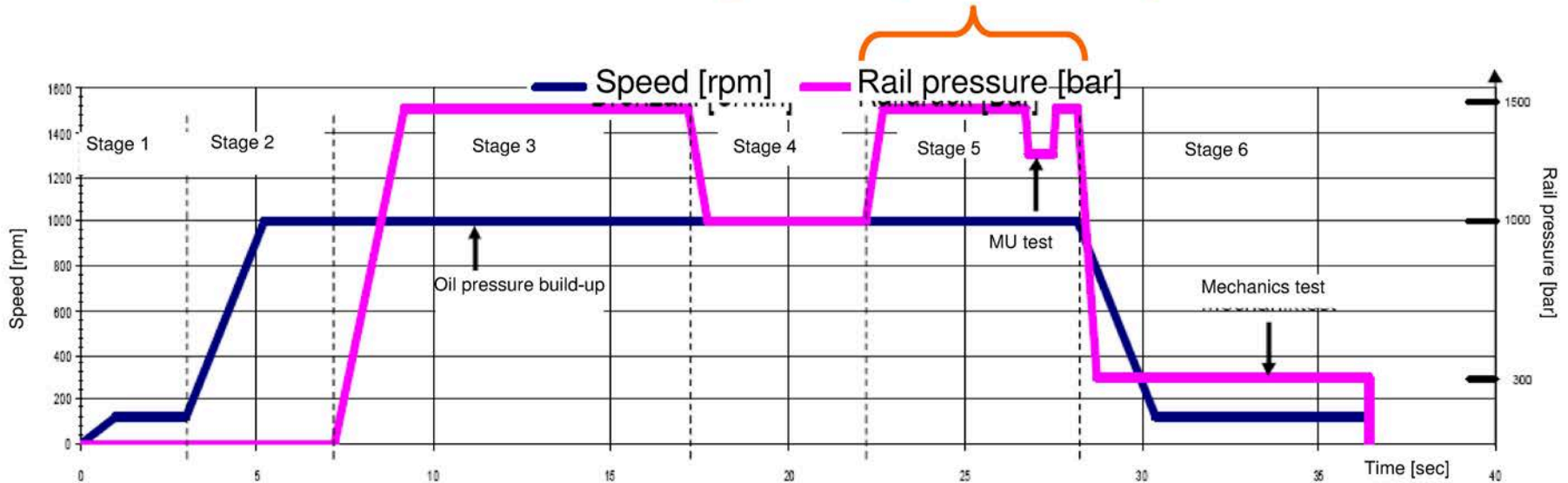
Within a few minutes, considerable rail pressure fluctuations occurred, breakaway torque remaining too high



ACTUAL rail pressure



Rail pressure in the further phases of the testing were always unstable, engine not OK



1) Test sequence VW R4, CP4.1

- The target test sequence for [REDACTED] presented by Audi at the end of March 2008 is basically in line with Bosch requirements
- The startup phase, 1,000 rpm without rail pressure, is to be reduced to the minimum possible time and is currently OK at < 10 seconds.

2) Further test bench procedure, recommendation from Audi/Bosch, 4/10/2008:

- joint measurement of at least one test bench "actual test process" by Bosch/Audi/Fröhlich (Wednesday, early shift), Audi/Fröhlich to provide the interface, Bosch the measurement technology (each party to be responsible for their own costs)
Target date 04.2008
- Development/Test Bench Technology in [REDACTED] will attend during measurement, so that it will be able to carry out these measurements itself on the other test benches
- VW Test Technology in [REDACTED] were to take part in the meeting

3) Exchange of information relating to CP4 requirements

- A local meeting will be held in [REDACTED] after the measurement results are available, involving Bosch Development, the plant and QM, target date 05.2008

4) Permanent saving of test bench test parameters

- Check to establish that the present offering in relation to documentation from Fröhlich meets requirements, R: Bosch, date 04.2008
- Costs are to be clarified between Fröhlich and Audi

5) Hot test

- If the schedule allows, the hot test is also to be measured on the Wednesday afternoon, following the same procedure as for the cold test as described above




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Deadline	Agenda: Topics	Agenda: Details	Responsible
1/31/2008	CP4 Q meeting/zero error meeting VW/Audi in Feuerbach		
1/31/2008	presentation of current Q situation 0km/field Audi VW		Non-responsive content removed
1/31/2008	Defective O-ring on MU	Summary of Audi complaints (including pump from [redacted] storage check)	
1/31/2008		Action plan	
1/31/2008		Current point cloud for MU testing point	
1/31/2008	CP4 drivetrain damage	Summary of complaints total/VW/Audi and diagnosis results	
1/31/2008		Measures	
1/31/2008		- C coating	
1/31/2008		- assembly, manufacture, test processes	
1/31/2008	Field failure Q7 CP4.2 crack in cylinder head		
1/31/2008	Intake/high-pressure valve leakage due to particles	Overview of complaints VW/Audi and diagnosis results	
1/31/2008		Measures	
1/31/2008		Overall situation of CP4 cleanliness:	
1/31/2008		- cleanliness concept FeP	
1/31/2008		- action plan incl. prospects for CP4 cleanliness	
1/31/2008		- Status of reworking of [redacted] pumps	
1/31/2008	Production tour - CP4		
1/31/2008	Complaints from leak test Chemnitz	Results of findings for the returns	
1/31/2008		Further action	
1/31/2008	Status of Jihlava release		
1/31/2008	Planning 1. PHA in Salzgitter and vehicle plants, 2. SOP tour [redacted]		
1/31/2008	Miscellaneous		
1/31/2008	Coordination of drafts for presentations of changes to customers.		
1/31/2008			
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2/27/2008	CP4 Q meeting VW Salzgitter		
2/27/2008	Discussion of OPL		
2/27/2008	- Status of 0km complaints		
2/27/2008	- Status of field complaints		
2/27/2008	- Status of PHA (if applicable, manufacture inspection - body assembly)	PHA OPL is distributed. Addition VW deadlines measures is in progress	
2/27/2008	- Status of internal failures	Not dealt with	
2/27/2008	- Status of other lines	Was presented in advance in separate round	
2/27/2008	- Miscella-		
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3/26/2008	CP4 Q meeting telcon netmeeting Braunschweig (Brunswick)		
3/26/2008	9:30 AM - 11:00 AM CP4 topics		
3/26/2008	Status of OPL from WaP (MU manufacture)		
3/26/2008	PHA: Status of OPL, next steps		
3/26/2008	Status of complaints "Particles in intake valve " (measures, current cases, other open points)		
3/26/2008	Drivetrain damage to US pump (status of investigations, current situation, implementation of measures)		
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OPL 2. Audi CP4 zero-fault meeting on 3/11/2008 with a focus on cleanliness									Changes
Ser. no.	Q meeting deadline	Discussion with	Topic	Component	Detail/construction element	OPL point / measure	Responsible	Date	Status
218	3/11/2008	Audi	Component	CP4	CP4 release	Draw up change notification for release of CP4.1 and CP4.1, [REDACTED] plant and to Audi	Non-responsive content removed	3/14/2008	t.b.d.
219	3/11/2008	Audi	Verification	CP4	Release of module 4. Sampling scope, number of parts	1. Complete sampling of CP4.1 with VW 2. In each case carry out cover sheet sampling for ... 755 AB and ...755 AG. 3. 3-5 CP4.1 or CP4.2 go to Győr for installation test and brake; 3. Clarification of feasibility QZ-ER for CP4.2 from module 4. , feedback to Mr Nilp		1. Clarification 2. 3/20/2008 3. Clarification 4. Clarification	t.b.d.
220	3/11/2008	Audi	Verification	CP4	Release of GP38 - production Bosch Hallein Planning	Clarification of orders for CP4.2 with GP38 to establish a 2DP date, Hallein plant with participation of Audi; Feedback possible 2DP deadlines to distributors		3/21/2008	t.b.d.
222	11.03.2008	Audi	Cleanliness	CP4	2DP GP38 Pneumatic air flushing of cylinder head	Audi wants presentation of trials with specification of place of introduction (map), particle type and size and identified effectiveness.		4/10/2008	t.b.d.
223	3/11/2008	Audi	Cleanliness	CP4	Pneumatic air flushing of cylinder head	The particle collection container for the respective modules/stations must be emptied and evaluated at set intervals (number of flushed heads). The number of particles, the particle size and materials must be documented.		4/10/2008	t.b.d.
224	3/11/2008	Audi	Cleanliness	CP4	Pneumatic air flushing of cylinder head	Audi question - can a damage to the intake valve on account of a pneumatic flushing be excluded?		4/10/2008	t.b.d.
225	3/11/2008	Audi	Component	CP4	Bruss oil seal	Update of the individual tracking slide with regard to the measures with the supplier, CP4.1 on shaft seal leaking		3/26/2008	t.b.d.
226	3/11/2008	Audi	Cleanliness	CP4	Establishing cleanliness progress EZ-CP4 high-pressure side	1. Carry out and evaluate a particle material analysis on the CP4 product high-pressure side on 25 CP4 2. Add ppm valuations to point cloud		4/10/2008	t.b.d.
227	3/11/2008	Audi	Cleanliness	CP4	MU action	1. Analysis of particles found during the visual inspection in the MU at [REDACTED] plant. 2. Correlation of the particles to processes [REDACTED] 3. Definition of corrective action at [REDACTED] plant		Immediate	t.b.d.
228	3/11/2008	Audi	Cleanliness	CP4	Clean assembly line Material containers	Creation of work instructions for the cleaning of material containers on CP4 assembly line.		4/10/2008	t.b.d.
229	3/11/2008	Audi	Cleanliness	CP4	Cleanliness workshop Housing/ Flange	Sending of matrix from cleanliness workshop to Audi, recording of implementation status		4/10/2008	t.b.d.
230	3/11/2008	Audi	Cleanliness	CP4	Cleanliness workshop Bore hole coverage	Clarification as to whether the bore hole coverage adhesive can be removed again without leaving any residue		4/10/2008	t.b.d.
231	3/11/2008	Audi	Cleanliness	CP4	Risk assessment for CH CU failures	VW requests risk assessment of number of possible further failures due to particles in the intake valve.		3/14/2008	t.b.d.
232	3/11/2008	Audi	Cleanliness	CP4	Cleanliness workshop on ECM for housing/ Flange	Audi wants a check to ascertain whether housing and flange couldn't also be deburred by means of ECM.		4/10/2008	t.b.d.
233	3/11/2008	Audi	Cleanliness	CP4	Cleanliness workshop on MU4 O-ring	Audi requests that cleanliness tests also be carried out on O-ring deliveries alongside series production		immediately	t.b.d.
234	3/11/2008	Audi	Cleanliness	CP4	Cleanliness workshop MU4-pot	Check as to whether brush process or other measures can be introduced to MU4 housing to reduce possible particles. Clarification with supplier.		03/21/2008	t.b.d.
235	3/11/2008	Audi	Cleanliness	CP4	100% Visual inspection of MU4	Introduction of a 100% visual inspection, scope analog to Feuerbach in the Waiblingen p		immediately	t.b.d.
236	3/11/2008	Audi	Cleanliness	CP4	Visual inspection of MU strainer	Visual inspection of a large number of MU strainers relating to plastic chips, present results in Feuerbach, if applicable introduce measures at suppliers		03/21/2008	t.b.d.
237	3/11/2008	Audi	Cleanliness	CP4	Audi request 250µm CP4-EZ	Activation of 250µm particle limit for timeframe WK12/2008 with execution of B-test test when limit value is exceeded. Info on results at next pump technical meeting on 03/26/2008 in NSU. Then a mutual decision regarding further steps.		WK 12/2008	t.b.d.
238	3/11/2008	Audi	test	CP4	Leak test [REDACTED] geometry calotte	Audi demands the preparation and presentation of the suppliers calotte roundness data measured since 02/18/2008		3/26/2008	t.b.d.
239	3/11/2008	Audi	Component	CP4	Assembly CP38 CP4.2	Audi requires that an interim report be drawn up as soon as possible regarding status of point 2 and point 4 of the OPL		3/21/2008	t.b.d.

The image shows a vertical strip of a document page, which is mostly obscured by a large 'CONFIDENTIAL' watermark. The visible portion of the page contains a table with multiple columns and rows of text. The text is very small and dense, typical of a technical specification or a detailed data sheet. The table appears to have several columns, possibly representing different parameters or categories, and many rows of data. The overall layout is highly structured and organized.

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Paynter Chart 0km and field failures CP4.1 for

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Production period		Jan 08	Feb 08	Mar 08	Apr 08	May 08	Jun 08	Jul 08	Aug 08	Sept 08	Oct 08	Nov 08	Dec 08	Jan 09	No of units 08/01-09/01	PPM
Supply Qty (..507)		0	13,168	17,648	0	0	0	0	0	0	0	0	0	0	30,816	
Drivetrain damage / turned tappet	0km														0	0
	Field														0	0
Particles IV	0km		1												1	32
	Field														0	0
Particles NRV	0km														0	0
	Field														0	0
MU O-ring damaged	0km														0	0
	Field														0	0
Leaky shaft seal	0km														0	0
	Field														0	0
pressure retaining test not OK, RB OK according to spec.	0km														0	0
	Field														0	0
OK according to specification	0km			2											2	65
	Field														0	0
Customer error (shaft seal folded)	0km														0	0
	Field														0	0
t.b.d.	0km														0	0
	Field														0	0
Total of complaints	0km	0	1	2	0	0	0	0	0	0	0	0	0	0	3	
	Field	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Total ppm-quota	ppm 0km	0	76	113	0	0	0	0	0	0	0	0	0	0		97
	ppm Field	0	0	0	0	0	0	0	0	0	0	0	0	0		0
Total number of acknowledged complaints	0km	0	1	0	0	0	0	0	0	0	0	0	0	0	1	
	Field	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
acknowledged ppm-quota	ppm 0km	0	76	0	0	0	0	0	0	0	0	0	0	0		32
	ppm Field	0	0	0	0	0	0	0	0	0	0	0	0	0		0

acknowledged complaints

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EA11003EN-01405[1]

Paynter Chart 0km and field failures CP4.1 for Non-responsive content removed

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Production period		Jan 08	Feb 08	Mar 08	Apr 08	May 08	Jun 08	Jul 08	Aug 08	Sept 08	Oct 08	Nov 08	Dec 08	Jan 09	No of units 08/01-09/01	PPM
Supply Qty (..507) (to Non-responsive content removed)		0	0	1,536	0	0	0	0	0	0	0	0	0	0	1,536	
Supply Qty to Non-responsive content removed		0	13,168	19,184	0	0	0	0	0	0	0	0	0	0	32,352	
Drivetrain damage / turned tappet	0km														0	0
	Field														0	0
Particles IV	0km														0	0
	Field														0	0
Particles NRV	0km														0	0
	Field														0	0
MU O-ring damaged	0km														0	0
	Field														0	0
MU RAS missing	0km														0	0
	Field														0	0
Crack on cylinder head	0km														0	0
	Field														0	0
OK according to specification	0km														0	0
	Field														0	0
Customer error (shaft seal folded)	0km														0	0
	Field														0	0
t.b.d.	0km														0	0
	Field														0	0
Total of complaints	0km	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Field	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Total ppm-quota	ppm 0km	0	0	0	0	0	0	0	0	0	0	0	0	0		0
	ppm Field	0	0	0	0	0	0	0	0	0	0	0	0	0		0
Total number of acknowledged complaints	0km	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	Field	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
acknowledged ppm-quota	ppm 0km	0	0	0	0	0	0	0	0	0	0	0	0	0		0
	ppm Field	0	0	0	0	0	0	0	0	0	0	0	0	0		0

acknowledged complaints

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EA11003EN-01405[2]

Paynter Chart 0km and field failures CP4.1 for all plants

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Production period		Jan 08	Feb 08	Mar 08	Apr 08	May 08	Jun 08	Jul 08	Aug 08	Sept 08	Oct 08	Nov 08	Dec 08	Jan 09	No of units 08/01-09/01	PPM
Supply Qty to		0	13,168	19,184	0	0	0	0	0	0	0	0	0	0	32,352	
Drivetrain damage / turned tappet	0km														0	0
	Field														0	0
Particles IV	0km		1												1	31
	Field														0	0
Particles NRV	0km														0	0
	Field														0	0
MU O-ring damaged	0km														0	0
	Field														0	0
Leaky shaft seal	0km														0	0
	Field														0	0
Crack on cylinder head	0km														0	0
	Field														0	0
pressure retaining test not OK, RB OK according to spec	0km														0	0
	Field														0	0
OK according to specification	0km			2											2	62
	Field														0	0
Customer error (shaft seal folded)	0km														0	0
	Field														0	0
t.b.d.	0km														0	0
	Field														0	0
Total of complaints	0km	0	1	2	0	0	0	0	0	0	0	0	0	0	3	
	Field	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Total ppm-quota	ppm 0km	-	76	104	0	0	0	0	0	0	0	0	0	0		93
	ppm Field	-	0	0	0	0	0	0	0	0	0	0	0	0		0
Total number of acknowledged complaints	0km	0	1	0	0	0	0	0	0	0	0	0	0	0	1	
	Field	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
acknowledged ppm-quota	ppm 0km	-	76	0	0	0	0	0	0	0	0	0	0	0		31
	ppm Field	-	0	0	0	0	0	0	0	0	0	0	0	0		0

acknowledged complaints

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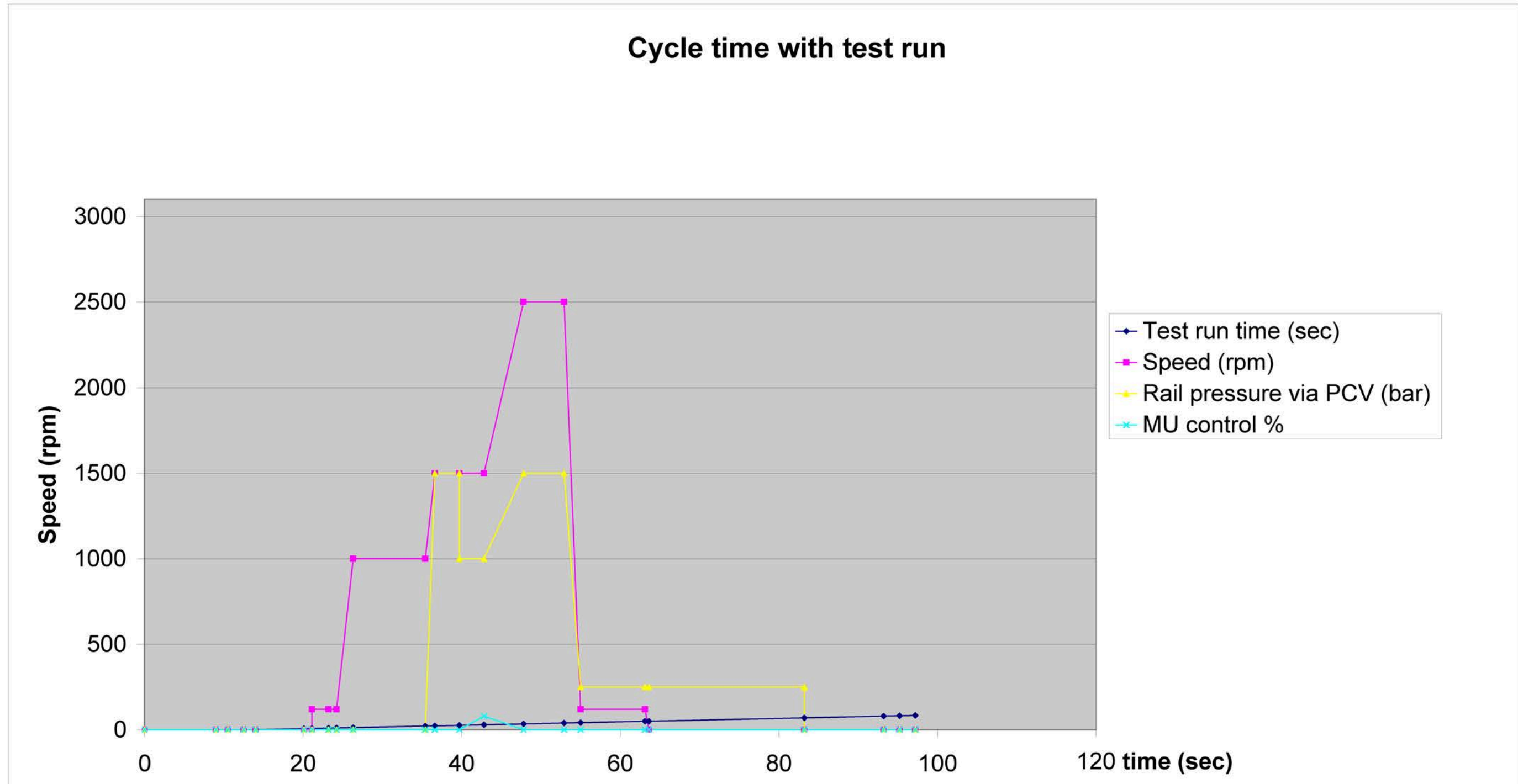
EA11003EN-01407[0]

Provisional test program for CR engine with Bosch HPP

Stage no.

	R0	9	0R	1.5	0R	11	12R	12	13R	13	21R	21	15R	15	16R	16	22R	22	23R	23	24R	24	25R	25	31R	31	32R	32	33R	33	41R	41	32R	32	41R	41	
Designation		Pallet change		Pallet lift		Provide drive carriages with MKP		E-contacting		Glow plugs Sensor test Regulating flaps Throttle valves glow plug test		Injector connection test		Breakaway Breakaway torque		Mechanics test (Control time check) (Additional function)		Oil pressure build-up		Rail pressure build-up		MU test		Turbocharger Mechanical vibration		Mechanics test		Blow out		Rail pressure drop test (additional integrated)		residue		E contacting and drive carriage back		Lower pallet	
Stage time / ramp time (sec)	0	9	1.5	0	2	0	1.5	0	0	6.1	0	1	0	2.1	0	1	2.1	9.1	1.2	3.1	0	3.1	5	5.1	2.1	8.1	0	0	0.5	19.6	0	10	0	2	0	2	
Cycle time (sec)	0	9	10.5	10.5	12.5	12.5	14	14	14	20.1	20.1	21.1	21.1	23.2	23.2	24.2	26.3	35.4	36.6	39.7	39.7	42.8	47.8	52.9	55	63.1	63.1	63.1	63.6	83.2	83.2	93.2	93.2	93.2	95.2	95.2	97.2
Test run time (sec)	0	0	0	0	0	0	0	0	0	6.1	6.1	7.1	7.1	9.2	9.2	10.2	12.3	21.4	22.6	25.7	25.7	28.8	33.8	38.9	41	49.1	49.1	49.1	49.6	69.2	69.2	79.2	79.2	81.2	81.2	83.2	
Speed (rpm)	0	0	0	0	0	0	0	0	0	0	0	0	120	120	120	120	1,000	1,000	1,500	1,500	1,500	1,500	2,500	2,500	120	120	120	120	0	0	0	0	0	0	0	0	
Rail pressure via PCV (bar)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1,500	1,500	1,000	1,000	1,500	1,500	250	250	250	250	250	250	0	0	0	0	0	0	
MU control %	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	80	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

Cycle time with test run



Cleanliness CP4

Increase in permissible residual dirt values

- ➔ Audi is insisting on an increase in the residual dirt values permitted for CP4
 - No particles > 250 µm permitted
 - CP4 residual dirt values coordinated with the injector requirements
- ➔ Background:
 - Pump failures due to particles with a size in the region of 300 µm
Failure mechanism: Intake valve and non return valve malfunction in the cylinder head caused by particles
 - Current plant limit for the product:
 - High pressure: 4 particles permitted in the category 200-400µm
 - Low pressure 8 particles permitted in the category 200-400µm
- ➔ Current particle situation
 - The cleanliness values for the product comply with the current plant limits.
 - Particle category 200-400 µm:
 - High pressure* Mean value = 0.68 particles (25 measurements CP4.1 VW)
 - Low pressure Mean value = 1.68 particles (25 measurements CP4.1 VW)

High pressure: Measurement of the particles flushed by the high pressure – Hydraulic flow: Flow into housing ´ MU – inlet hole between the housing and the CH – inlet hole between the CH and the IV space - HP



Cleanliness CP4

Possible actions when limit value exceeded

- Repeated function test/flushing – previous investigations did not show any improvement in the residual dirt values for products flushed twice
- Disassembly of products – great risk of damage and occurrence of particles
- **No known effective procedure for flushing finished products**



Cleanliness CP4

Strategy and objectives

- Cleanliness must be ensured at part and assembly level.
 - Housing/flange workshop
 - Cylinder head
 - Pneumatic flushing (current test stage)
 - ECM deburring
- Previously, particle-based failures were solely due to particles in the IV and NRV areas of the cylinder head.
- Consequently, more stringent cleanliness requirements are necessary, especially in relation to the fuel-carrying areas from the MU to the non-return valve.
- The main objective of such intensive activities to improve cleanliness is to prevent the occurrence of small particles in the aforementioned areas.
- Particle extraction from components also includes the complete outer contour. A separate evaluation is not possible for the relevant fuel-carrying areas.
- The objective is, as far as possible, particle-free production of the aforementioned area (MU - NRV) in order to prevent the occurrence of pump failures. Monitoring through the use of particle measurements with an upper limit is not possible at present.



Cleanliness CP4

Simulation with a higher upper limit for residual dirt

- ➔ Over a production period of 2 weeks, the upper limit of “no particles > 200 µm” was reliably simulated in high pressure.
- ➔ Result
 - The upper limit of “no particles > 200 µm” was exceeded three times.
 - The B samples taken subsequently (2 pumps in each case) were within the increased specification.
 - No noticeable development of the “internal particle-based failures”.
 - All in all, continuation of the positive trend in the development of residual dirt values
- ➔ Summary
 - Compliance with the upper limit of “no particles > 200 µm” cannot be ensured at present.
 - At present, the residual dirt results for particles > 200 µm does not suggest a deviation in the processes.
 - There is no recognizable correlation between the individual residual dirt results and pump failures.



Cleanliness CP4

Further action

- Continuation of cleanliness work with the following objectives:
 - No external and internal particle-based failures
 - Further improvement of the residual dirt level, ensured compliance with the upper limit of “no particles > 200 µm” in high pressure
 - Focus
 - Housing
 - Flange
 - Cylinder head
 - MU
- Test program involving 25 pumps to determine the origin of the particles in each particle category (similar to the investigation conducted in 2006) – question: What particle sources exist following implementation of the improvements?
D: M05/2008
- Decision on how to proceed when particles > 200 µm occur in the high-pressure area
 - Amend the action plan – Problem: No effective procedure for finished products when the limit value is exceeded.
 - Analysis of all particles > 200 µm – Problem: Handling of small particles



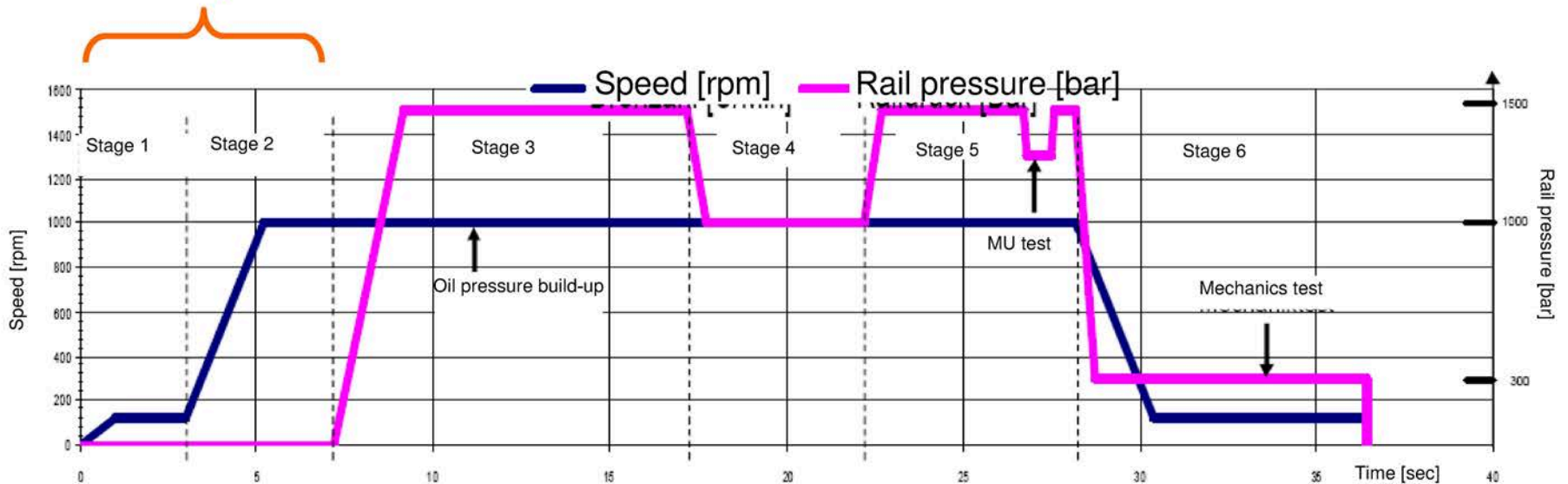
R4 CR TDI

High-pressure fuel pump seized, noisy

Detection of fault in the cold test curves

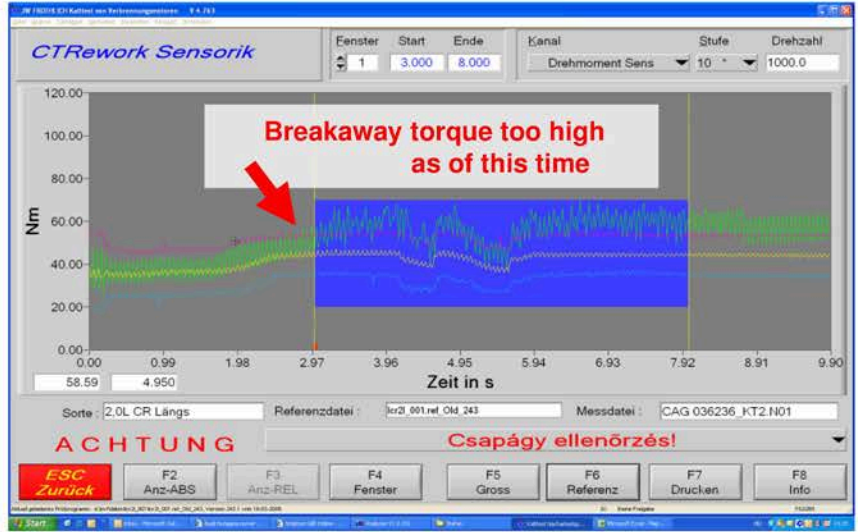
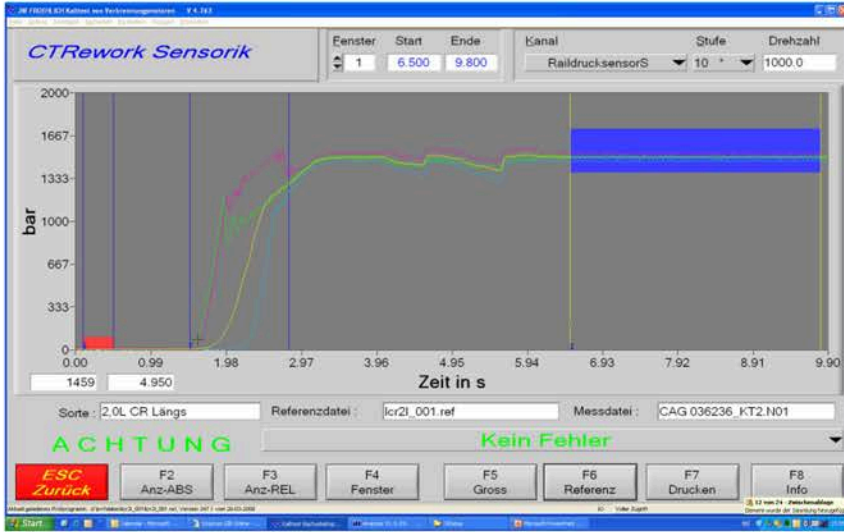
(e.g. on the engine Motor CAG 036236, but it manifests in the same manner in the other two failures)

No striking features

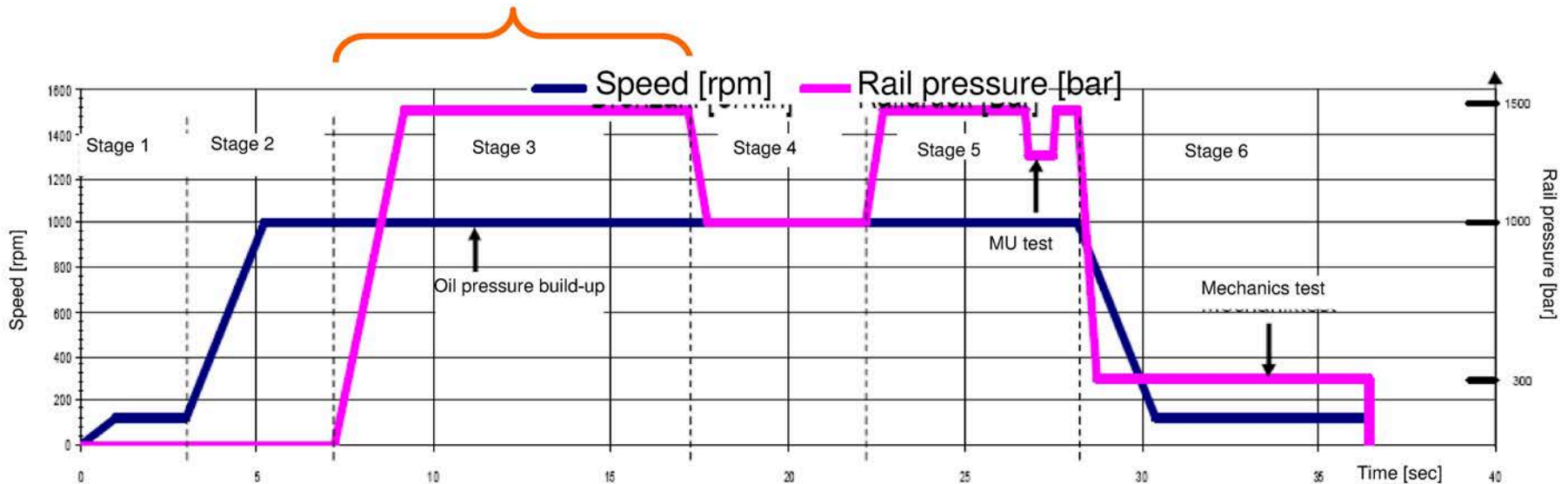


ACTUAL rail pressure

ACTUAL breakaway torque of the engine

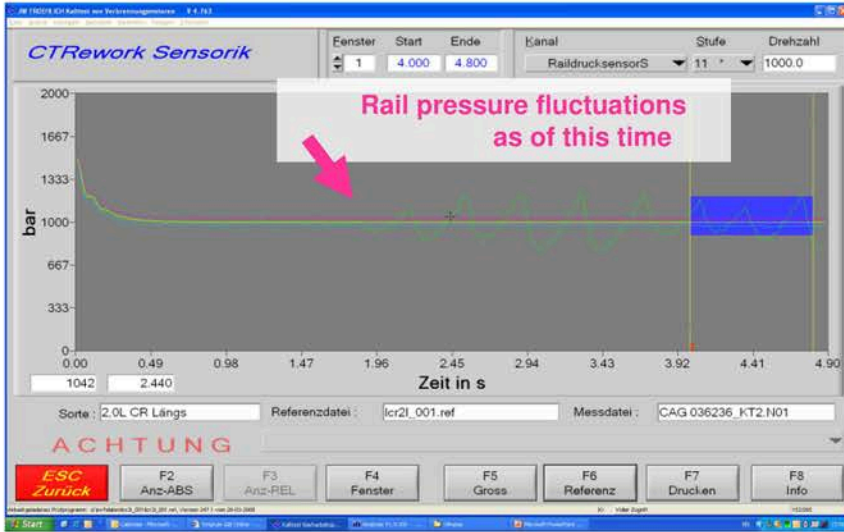


Rail pressure build-up and kept stable, but the torque curve has run up since approx. the second third to a level that is greater than the reference curves

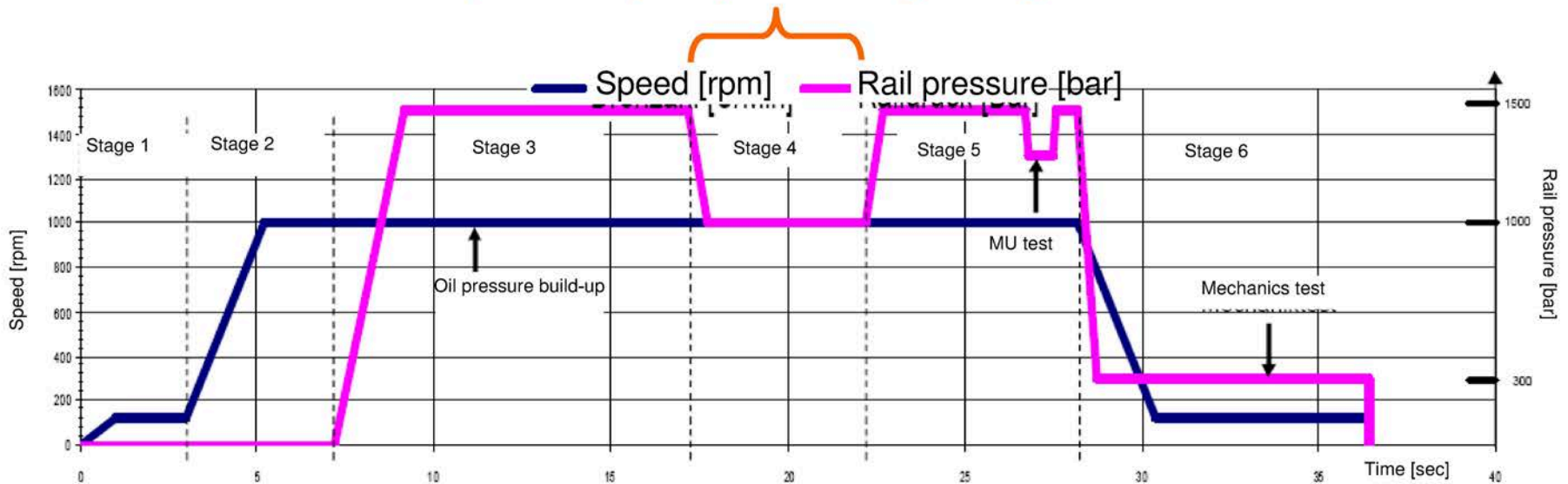


ACTUAL rail pressure

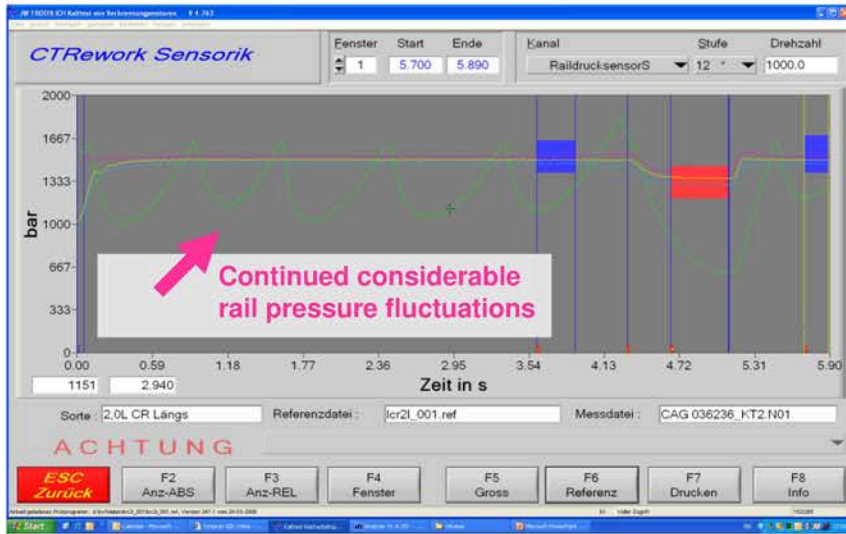
ACTUAL breakaway torque of the engine



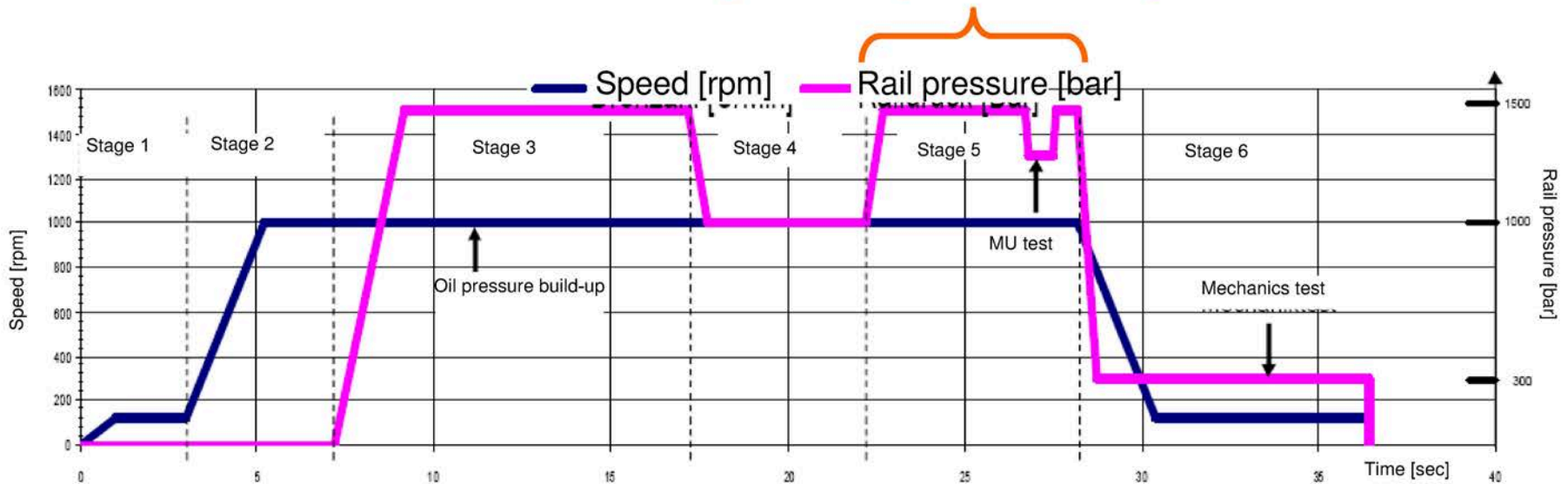
Within a few minutes, considerable rail pressure fluctuations occurred, breakaway torque remaining too high



ACTUAL rail pressure



Rail pressure in the further phases of the testing were always unstable, engine not OK



From: Non-responsive content removed

To:

CC:

Date: 7/19/2007 6:27:25 PM

Subject: Re: Minutes from OEM meeting on CP4.x turned tappet from 7/13/2007 - Item 4
Inspection oil quality CP4

Dear Non-responsive content removed

Regarding your question relating to the HFRR value, please consider the following:

- Inspection oil contains anti scuff additives. The effect is specified and must be proven by the supplier in a FBBD (Four Ball Bearing) test.
- HFRR is a standardized test used to determine wear (ball on plate). In other words, it is a measure of the amount of wear. The test runs in the mixed friction area.
- It is possible to measure wear and friction in the HFRR test. However, a correlation of these parameters cannot be proven. This is partly due to the wide dispersion of the HFRR results in the test per se and also to the fact that different wear mechanisms (tribochemical wear/abrasive wear/adhesive wear) are involved here.
- This means that the HFRR value is not a suitable parameter with which to assess friction behavior.
- The HFRR value is relatively high for the inspection oil used in order to ensure a certain running in (abrasion/ smoothing of the surface tips of the parts).

Friction is affected by the following parameters:

- For the hydrodynamic element of friction: f (viscosity of the inspection oil) --> viscosity is specified and is tested (per delivery batch)
- Impurities in the inspection oil:
 1. Caused by particles: --> inspection oil is filtered or tested with regard to contamination in the circuit (on a weekly basis).
 2. Chemicals in the inspection oil: --> The chemical composition is tested using the FTIR (Fourier Transform Infrared Spectrometry) spectrum (per delivery batch)
- In our opinion therefore, the key parameters that influence the friction properties of the inspection oil are monitored.

Best regards / Mit freundlichen Grüßen / Cordiali saluti

Non-responsive content removed

From: Non-responsive content removed
Sent: Thursday, July 19, 2007 12:54 PM
To: Non-responsive content removed
Subject: Re: Minutes from OEM meeting on CP4.x turned tappet from 7/13/2007 - Item 4 Inspection oil quality CP4

As discussed, please reply.

Best regards / Mit freundlichen Grüßen

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From: Non-responsive content removed
Sent: Thursday, July 19, 2007 8:08 AM
To: Non-responsive content removed
Cc: Non-responsive content removed
Subject: ANS: Minutes from OEM meeting on CP4.x turned tappet from 7/13/2007 - Item 4 Inspection oil quality CP4

Hello

Why is the lubrication not being monitored? I thought that was the whole idea?

-----Original message-----

From: Non-responsive content removed
Sent: Wednesday, July 18, 2007 6:26 PM

Non-responsive content removed

Subject: Minutes from OEM meeting on CP4.x turned tappet from 7/13/2007 - Item 4 Inspection oil quality CP4

Hello,

In the meeting on 7/13/2007, a presentation on the monitoring of the inspection oil quality at RB was requested.

1) Inspection oil used: Shell V-Oil 1404 (trade name)

2) The following parameters are monitored: appearance, viscosity, color, density. These are verified by the supplier by means of a certificate.

In the goods receiving inspection at RB, these parameters and the water content and the FTIR spectrum are determined.

Attached are the results of the goods receiving inspection in 2007

<<V1404_AnfrageCP4_VW.pdf>>

Best regards / Mit freundlichen Grüßen

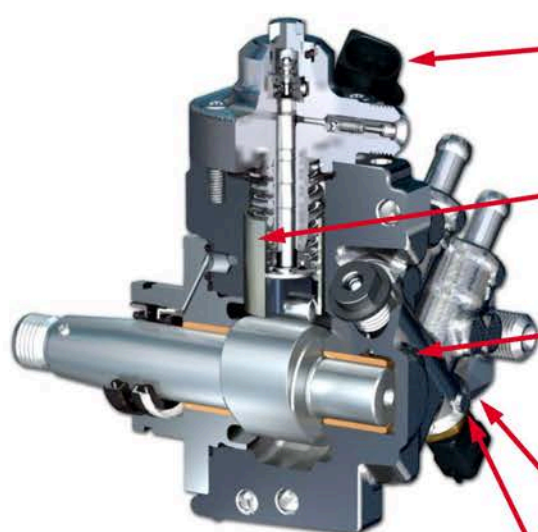
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Domicile: Stuttgart, Court of Registry: Local District Court Stuttgart Commercial Register No. 14000
Chairman of the Supervisory Board: Hermann Scholl; Management: Franz Fehrenbach, Siegfried Dais;
Bernd Bohr, Wolfgang Chur, Rudolf Colm, Gerhard Kümmel, Wolfgang Malchow, Peter Marks;
Volkmar Denner, Peter Tyroller

List of Design Differences of W36 to Production Pumps

W36: List of Design Differences of W36 to Current Production Pumps



Metering unit	new (axial exit direction of metering unit [electrical] connector)
Tappet	optimized tappet assembly, C2.1 on end of roller
Housing	new housing (metering unit rotated, through holes, engine-side radial shaft seal ring)
Cylinder head left	new cylinder head, due to changed exit direction (on side);
Nameplate	new assembly setup (TSS position on left)

Diesel Systems



Replication operation with non-OK rollers

Topic

Confirmation of failure hypothesis for "export countries"

"Drivetrain damage due to combination of stiff cam roller (in this instance, fusing on the cam roller) in combination with country-specific peculiarities (in this instance, fuel)" **through a replication test**

Implementation (0445010613 instead of 0445010611 due to C-coated piston to prevent piston seizure) CP4.2 W19 BIN5 with melt on the cam rollers (waste from straightedge test; subsequent frictional value test OK) set up and operated with poorly lubricating fuel GDK650 (HFRR 650 µm).

Result

Drivetrain damage after 35 hours of operation

Note

The **drivetrain** task force carried out several similar tests with EN590, although only one case of drivetrain damage occurred.

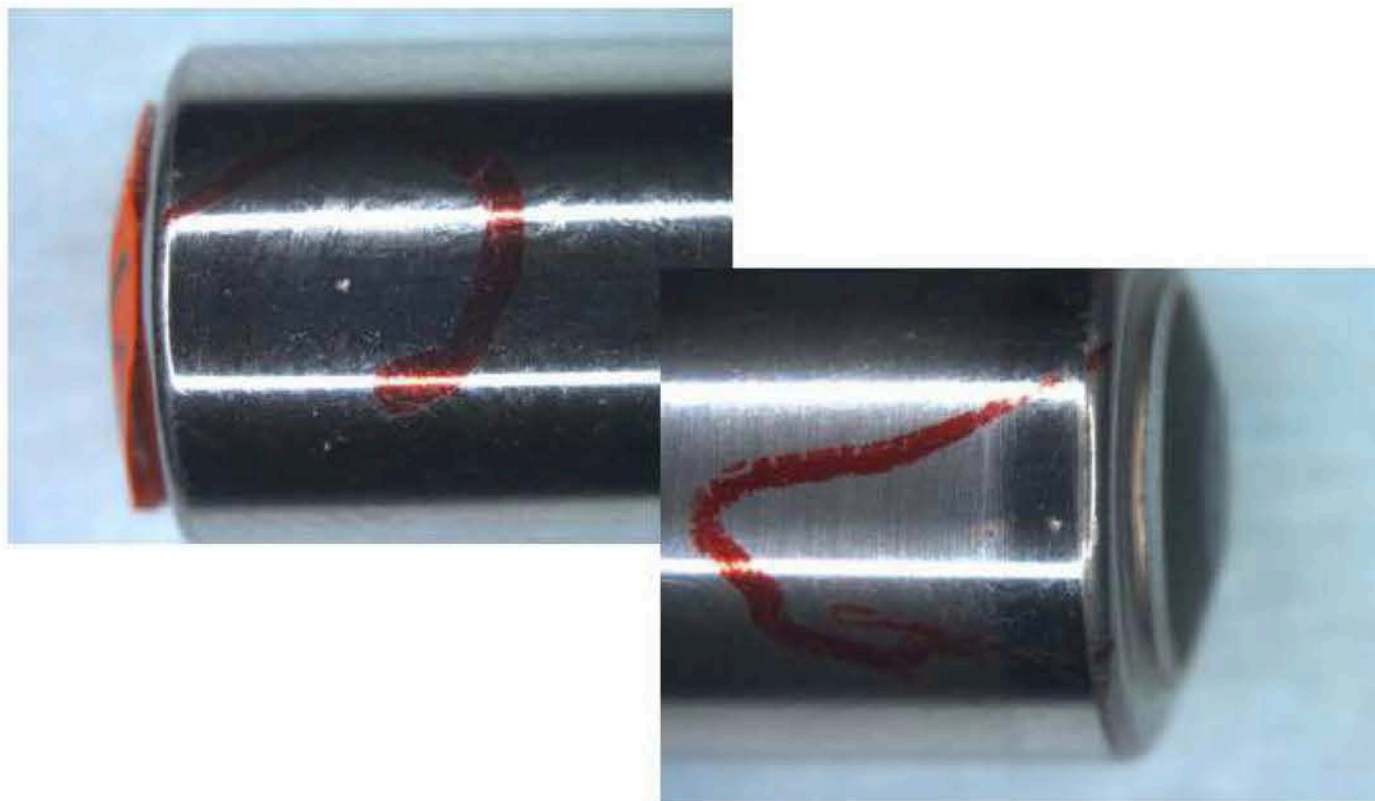
Conclusion

Result confirms the **failure hypothesis**. Pumps manufactured prior to the introduction of the straight-edge test (7.04.2008) can--in combination with poor lubricity--experience failures.



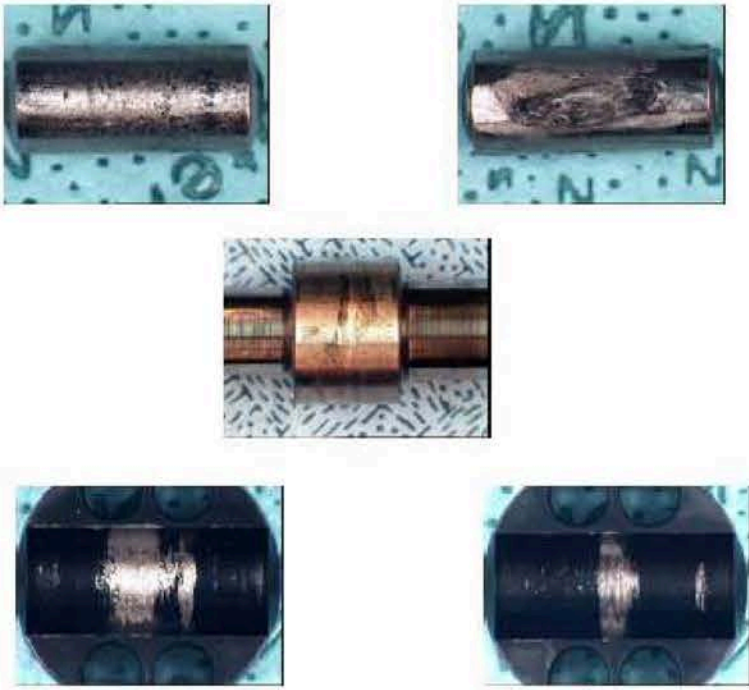
Provocative operation with non-OK rollers

Photos of roller before continuous test



Provocative operation with non-OK rollers

Photos after continuous test



3

Diesel systems

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Task Force Summary

→ Status of new information since last update on 1/20/2010
(changes in blue):

Task force work concentrates on the following key areas:

1. Analysis of field parts/fuel samples, good pumps, filtering, reserve samples from production.
2. Analysis of the differences between CP4.1 and CP4.2 in the case of critical fuels.
3. Reappear test of the differences between CP4.1 and CP4.2 and confirmation of the damage mechanisms.
4. Introduction of anti-wear package 1 (C2 coating, reduced play on roller/roller support, 100% avoidance of fusing and metal splashes)
Implementation decision by RB/AUDI after positive completion of validation
Start of week 9/2010
5. Definition of anti-wear package 2 (RoW action) after completion of points 1 and 2.
This needs to be checked and validated with boundary fuel (already defined with AUDI).



1. Summary of analysis

- ➔ Other analyses in the fuel samples from local factions in [redacted] support the results from the fuel survey in [redacted] and the analyses from the problematic pumps. The mineral oil industry in [redacted] confirms in principle the poor fuel results (water, aged biofuel).

The analyses in relation to pumps, fuel samples and particles/ residues from local actions are complete. In some cases oxidation stability (aging) was outside the standard; in addition, particles of plastic and traces of algae were found in some tanks and pumps. One of the special features in [redacted] is the use of the **Tunap 183** additive to clean the fuel injection system in service. **According to the manufacturers, Tunap 183 is supposed to improve lubrication (HFRR value). Evaluation of the information by the Bosch and Audi laboratories.** Verification of influence through tests run by Bosch.

Tests conclusion in week 8/2010 .



1. Summary of analysis

→ Return of the requested 40 good pumps from [redacted] and 20 good pumps from [redacted]

First returns announced from [redacted] (5 pumps) and [redacted] (4 pumps). 4 pumps received from [redacted] on 1/25/2010. Pumps from [redacted] still outstanding.

1 in 4 pumps has signs of previous damage to the roller/ camshaft at TDC, same results as with 1 pump from returns from local team action.

Similar damage was found on an as yet still working V12-TDI pump from

[redacted] (sister pump of drivetrain damage after 1,600 km), where the roller was at a significant slope on the cam and there were signs of corrosion on the roller. These signs of damage indicate sluggish rollers in conjunction with poor quality fuel.

Further detailed analysis required, completion by 2/3/2010.

1. Summary of analysis

Information gathered to date supports the failure mechanisms presented in the last reports.

1. Tribochemical wear
2. Deposit / coatings from algae and oxidation products and therefore significant deterioration in friction coefficient.
3. Corrosion on the surface of cams and roller

Analysis of reference samples:

The analysis of the reference samples from the conspicuous production period (up to May 2008) indicates nothing unusual in relation to drawing-related features. Other detailed analyses (roller surface texture, ripple in roller support, roundness with Fourier analysis, local adhesion of coating with temperature analysis) are complete.

Analyses to date confirm the production status at the time, with spatter of metal on the roller support; also the surfaces of the C coatings indicate abnormalities that are still under investigation. Will be concluded on a further 25 parts by 2/3/2010.

2. Summary of differences between CP4.1 and CP4.2

- The MIS12 (MY08) failure quota of the CP4.2 is up to 10 times higher in [redacted] than the CP4.1.
- The MIS 12 (MY08) of CP4.2 is approximately 10 times higher [redacted] than in [redacted]
- The MIS 12 (MY08) of CP4.2 is approximately 2 times higher [redacted] than in MY09.

Conclusions:

- In addition to the influence of the fuel quality, there must also be design and application-specific differences between CP4.1 and CP4.2.
- Concentration of further work on an analysis of the differences between CP4.1 and CP4.2 (see slide 6 and 7).

2. Summary of differences between CP4.1 and CP4.2

Further action:

Implement examinations of

→ the flow and pressure conditions in the tappet chamber of both pump types.

Initial investigations of flow conditions indicate now differences.

→ the influence of the low pressure circuit.

The plan is to reproduce the entire low pressure circuit of 4-/6-cyl. engines on the test bench in order to test individual influences, such as water ingress from the tank to the pump. D. 2/24/2010

→ the tappet position when stopping (position of roller with cam at TDC).

Initial analysis showed that the tappet position in 6-cylinder engines in approx. 10% of cases can be just before or at TDC after the motor stops. When the engine is restarted, the roller must start from the instable position at TDC. This could cause the tappet to turn.

In the case of 4-cylinder engines this critical position does not exist, however this is to be confirmed again by VW/AUDI by means of measurement data on the vehicle.

T. 2/3/2010



3. Reappear test for differences between CP4.1 and CP4.2

Further action:

Validation with EN590 shows a turned tappet on the cam shaft of less than one degree.

Further investigations are required on the test bench in relation to the startup of the roller at TDC with critical fuel (Arctic Diesel). D. 2/3/2010

Measurements need to be carried out using kerosene on the complete engine at AUDI in [redacted] in week 5/2010.



4. Summary of anti-wear package 1

→ Further action:

Measures to increase robustness (roller surface texture, roller support and play) are defined and their effectiveness will be verified with the same test parameters. A test schedule has been drawn up, **partial results** will be available by the **end of week 8/2010**. The latest information shows that the roughness of the roller support is the decisive parameter in increasing robustness. According to a simulation, narrowing tolerance R_v from 1.3 to **0.8** μm increases the safety factor of the friction coefficient by **approx. 50%**.

Investigations into the creation of roughness in the roller support shows that roughness is primarily determined by the C3 coating and not the processing.

4. Summary of anti-wear package 1

Roughness measurements on roller supports with C2 coating show a clear improvement in roughness.

Changes in process technology from C3 sputter coating to C2 plasma coating on the roller support and roller enables quality to be improved by avoiding 100% of fusing and metal splashes.

That is why it is necessary to switch to C2 coating.

The basic test with EN590 and BDF 570 for C2 coating is complete.

The “rest of the world” trials are still outstanding.

Further action:

→ In case of positive validation of the anti-wear package by the end of WK 8/2010 with limit samples and critical fuels (Kerosene, Arctic Diesel, WCF, FCF), a series introduction was decided for V6-TDI EU5 + BIN5 series and W36 pumps.

Production readiness is assured from WK 9/2010 onwards.

This will confirm the schedule requirements from Audi from the last task force.



4. Summary of anti-wear package 1

- A further objective is to enable the anti-wear package on a provisional basis in customer service worldwide.
After the anti-wear package is installed in series, the first 400 pumps will be provided for customer service.



Task Force Summary

- Status of new insights since last update on 2/3/2010
(changes in blue):

Task force work concentrates on the following key areas:

1. Analysis of field parts/fuel samples, good pumps, filtering, reserve samples from production.
2. Analysis of the differences between CP4.1 and CP4.2 with critical fuels.
3. Reappear test of the differences between CP4.1 and CP4.2 and confirmation of the damage mechanisms.
4. Introduction of anti-wear package 1 (C2 coating, reduced play between roller/roller support, 100% avoidance of fusing and metal spatters), decision for implementation through RB/AUDI after positive conclusion of validation early WK9/2010.
5. Definition of anti-wear package 2 (RoW action) after completion of points 1 and 2. This needs to be checked and validated with boundary fuel (already defined with AUDI).

1. Summary of analysis

- **Analysis of field pumps and fuel samples from** Non-responsive content removed
- FAME deposits **11 of 54 pumps**
- Corrosion indicators, evidence of water **45 of 54 pumps**
- Free water in fuel sample **4 of 24 samples**
- Cellulose residue, algae, glycerin **9 of 24 pumps**
- Heavy wear of shaft seal **17 of 17 pumps**
- OK pumps with preliminary damage Non-responsive content removed **6 of 13 pumps**

1. Summary of analysis

→ Return of the requested 40 good pumps from [REDACTED] and 20 good pumps from [REDACTED]

Non-responsive content removed

First returns received from [REDACTED] (6 pumps) and [REDACTED] (13 pumps).

6 of 13 pumps have preliminary damage and show braking flats with transfer of material to roller and camshaft.

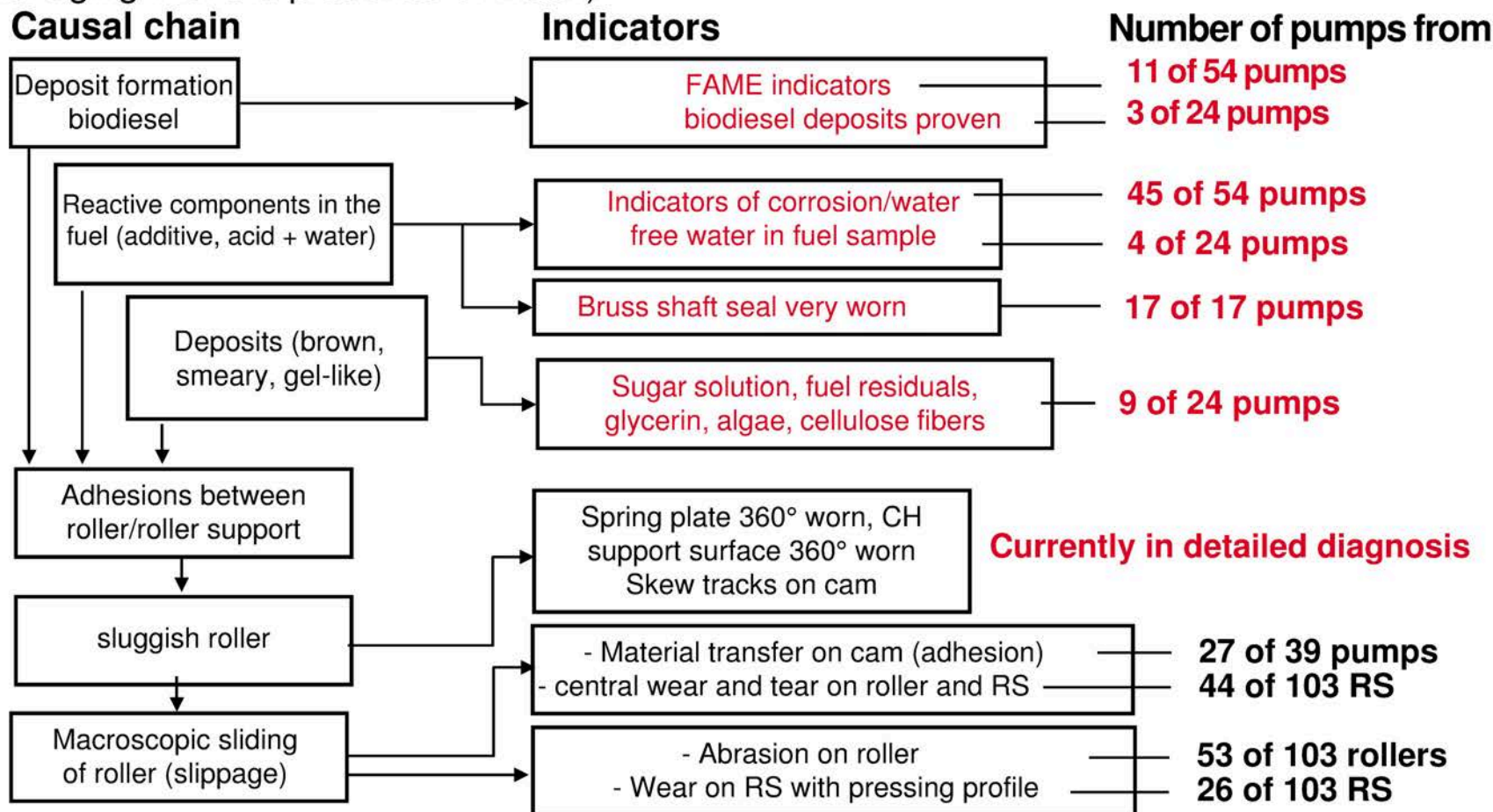
Damage symptoms indicate a seized roller during pump startup with poor fuel.

The cause of the roller standstill is the clogging in the roller support through deposits of reaction products from the aged biofuel.

Reappear tests with poor fuel confirm the seized roller and similar damage symptoms.

1. Summary of analysis

(fuel aging with the presence of water)



2. Summary of differences between CP4.1 and CP4.2

- The MIS12 (MY08) failure quota of the CP4.2 is up to 10 times higher in Non-responsive content removed than the CP4.1.
- The MIS 12 (MY08) of CP4.2 is approximately 10 times higher in Non-responsive content removed than in Non-responsive content removed
- The MIS 12 (MY08) of CP4.2 is approximately 2 times higher in Non-responsive content removed than in MY09.

Conclusions:

- In addition to the influence of the fuel quality, there must also be design and application-specific differences between CP4.1 and CP4.2.

A stationary roller with potential to transfer material on the camshaft can only be generated under load (pressure) and with low-quality fuel.

Based on the new hypothesis of the stationary roller during the start-up with low-quality fuel, the additional tests focus on the differences in the pressure build-up/pressure changes between CP4.1 and CP4.2. To this end, further measurements are performed at the engine. Additional measurements will be carried out on the engine for this purpose. [Date coordination with VW underway.](#)

4. Summary of anti-wear package 1

→ Further action:

Measures to increase robustness (roller surface texture, roller support and play) are defined and their effectiveness will be verified with the same test parameters. A test schedule has been drawn up, partial results will be available by the end of week 8/2010. The latest information shows that the roughness of the roller support is the decisive parameter in increasing robustness.

According to a simulation, narrowing tolerance R_v from 1.3 to 0.8 μm increases the safety factor of the frictional coefficient by approx. 50%.

Investigations into the creation of roughness in the roller support shows that roughness is primarily determined by the C3 coating and not the processing.



4. Summary of anti-wear package 1

Roughness measurements on roller supports with C2 coating show a clear improvement in roughness.

Changes in process technology from C3 sputter coating to C2 plasma coating on the roller support and roller enables quality to be improved by avoiding 100% of melts and metal spatter. That is why it is necessary to switch to C2 coating.

The basic test with EN590 and BDF 570 for C2 coating is complete. The “rest of the world” trials are still outstanding.

Friction coefficient investigations (Stribeck curves) with C2 coating and close play between the roller and roller support indicate a positive shift toward lower frictional coefficients with poor quality fuels (Arctic diesel, kerosene), (see slides 8 and 9).

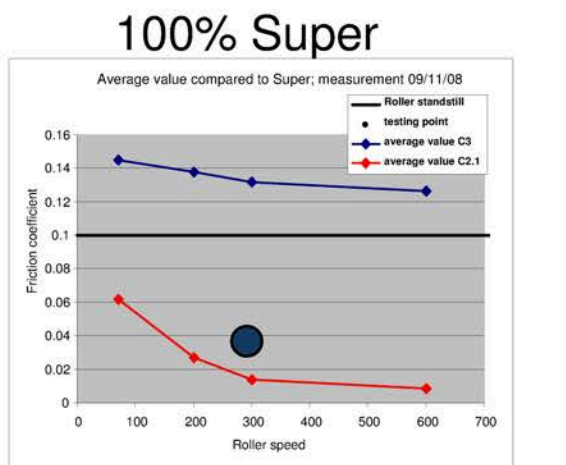
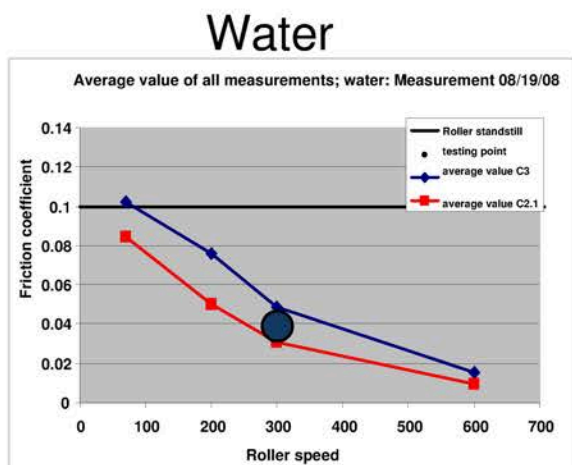
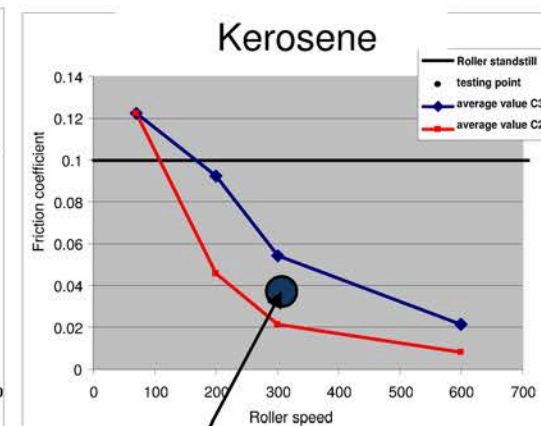
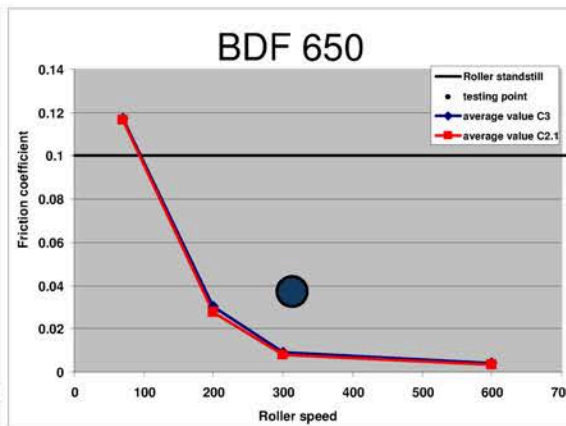
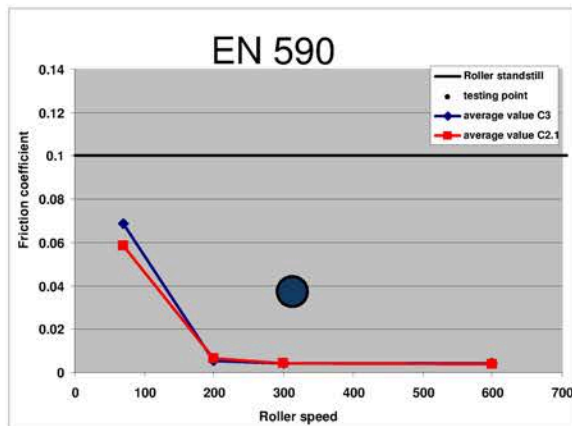
→ Better frictional coefficients improve the start-up behavior of the roller in the roller support.

AUDI-CP4 Situation in the field in Non-responsive content removed

2/10/2010

4. Summary of anti-wear package 1

Comparison of layer system* C3-C2.1 on friction coefficient test bench for



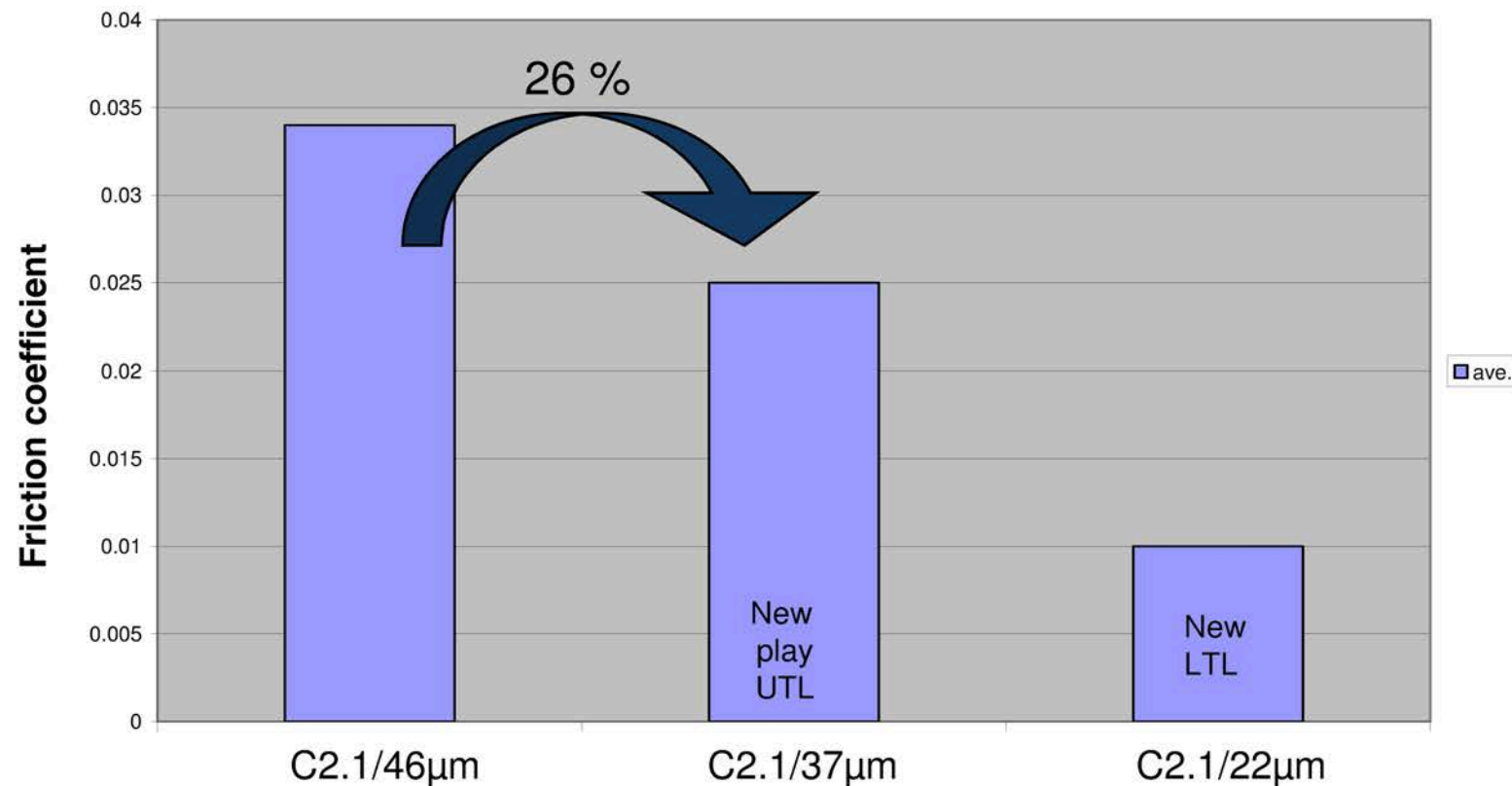
Assessment criterion: friction coefficient

*average comparable play



4. Summary of anti-wear package 1

Examination with viscosity 1.4mm²/s @40°C (Arctic Diesel)
Testing point 300rpm



4. Summary of anti-wear package 1

Further action:

- Because the anti-wear package was positively validated by the end of week 8/2010 with limit samples and critical fuels (kerosene, Arctic Diesel, WCF, FCF) series introduction approved for all CP4.2 pumps from Audi / VW (V6, V8, V12 TDI).
Production readiness is assured from week 9/2010 onwards.
This will confirm the schedule requirements from Audi from the last task force.
- A further objective is to enable the anti-wear package on a provisional basis in customer service worldwide. After the anti-wear package is installed in series, the first 400 pumps will be provided for customer service.
- An additional low-lubricity package (LLPx) is required for RoW (rest of world). LLPx is a combination of anti-wear package 1 plus a C coated pump piston plus measures for the improved start-up of the roller when starting the engine with poorly lubricating fuel.

4. Summary of anti-wear package 1 Effectiveness of robustness system:

Fuel quality	Problem	Series	RP1	LLPx*	Water separator
EN590/BDF520		+++	+++	++	
BDF650	Lubricity	(+)**	+++	+	
Kerosene	Viscosity	-	(+)	+	
Old biofuel	Adhesion, Lubrication	-	(-)	+*	
Water > 200ppm	Lubrication Visco, Corrosion	-	-	-	+

* LLPx: Depending on investigations of the differences between CP4.2 zu CP4.1 and the results of the FCF and WCF tests with RP1 measures, determination in the next 8 weeks

** with C coated piston (USA)

AUDI-CP4 Situation in the field in Non-responsive content removed

2/10/2010

AQUA: Active quality analysis
 Status 12/09-01/16/10 8:43 AM
 Source/user Non-responsive content removed

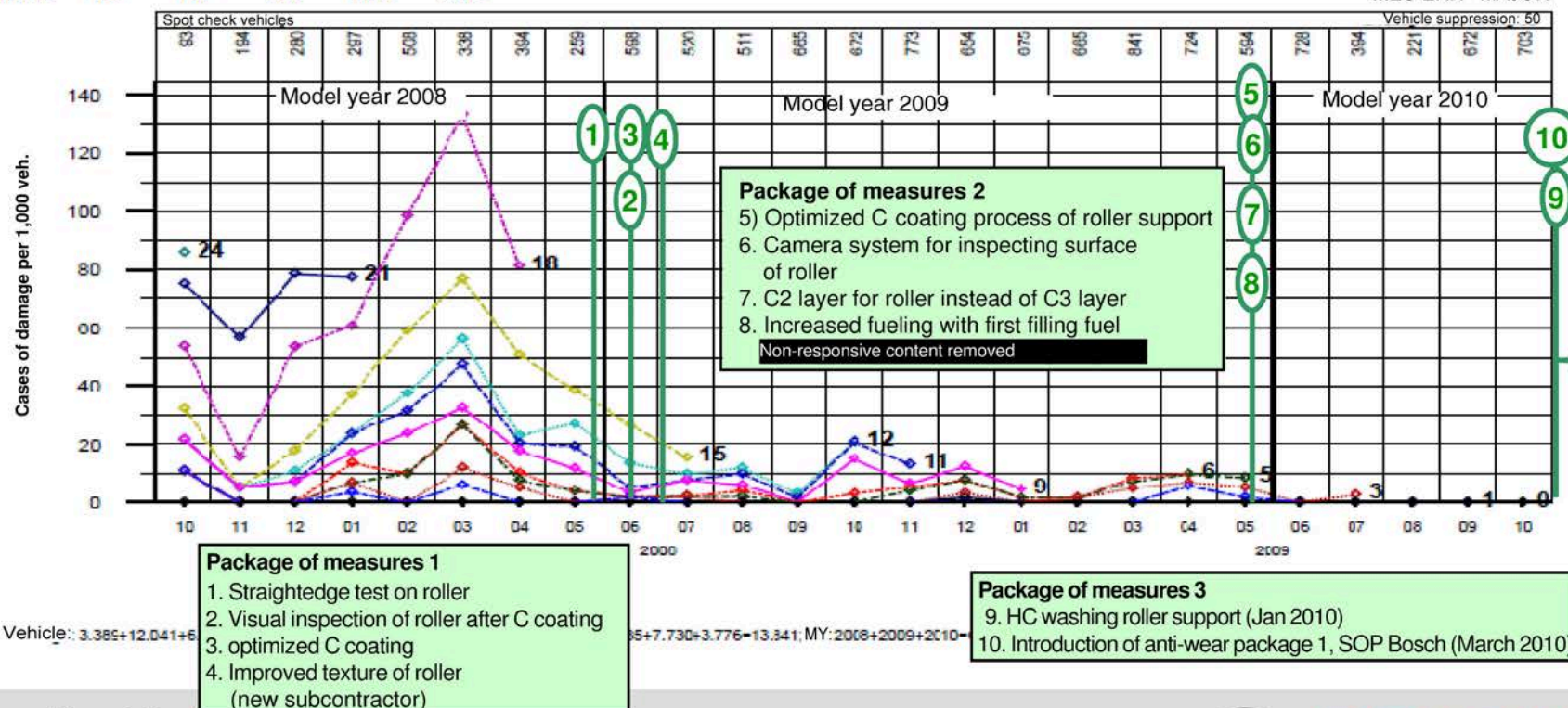
Audi, *, market: Non-responsive content removed CP4.2

Confidential
 Without PR numbers
 CNR 23/4

MY 2008 - 2010, Offset: all (Max: 2)
 CNR / Groups High-pressure pump

MY	MIS 0	MIS 1	MIS 3	MIS 5	MIS 6	MIS 9	MIS 11	MIS 12	MIS 15	MIS 16	MIS 21	MIS 24	MY	Exchange	BD	SA 13	SA 17
2008	00	1,7	3,9	9,0	10,3	18,0	23,6	27,8	44,5	78,5	103,2	119,7	2008	100,0%	81,3%	75,6%	14,2%
2009	01	0,9	1,9	3,8	4,4	7,8	11,7	14,3	23,0				2009	97,2%	86,0%	78,4%	13,1%
2010	00	0,0	2,1	3,1	3,1								2010	100,0%	100,0%	50,0%	50,0%
Diff%	-100	-100	8,53	-16,22	-29,13												

MEC ERR MAJOR



Diesel Systems



BOSCH

CP4 complaints - Collective completion QTS / IQIS messages

Background

- Completion of approx. 600 [REDACTED] pumps by AUDI in late 2010
- Reference report on distribution of error pattern through completed measures
 - Completion statistics with failure country [REDACTED] complaint period 01/2008 - 12/2010 (IQIS) by pump DM and fault name or fault pattern
 - In accordance with mail from [REDACTED] from 01/11/2010

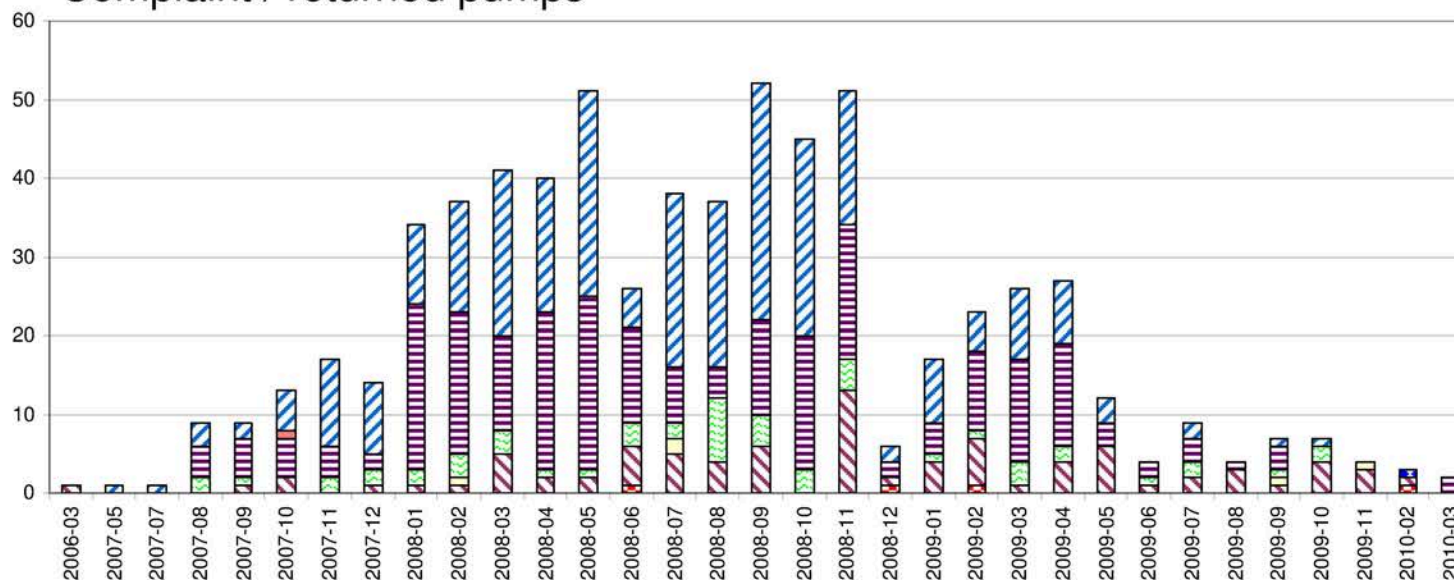
Overview: Number by fault name, pump family, [REDACTED] 01/2008 - 12/2010

Fault name	CP4.1	CP4.2	Total result
External intervention	1	3	4
OK according to spec.	16	70	86
Non-starter	5		5
Poor quality fuel	15	39	54
Drivetrain damage	62	176	238
Drivetrain damage / fuel not OK	68	211	279
CH cracked	1		1
MU defective	1		1
Overall result	169	499	668

CP4 complaints - Collective completion QTS / IQIS messages

Distribution of error symptoms through completed messages

Failure country: [REDACTED] complaint period (IQIS): 1/1/2008 - 12/31/2010
Complaint / returned pumps



Fault name

<input checked="" type="checkbox"/> External intervention	<input checked="" type="checkbox"/> OK according to spec.	<input type="checkbox"/> Non-starter
<input checked="" type="checkbox"/> Poor quality fuel	<input checked="" type="checkbox"/> Drivetrain damage	<input checked="" type="checkbox"/> MU defective
<input checked="" type="checkbox"/> Drivetrain damage / fuel not OK	<input checked="" type="checkbox"/> CH cracked	

Customer responsibility Pump DM month



CP4 drivetrain damage - Collective completion QTS / IQIS messages

Distribution of error symptoms through completed messages

Total complaints	Fault name	External intervention	OK according to spec.	Non-starter	Poor quality fuel	Drivetrain damage	Drivetrain damage / poor fuel	CH cracked	MU defective	Overall result
2006-03			1							1
2007-05							1			1
2007-07							1			1
2007-08					2	4	3			9
2007-09			1		1	5	2			9
2007-10			2			5	5		1	13
2007-11					2	4	11			17
2007-12			1		2	2	9			14
2008-01			1		2	21	10			34
2008-02			1	1	3	18	14			37
2008-03			5		3	12	21			41
2008-04			2		1	20	17			40
2008-05			2		1	22	26			51
2008-06	1		5		3	12	5			26
2008-07			5	2	2	7	22			38
2008-08			4		8	4	21			37
2008-09			6		4	12	30			52
2008-10					3	17	25			45
2008-11			13		4	17	17			51
2008-12	1		1			2	2			6
2009-01			4		1	4	8			17
2009-02	1		6		1	10	5			23
2009-03			1		3	13	9			26
2009-04			4		2	13	8			27
2009-05			6			3	3			12
2009-06			1		1	2				4
2009-07			2		2	3	2			9
2009-08			3			1				4
2009-09			1	1	1	3	1			7
2009-10			4		2		1			7
2009-11			3	1						4
2010-02	1		1					1		3
2010-03						2				2
Overall result	4		86	5	54	238	279	1	1	668

Failure country: █████ complaint period (IQIS): 01/01/08 - 12/31/10, complaint / returned pumps



CP4 drivetrain damage - Collective completion QTS / IQIS messages

Distribution of error symptoms through completed messages

Pump DM month	CP4.1			CP4.1 result					CP4.2			CP4.2 result		Total result	
	External intervention	OK according to spec.	Non-starter	Poor fuel	Drivetrain damage	Drivetrain damage/ not OK	CH cracked	MU defective	External intervention	OK according to spec.	Poor fuel	Drivetrain damage	Drivetrain damage / not OK		CP4.2 result
2006-03									1					1	1
2007-05													1	1	1
2007-07													1	1	1
2007-08											2	4	3	9	9
2007-09	1								1		1	5	2	8	9
2007-10							1		1		2	5	5	12	13
2007-11				1		2			3			1	4	9	14
2007-12					2	3			5		1	2		6	9
2008-01					5	1			6		1	2	16	9	28
2008-02	1	1	2	8	3				15		1	10	11	22	37
2008-03	1		1	5	7				14		4	2	7	14	27
2008-04	2				12	3			17			1	8	14	23
2008-05					12	10			22		2	1	10	16	29
2008-06			1	4	3				8	1	5	2	8	2	18
2008-07			2			7			9		5	2	7	15	29
2008-08				4	2	6			12		4	4	2	15	25
2008-09	3		2	2	6				13		3	2	10	24	39
2008-10			1	3	4				8			2	14	21	37
2008-11	1			3	4				8		12	4	14	13	43
2008-12										1	1		2	2	6
2009-01	2		1	1	3				7		2		3	5	10
2009-02	1				2				3	1	5	1	10	3	20
2009-03					2				2		1	3	13	7	24
2009-04			1	1					2		4	1	12	8	25
2009-05	3					1			4		3		3	2	8
2009-06											1	1	2		4
2009-07											2	2	3	2	9
2009-08					1				1		3				3
2009-09			1	1	1				3		1	1	2		4
2009-10				1					1		4	1		1	6
2009-11			1						1		3				3
2010-02	1	1					1		3						3
2010-03													2		2
Overall result	1	16	5	15	62	68	1	1	169	3	70	39	176	211	499

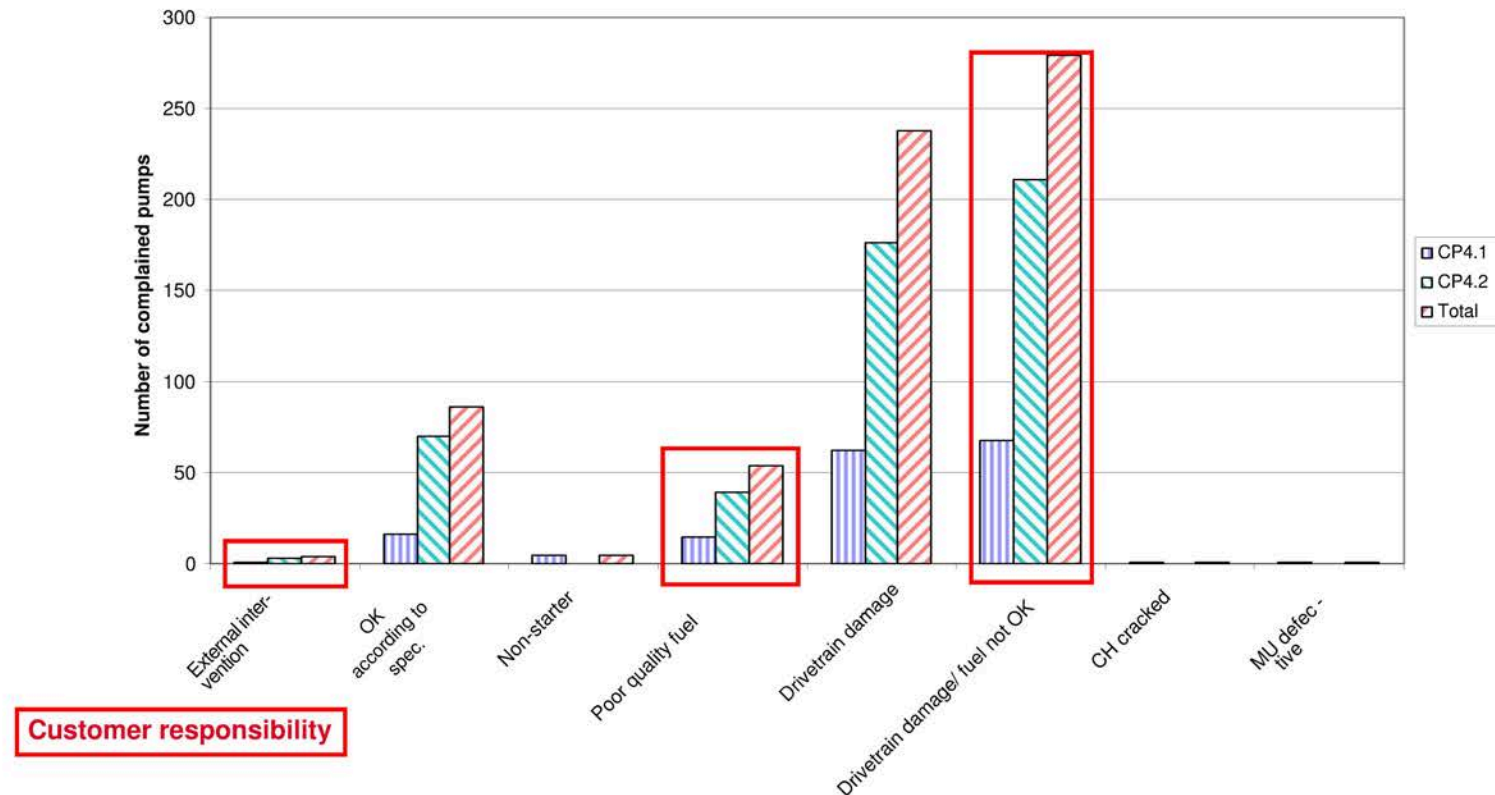
Failure country: [redacted]; complaint period (IQIS): 01/01/08 - 12/31/10, complained / returned pumps, single/twin pistons



CP4 drivetrain damage - Collective completion QTS / IQIS messages

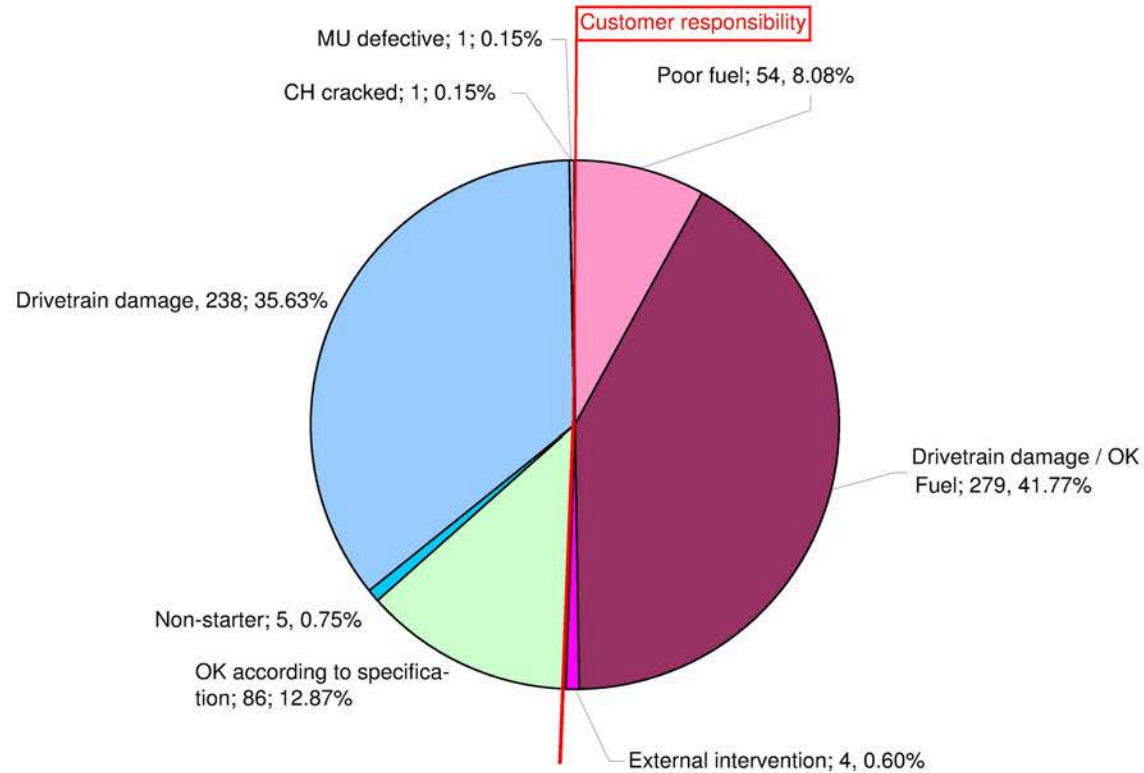
Distribution of error symptoms through completed Messages

Failure country: Non-responsive content removed complaint period (IQIS): 1/1/2008 - 12/31/2010
Complained / returned pumps



CP4 drivetrain damage - Collective completion QTS / IQIS messages

Share of CP4 error symptoms of returned pumps - completed messages 01/01/2008 - 12/31/2010



■ Poor fuel ■ Drivetrain damage / not OK Fuel ■ External intervention ■ OK according to spec. ■ Non-starter ■ Drivetrain damage ■ CH cracked ■ MU defective

Failure country [redacted] complaint period (IQIS): 01/01/08 - 12/31/10, complained / returned pumps

Diesel Systems

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CP4 drivetrain damage - Collective completion QTS / IQIS messages

Notes on individual error symptoms

RB responsibility:

- Drivetrain damage
- Non-starter
- MU defective (o-ring damaged)
- CH cracked

Summary:*

Measures see slide 8.
Measures see slides 9-14
Measure: new process for ensuring lubrication of o-ring before MU assembly starting 11/22/07
Measures: high-resolution ultrasound examination (Circular disc reflector = 0.7 instead of 1.5 previously) from 03/17/08; lining of fusing plant from 12/01/07

OK according to specification

- Will be tracked further as part of rail pressure fluctuation (error memory P0087 and P0088)

Customer responsibility:

- Poor fuel - during fuel analysis, water/RME content above the EN590 requirements or deposit formation was determined

* Details are documented in the respective 8D reports

CP4 drivetrain damage - Collective completion QTS / IQIS messages

Measures to avoid drivetrain damage

No.	Measures to reduce drivetrain damage	Introduction FeP		Introduction JhP	
		Today's date	WK	Date	WK
1	No reuse of tappet after OK press-in process	5/10/2007	WK19/07	1/31/2008	WK04/08
2	Click-clack test prior to delivery	5/10/2007	WK19/07	1/31/2008	WK04/08
3	Click-clack test	5/14/2007	WK0/07	1/31/2008	WK04/08
4	Delta T and Delta Tmax test on test bench	5/23/2007	WK21/07	1/31/2008	WK04/08
5	Click-clack test at end of assembly line	5/29/2007	WK22/07	1/31/2008	WK04/08
6	New switching process between flushing and inspection	5/30/2007	WK22/07	1/31/2008	WK04/08
7	Simultaneous noise measurement	6/18/2007	WK25/07	1/31/2008	WK04/08
8	Retest on friction coefficient test bench dropped	6/20/2007	WK25/07	12/1/2007	WK48/07
9	Optimization of test rig sequence (>500 rpm)	7/9/2007	WK28/07	1/31/2008	WK04/08
10	Cylinder head assembly with 5° torsion allowance	7/23/2007	WK30/07	12/1/2007	WK48/07
11	Dry pressing in of roller support	7/23/2007	WK30/07	2/6/2008	WK05/08
12	Uncoated spring plate (Customer C)	7/23/2007	WK30/07	1/31/2008	WK04/08
13	Introducing dwell time during roller tappet assembly	8/28/2007	WK35/07	2/6/2008	WK05/08
14	Extension of high-load testing point	10/1/2007	WK40/07	1/31/2008	WK04/08
15	Testing point V7.2 (Customer C)	11/16/2007	WK46/07	1/31/2008	WK04/08
16	Improved visual inspection of roller support	12/13/2007	WK50/07	1/31/2008	WK04/08
17	Friction coefficient test + / -10°	12/13/2007	WK50/07	2/7/2008	WK05/08
18	Tappet position query during assembly	12/21/2007	WK51/07	2/7/2008	WK05/08
19	New visual inspection catalog for roller support	1/2/2008	WK01/08	1/20/2008	WK02/08
20	Test program V7.2 (VW), visual inspection catalog for roller support	1/11/2008	WK02/08	1/31/2008	WK04/08
21	Test program V7.2 (Audi)	2/1/2008	WK05/08	1/31/2008	WK04/08
22	Switching of roller for models ... 507/...508	3/17/2008	WK12/08	1/31/2008	WK04/08
23	Straightedge testing, visual inspection catalog for roller support	4/7/2008	(WK5/08)	4/7/2008	WK14/08
24	Cleaning cloth with straightedge testing	5/1/2008	WK8/08	5/1/2008	WK7/08
25	Visual inspection of the roller after C coating	5/1/2008	WK8/08	5/1/2008	WK7/08
26	Optimization of the C coating (roller support)	5/1/2008	WK8/08	5/1/2008	WK7/08
27	Switching of roller for models ... 611/...613 to second source supplier	5/15/2008	WK0/08	11/3/2008	WK4/08
28	New washing and transport frames for the roller	10/29/2008	WK4/08	10/29/2008	WK4/08
29	Modified RS holding tool when pressing in the tappet body	11/24/2008	WK48/08	5/6/2009	WK19/09
30	Carbon covers / holders in system N for roller support	12/12/2008	WK50/08	12/12/2008	WK50/08
31	Carbon covers / holders in system O for roller support	3/16/2009	WK12/09	3/16/2009	WK12/09
32	Camera system to detect metal spatters on roller support System installed / testing Series introduction from mid 06/2009 soonest		WK19/09		Roller support will be supplied from FeP
33	Introduction of C2.1 layer instead of C3 layer on roller end (VW/Audi)	23.05.2009	WK25/09	23.05.2009	RS will be supplied from FeP
34	Optimized substrate holder to prevent fusing on roller, at the earliest	Activity broken off because not expedient	WK32/09	Activity broken off because not expedient	WK32/09
35	HC washing of roller supports instead of aqueous washing	12/2/2009	WK49/09	12/2/2009	WK49/09
36	Introduction of anti-wear package RP1 in FeP and JhP (twin pistons)	3/9/2010	WK10/10	3/9/2010	WK10/10
37	Introduction of anti-wear package RP2 in FeP and JhP (twin pistons)	10/26/2010	WK43/10	11/18/2010	WK45/10

Cause of error / measures will be developed in weekly task force with AUDI

Status: WK03/2011

Diesel Systems



Cleanliness status CP4 as of 10/13/2010

FeP: Cleanliness measures

Pre-assembly

CH pre-assembly

R: Non-responsive content removed

No.	Measure for reducing the residual dirt	Introduction FeP	
		Date	WK
4	Improvement of the LS bolting process: - Height monitoring, manual pre-fixing of screws at the assembly station 1 since 4/3/06 - Rearrangement of all the manual workplaces	5/26/2009	22
6*	Strainer in front of the intake valve	Pilot customer from 01/18/2010, additional customers in planning	
7	Changeover of the LS delivery from bulk goods to workpieces in blister	11/5/2009	45
8	St.220/230: Adhesive rollers for hand gloves introduced on all modules.	2/19/2010	7
9	St.220: Change the design of the HP screw thread	1/29/2010	4
10	St.230: Determine contact points for handling of parts (Manufacturing methods and processes)	1/22/2010	3
11	Encapsulation (supply LS and IV, module removal), module 1 and 6 completed	3/19/2010	11
12	Check the checker Parts not painted but covered with yellow shrink-fit hose	4/30/2010	17
12*	St.230: Support on the measuring device. Optimization of the CH alignment.	6/28/2010	26
13*	St.210: Change supports to Vulkollan material	7/17/2010	28
14*	St.220: Changeover to rotary plate with Vulkollan for handing over the workpiece	6/26/2010	30
15	St.220: Encapsulation (complete with doors)	9/10/2010	36
16	St.210: Encapsulated space / rack for reintroduction of parts with procedural errors in the production flow (on all modules)	10/1/2010	39
	St. 201 = Station to press in non-return valve (NRV)		
	St. 220 = Station to screw in locking screw (LS)		
	St. 230 = Station to match cylinder head and piston		
	Abbreviations: IV = Intake valve, NRV = Non-return valve		

Legend: implemented Implementation as planned Date of implementation exceeded Implementation not expedient; effectiveness being checked

Diesel Systems



Cleanliness status CP4 as of 10/13/2010

FeP: Cleanliness measures

Assembly

Assembly

Non-responsive content removed

No.	Measure for reducing the residual dirt	Introduction FeP	
		Today's date	WK
14	Introduction of radius on the MU magnetic core for avoiding shavings on the housing in the CP4 assembly station, screw on MU 130 - Test (3000 pc.) with radius on the magnetic core positively concluded - Test with early delivery (300 parts) on 07.07.09 - Implement	11/2/2009	45
15	Optimize cleaning to avoid soiling tappet body holders on WPC (Manufacturing methods and processes adjusted)	12/1/2009	49
16	Dyeing the transponder on the next delivery	1/29/2010	4
17	Work without gloves on module 2, test stopped due to risk of accident	1/29/2010	4
18	Introduction of new clamping device for WPC housing on module 6	2/5/2010	5
19	Optimization of the grab containers (O-rings) with larger radii (chip nests) on all modules (pc. 60/110/120)	2/5/2010	10
20	Tape roller for gloves and glove supports on all modules for cylinder head assembly stations 1 & 2 (st110 & st120)	4/16/2010	15
21	Change handling at station 10 Press in low-pressure connections and station 50 Pre-assemble flange to avoid intervention in the housing interior.	4/16/2010	15
22	Mount holding clips for goods accompanying documents on the corresponding stations (on all modules)	4/16/2010	15
23	Sensitization and instruction of all employees of all CP4 modules with cleanliness film Non-starters	4/30/2010	17
24*	St.80: Regular check and exchange of Murtfeld supports	7/1/2010	26
25*	Makrolon cover on the transport belt st.110 to st.130 (on all modules)	7/5/2010	27
26*	Change handling at st.50 to avoid intervention in the flange (adhesive films)	7/17/2010	28
27*	During the assembly of the cylinder head (st. 110/120), the frames will be replaced by blisters on all modules	7/31/2010	30
26	St. 10: New involute clamping device like module 6 (on all modules)	9/3/2010	35
28*	Pilot project on module 6: Add suction for o-ring insertion into housing during assembly of cylinder head st. 110/120, decision on introduction of other modules; R: FeP/MOE	10/2/2010	39

Legend: implemented implementation as planned Date of implementation exceeded Implementation not expedient; effectiveness being checked

Diesel Systems



Cleanliness status CP4 as of 12/16/2010

FeP: Cleanliness measures

Housing production

Housing

R: Non-responsive content removed

No.	Measure for reducing the residual dirt	Introduction FeP	
		Date	WK
22	Optimization deburring of the transition (no suggestions)	9/20/2009	38
23	Optimize deburring separating area with fan nozzle	9/21/2009	39
24	Optimization of the deburring of the separating area by mounting the fan nozzle in a titled manner	9/21/2009	39
25	Standardization of the visual inspection equipment	9/25/2009	39
26	Extension of the approach path of the HP lance in the bow-shaped channel (35 mm instead of 50 mm)	9/30/2009	40
27	Optimization of the processing sequence	9/30/2009	40
28	Rinsing the internal area of the pump from inside to outside	9/30/2009	40
29	Intr oduction of ball cutter for improving the situation of burr; cylinder head inlet to MWU	10/21/2009	43
30	Regular cleaning of the gripper in the chain. Extension of the inspection and maintenance plans	15.012.010	2
31	OP40 Optimization of the tool sequence (for avoiding the entry of dirt in the cleaning system)	2/28/2010	8
32	Production test with blasted housing blanks	4/30/2010	17
33	Increasing the nozzle diameter of the rotating HP lance	5/21/2010	19
34	Avoidance of particle in collar bushing (beneath stop disk)	5/21/2010	20
35	Avoidance of particles in housing interior: Optimization of seal & flush, fixing of additional pipes for more flow to the inner chamber flushing system	5/21/2010	20
36	Optimization of rotating HP lance	6/21/2010	24
37*	Avoidance of particles in the housing interior, test of HP lance on module 8	8/6/2010	31
38	Increase nozzle diameter of rotating HP lance; trial completed, implemented on one module; other modules by WK45	11/11/2010	45

Legend: implemented Implementation as planned Date of implementation exceeded Implementation not expedient; effectiveness being checked

Diesel Systems



Cleanliness status CP4 as of 10/13/2010

FeP: Cleanliness measures

CH production

CH production

R: Non-responsive content removed

No.	Measure for reducing the residual dirt	Introduction FeP	
		Date	WK
1*	Visual check after the HC cleaning: Temporary more strict visual check targeted at particles for collecting findings. No particles found since the date of introduction (statement applies to FeP)	2/16/2009	7
2	Ban on reuse of covering bags on finished cylinder heads (after visual inspection)	2/23/2010	8
3	Visual check: Equip cover transport belt with maintenance lid	2/23/2010	8
4	Eliminate compressed air connection at visual inspection station; connection of compressed-air pistol no longer possible	3/12/2010	10
5	Determine or re-define MAE cleaning intervals (revise cleaning catalog)	4/30/2010	17
6	Washing system: Magnetic separator in the filter	5/3/2010	18
7	Adjust cleaning intervals of the transport wagons	6/30/2010	26

Legend: implemented Implementation as planned Date of implementation exceeded Implementation not expedient; effectiveness being checked



Cleanliness status CP4 as of 10/13/2010

FeP: Cleanliness measures

Intake valve & flange

Intake valve

Non-responsive content removed

No.	Measure for reducing the residual dirt	Introduction FeP	
		Date	WK
1	Manual suction of the IV before introduction of visual check	4/9/2010	14
2	Do not reintroduce oil carried-off from the automatic station into the process, but dispose it off separately	4/29/2010	17
3	Protective coverings constantly between assembly and supermarket	8/13/2010	32
4	Integrate automatic suction facility in the automatic machine	9/10/2010	36

Flange

R: Non-responsive content removed

No.	Measure for reducing the residual dirt	Introduction FeP	
		Today's date	WK
1	Deburring the tapering 19 inch milling border	2/15/2008	7
2	Rinsing the cleaning chamber after every cleaning cycle (3 cleaning stages)	2/15/2008	7
3	Introduce the rinsing tool in OP40	10/20/2009	43
4	Optimizing the brushes of the screw contact surface	12/2/2009	49

Legend: implemented Implementation as planned Date of implementation exceeded Implementation not expedient; effectiveness being checked



Cleanliness status CP4 as of 10/13/2010

FeP: Cleanliness measures

Locking screw

LS supplier

R: Non-responsive content removed

No.	Measure for reducing the residual dirt	Introduction FeP	
		Date	WK
1	Sensitization of the supplier about the effects of faulty LS threads; short-term introduction of 2x sorting, currently more than 1x under higher resolution	1/29/2009	5
2	Further optimization of the spilling process after thread rolling and filling of the blasting system on the supplier's site	5/25/2009	23
	Additional LS brushing after thread rolling	6/8/2009	24
3	100% automatic camera check of LS thread in the (no proposals) - Camera inspection installed, query of geometric dimensions of LS introduced	8/1/2009	30
4	Optimization of image recognition of the LS thread flanks according to limit sample catalog (see pt. 7)	See item 7	
5	Change test guideline / LS limit sample catalog Draft of new test guideline: 10/09/09 / Creation of special release for test guideline with restrictions	10/14/2009	42
6	Changeover of the LS delivery from bulk goods to workpieces in blister (Presentation sample blister: 10/19 / Sample from series tool: 10/21/09 / Changeover from 10/30)	11/5/2009	45
7	Introduction LS washing before the visual check and packing	4/1/2010	13

Legend: implemented Implementation as planned Date of implementation exceeded Implementation not expedient; effectiveness being checked

Diesel Systems



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Diesel Fuel Oxidation Stability

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Diesel Systems



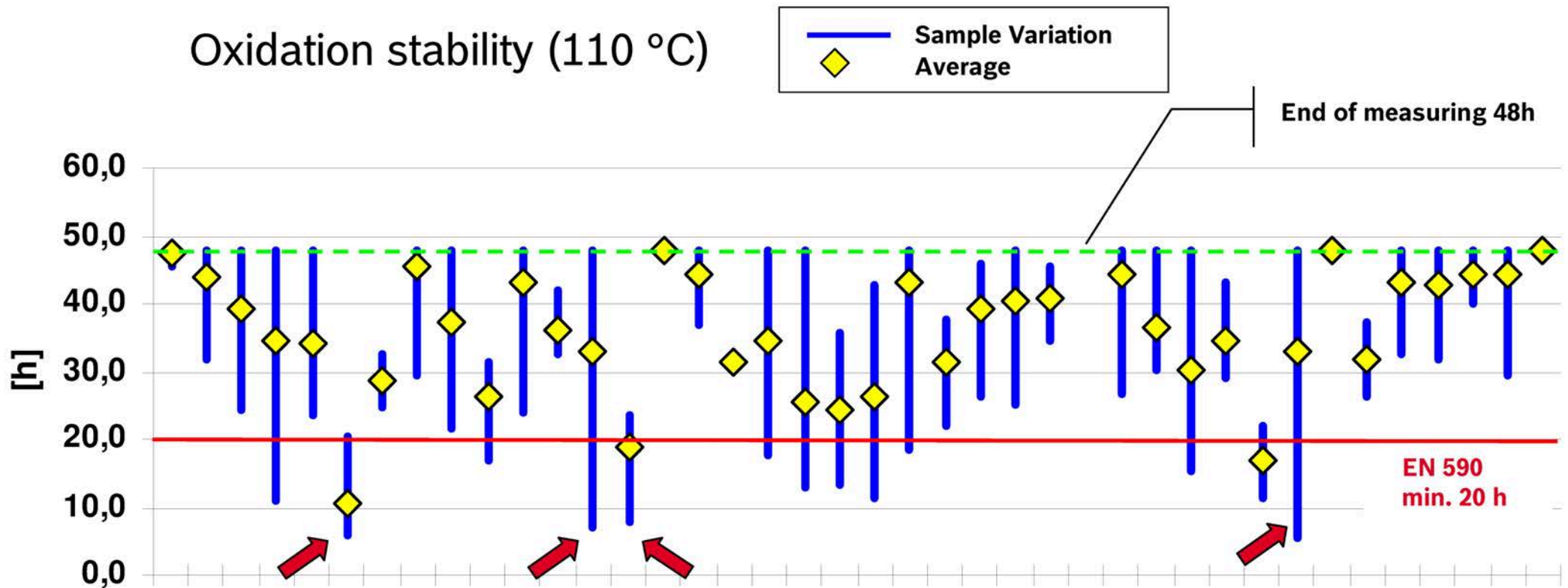
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Situation May 2011

- with introduction of biodiesel admixture oxidation stability diesel fuel
 - dropped significantly
 - exhibits larger number of samples not fulfilling EN590 specification
- worst case quality
 - similar to not developed diesel markets like
 - significantly worse than in established diesel markets like
 - or
- improvements seen between 2009 and 2010, but **quality worsened again in 2011!**
- **establishment of EN590 spec fuel quality absolutely necessary to avoid problems at end customer**



Oxidation stability (110 °C)



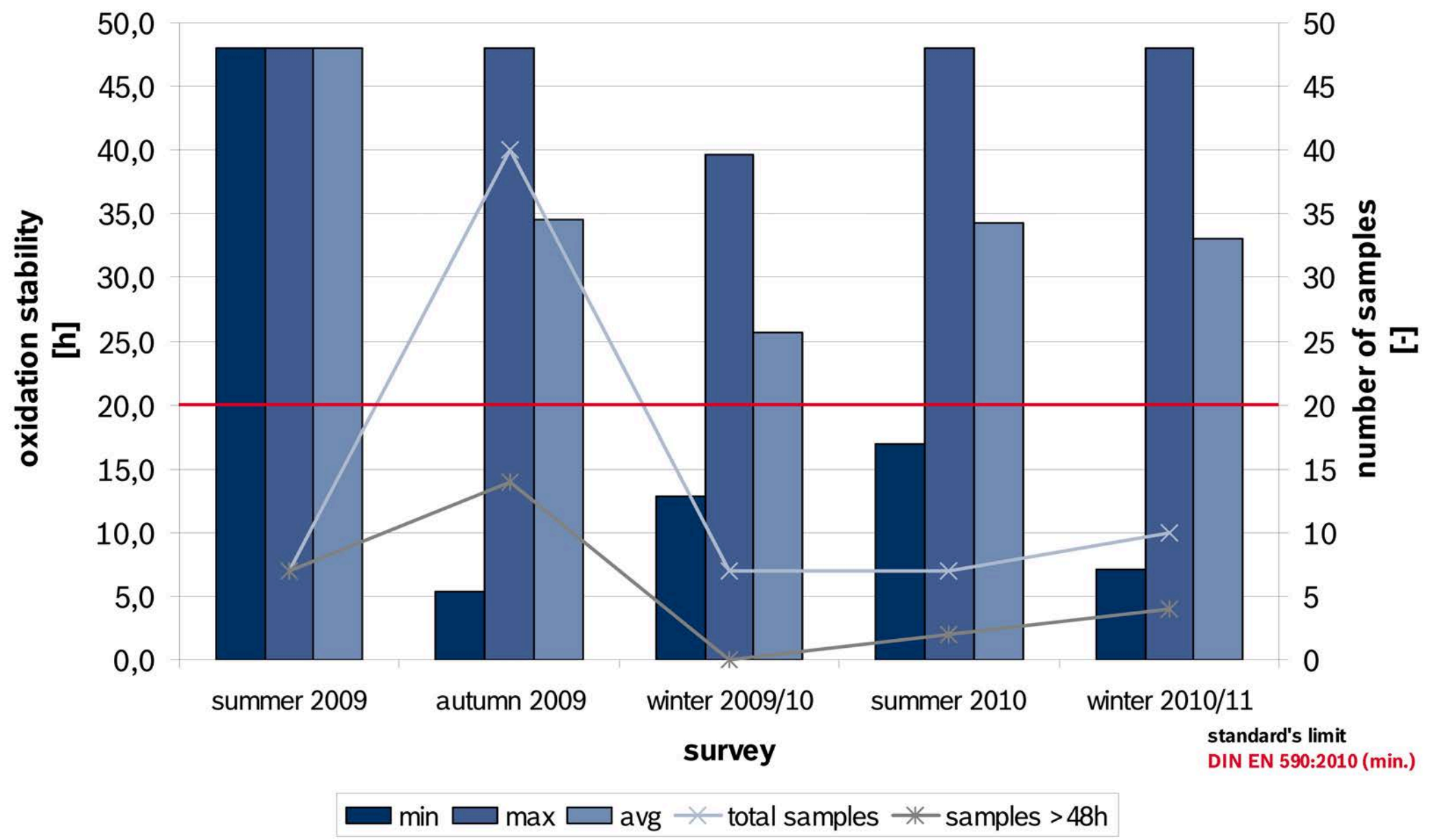
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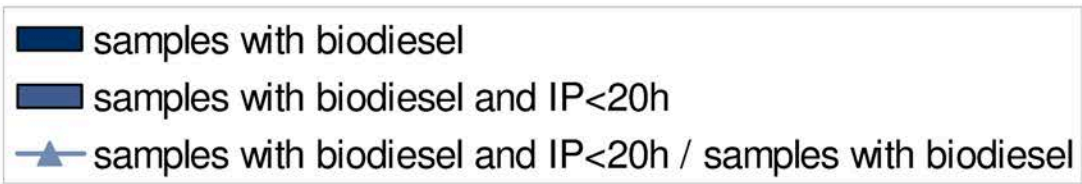
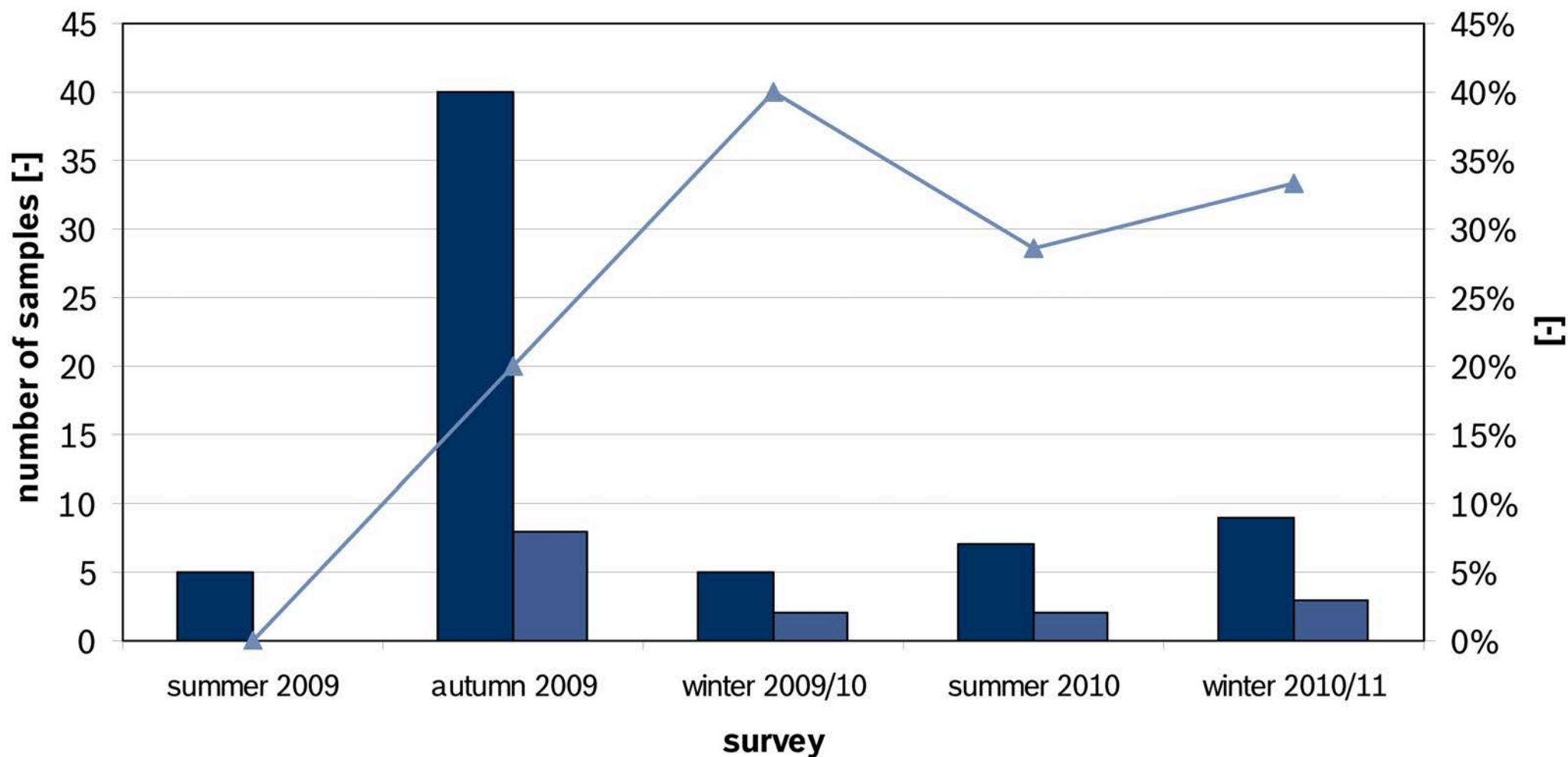
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Oxidation Stability (Rancimat)



Oxidation Stability (Rancimat)



Remarks

- in total 71 [Non-responsive content removed] SGS samples from summer 2009 to winter 2010/2011 are available
- samples above 48 hours of oxidation stability are included in minimum, maximum and average calculation with the value 48
- all samples from summer 2009 (without biodiesel!) are above 48 hours of oxidation stability
- source:
 - SGS_summer09,
 - SGS [Non-responsive content removed],
 - SGS [Non-responsive content removed],
 - SGS [Non-responsive content removed]
 - SGS_winter1011







Robustness of Common Rail System for Rest of the World

Problem	Increasing use of CR system in fuel-critical markets
Cause	Lubricity, viscosity, Water, particles in fuel
Measure/	Necessary to use additional measures on hydraulic components and on vehicle (water separator, parti- cle filtering)
Status	Launch SOP July 2010

ENTIRE PAGE CONFIDENTIAL

EA11003EN-01825[1]

Robustness of Common Rail System for Rest of the World
Status of evaluation of Rest of the World conditions for diesel

Product	P	K	L	D
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CP4	Currently under assessment 	free / resolved 	BDF570  BDF650 	>1,0 mm ² /s at 70°C  <1.0 mm ² /s at 70°C 
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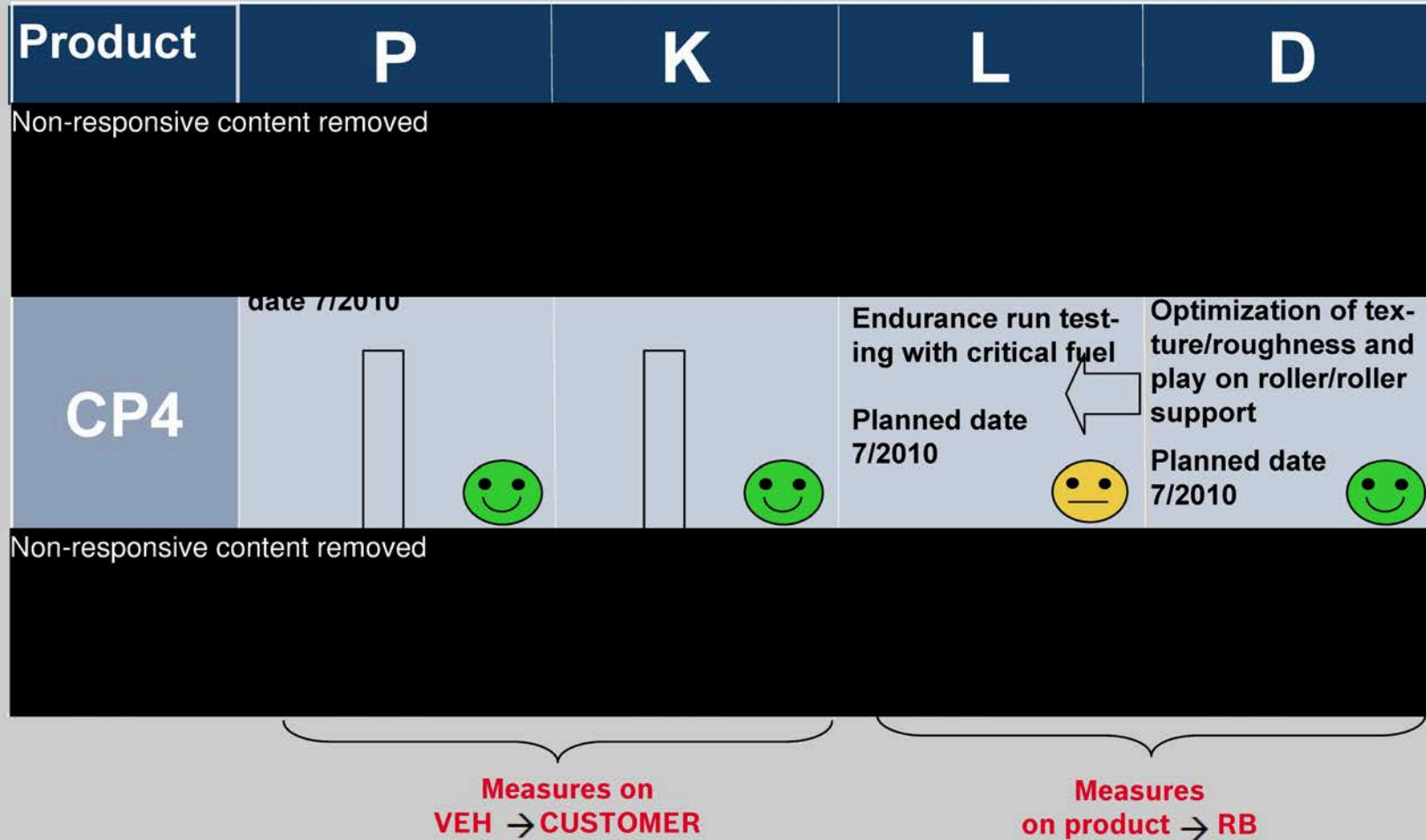
Measures on
VEH → CUSTOMER

Measures on
product → RB

ENTIRE PAGE CONFIDENTIAL

EA11003EN-01825[2]

Robustness of Common Rail System for Rest of the World
Status of evaluation of Rest of the World conditions for diesel



Workshop for detailed planning of RoW planned for 12/8/09 with VW/ Audi Development

Robustness of Common Rail System for Rest of the World Measures to increase robustness in fuel-critical markets

- Expert workshop VW/ Audi/ Bosch on fuel-related themes 12/8/2009

Lubricity

- Further development of wear-optimized C layer (already being tested in medium duty application) planned for SOP 07/2010

Viscosity

- Optimize texture/surface of roller done
- Optimize texture/surface of C layer in roller support planned for SOP 07/2010
- Optimize component tolerances (play) roller-roller support planned for SOP 07/2010

Water

- Introduction of water separator urgently necessary for critical markets OEM
- Avoidance of fatigue through higher quality materials on camshaft/roller (preliminary tests with higher quality material pairing ongoing) 04/2010
- Long-term testing will be necessary after the preliminary tests are complete SOP ?

ENTIRE PAGE CONFIDENTIAL

EA11003EN-01825[4]

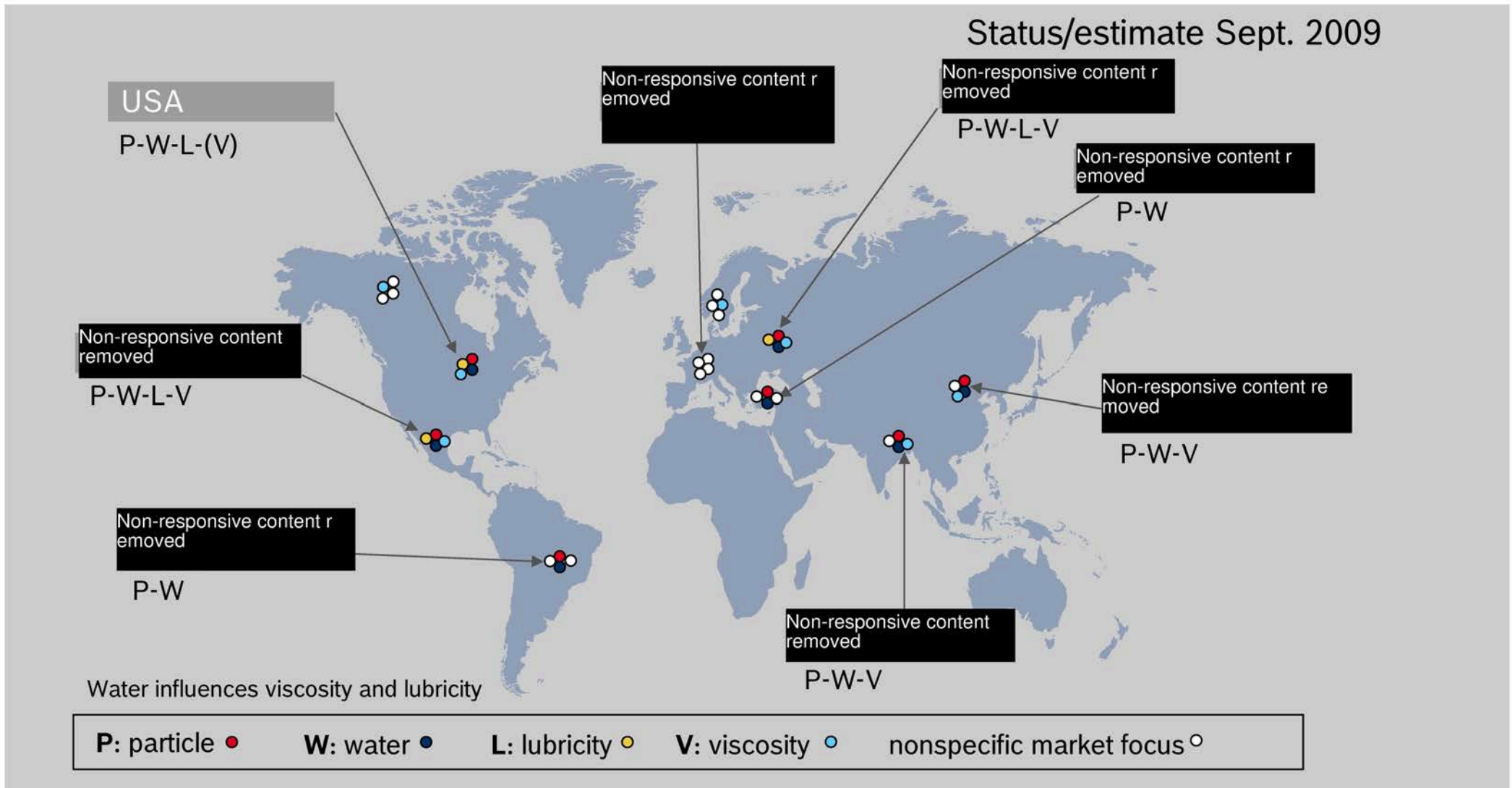
Robustness of Common Rail System for Rest of the World Backup



ENTIRE PAGE CONFIDENTIAL

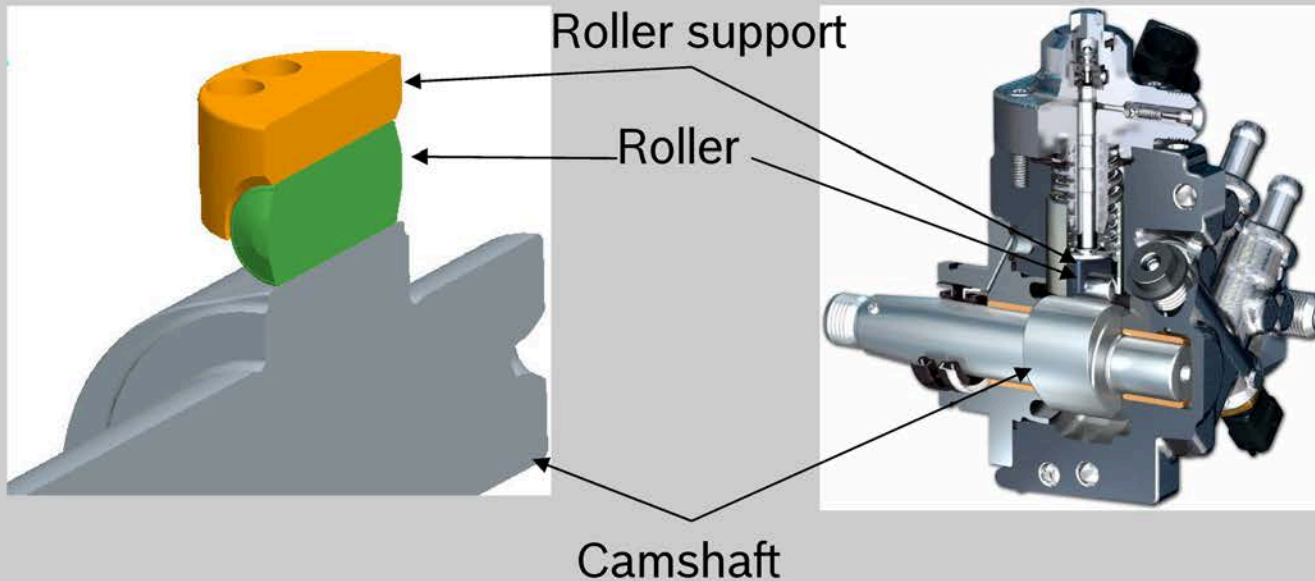
EA11003EN-01825[5]

Robustness of Common Rail System for Rest of the World Diesel Fuel Risk



Robustness of Common Rail System for Rest of the World Interactions of CP4 drivetrain damages

The cause of drivetrain damage is operation with impermissible fuel qualities and/or high component function sensitivity



Robustness of Common Rail System for Rest of the World Influence of fuel quality

Low lubricity (kerosene, water,...)

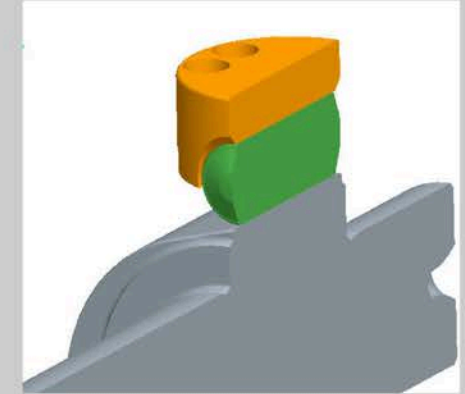
- causes greater wear in the roller/roller support assembly (up to 200 [rpm]) at start (mixed friction area)

Low viscosity Non-responsive content removed diesel, kerosene, water....)

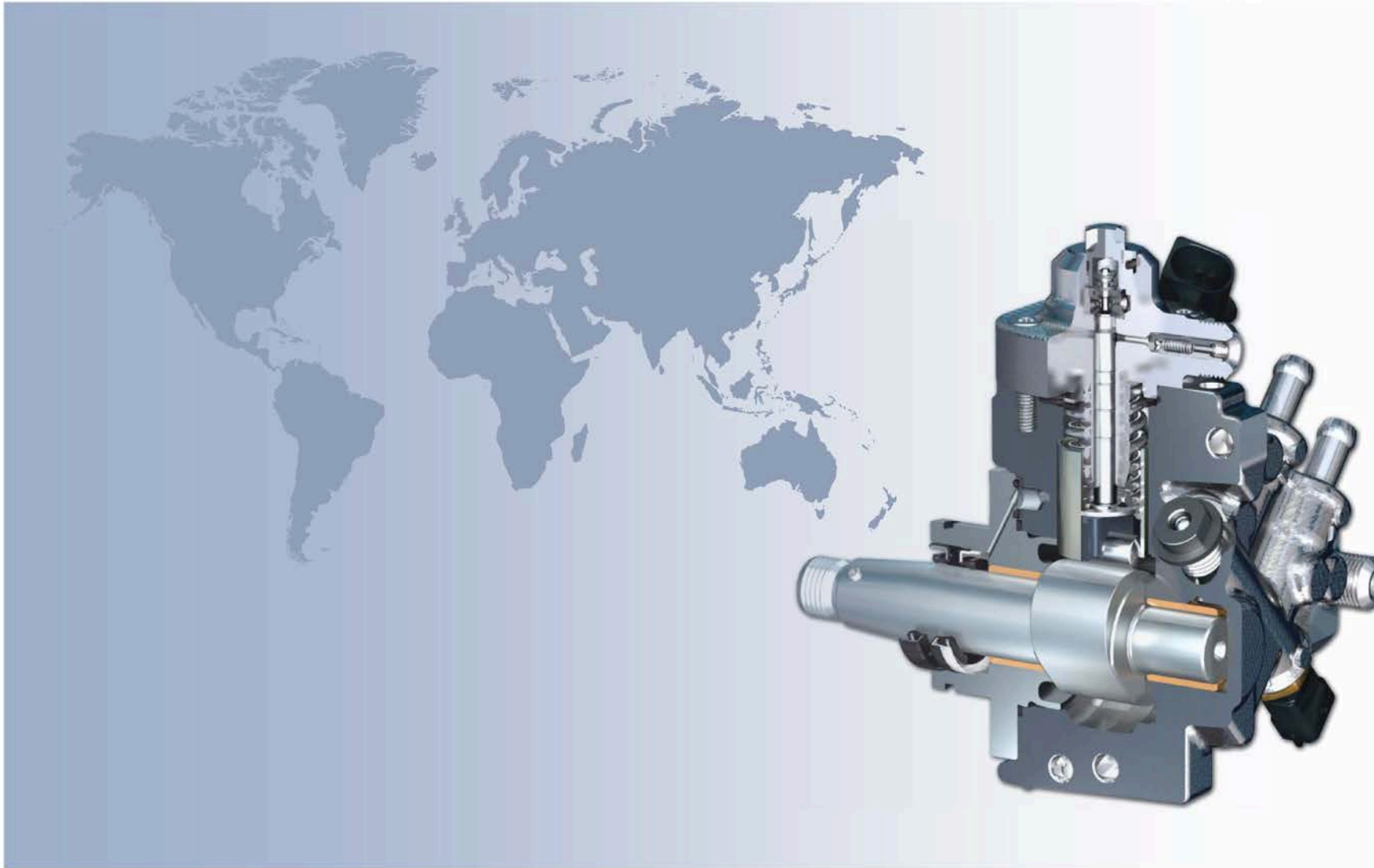
- leads to thin lubrication film -> increased friction/ component contact
-> increased slippage (idle roller)

Water in fuel

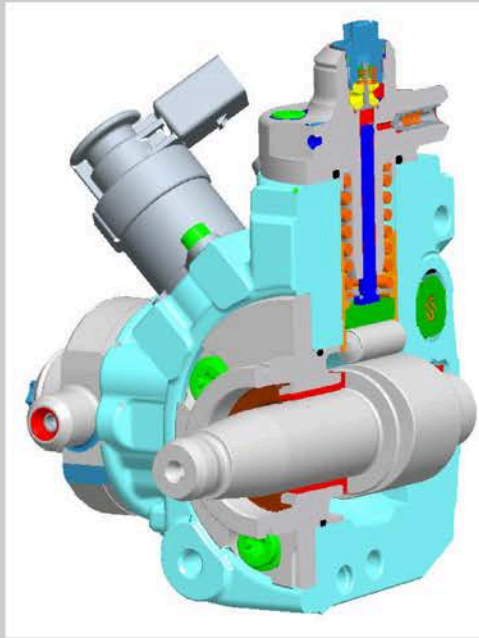
- Influence as emulsion, see lubricity & viscosity
- Free water (in droplet form) can result in hydrogen embrittlement / stress corrosion and thus to fatigue of the partner roller



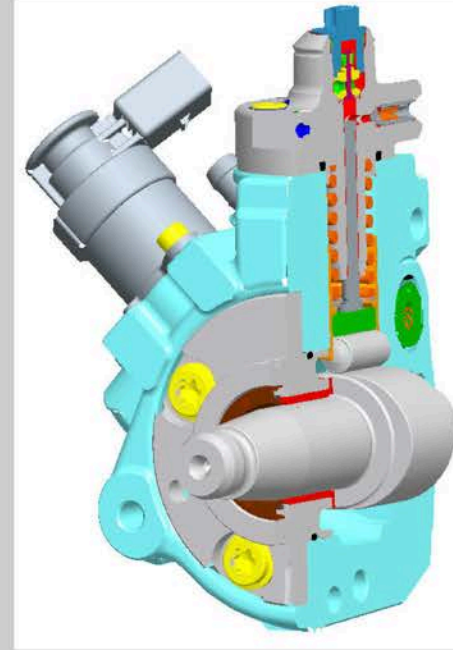
CP4 field situation worldwide



CP4 field situation worldwide Differences between CP4.1 and CP4.2



CP4.2
Twin pistons pump
for use in
6-cylinder engines



CP4.1
Single piston
pump for use in
4-cylinder engines

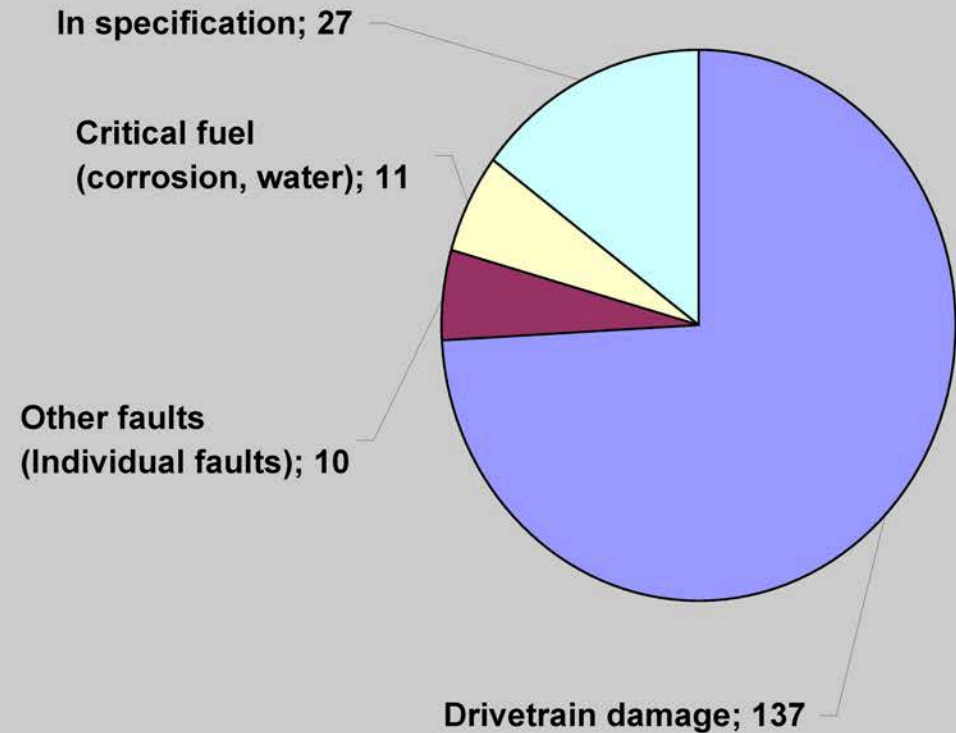
CP4 field situation worldwide AUDI CP4.2 complaints

Commercial calculations for dealers
(delivered quantity: 218,699)

ISO_CTRY	Overall result
Non-responsive content removed	328
	85
	63
	40
	21
	19
	18
	14
	9
	9
	8
	4
	4
	1
Overall result	623

Source Audi-Saga evaluation period: 08/2007 - 10/2009

Results of findings for the pumps returned to Bosch (185)



Source Bosch IQIS Date: 11/3/2009

EA11003EN-01826[3]

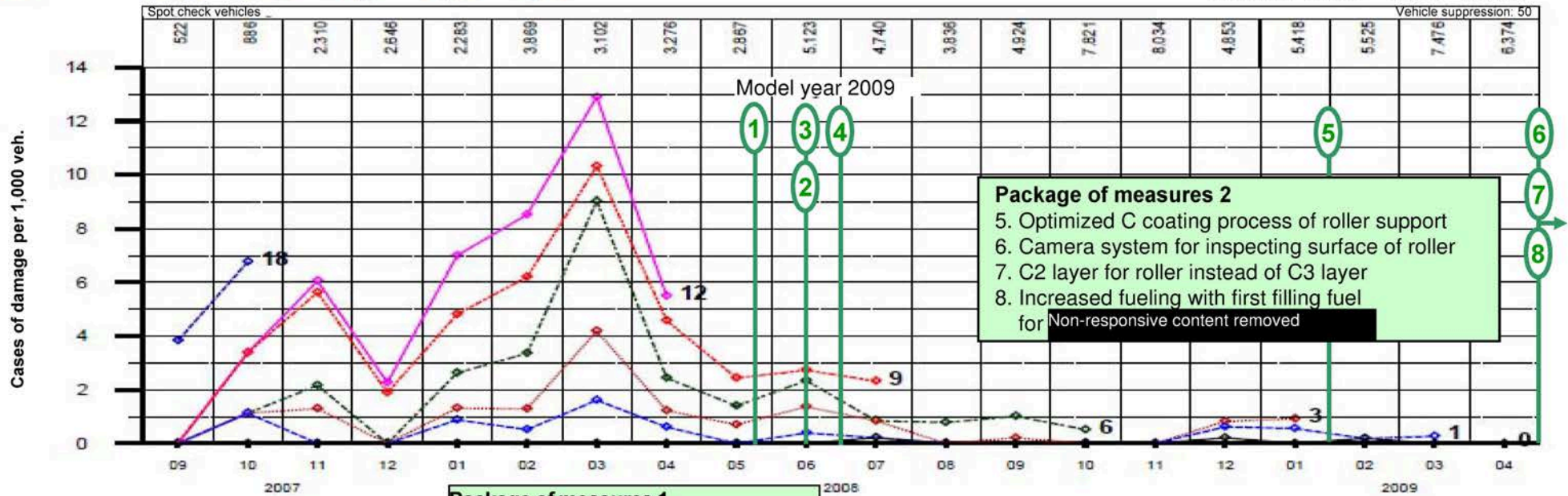
CP4 field situation worldwide AUDI VW 6-cylinder TDI

AQUA, Active quality analysis
Status 09/09-11.05.09 04:27 PM
Source/user Non-responsive content removed

Audi, market: AUDI (approved markets)
MY 2008 - 2010, Offset: all (Max: 5)
CNR / Groups High-pressure pump

Confidential
Without PR numbers
CNR 2374

MY	MIS 0	MIS 1	MIS 3	MIS 6	MIS 9	MIS 12	MIS 18	MY	Exchange	BD	SA 10	SA 17	SA 50	SA 18
2008	0,0	0,6	1,5	3,1	5,2	6,6	11,2	2008	98,0 %	62,8 %	76,7 %	12,3 %	7,0 %	1,7 %
2009	0,0	0,2	0,5	1,2	1,9	2,4		2009	96,7 %	50,0 %	69,7 %	17,1 %	5,3 %	4,6 %
Diff%		-64,45	-67,70	-61,37	-62,69	-62,99					MEC ERR	MAJOR	LEAK	MINOR



Vehicle: 29.592+92.395+37.767=159.754; Sold: 29.424+89

11.914; MY:2008+2009+2010=Total

CP42 AU alle MKB V6 Freil 08-10

I1003EN-01826[4]

CP4 field situation AUDI VW 6-cylinder TDI

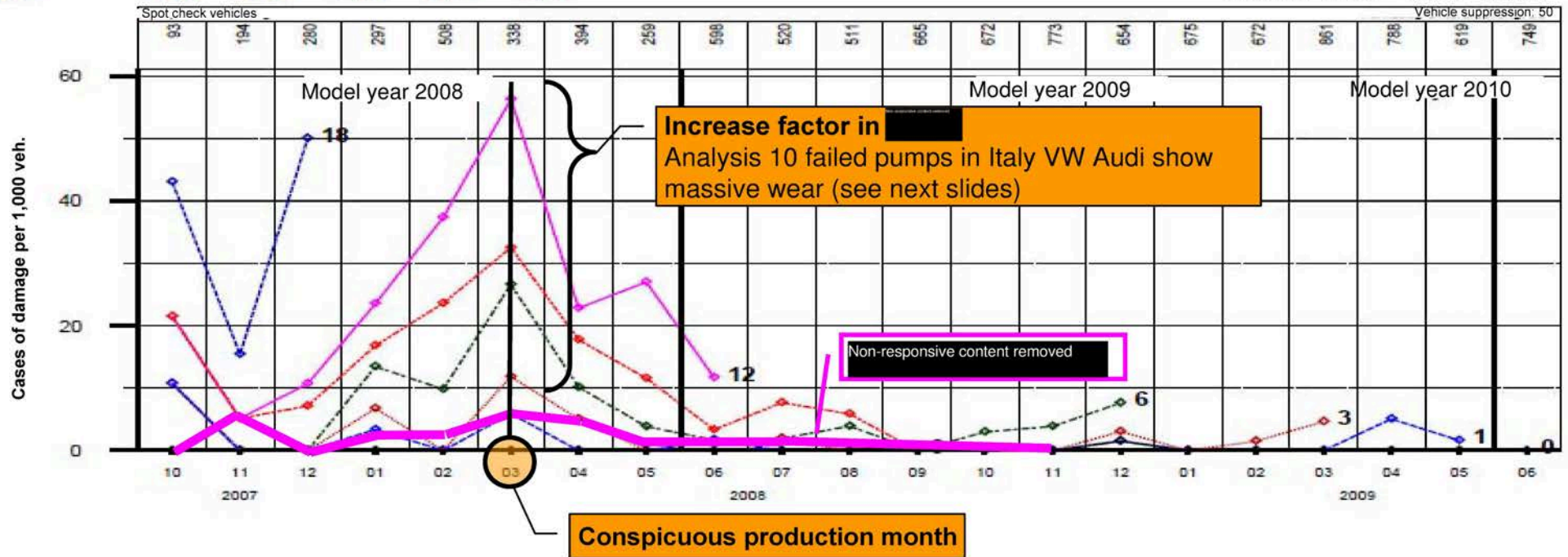
Non-responsive content removed

AQUA, Active quality analysis
Status 09/09-11.05.09 4:29 PM
Source/user Non-responsive content removed

Audi, market: [redacted]
MY 2008 - 2010, Offset: all (Max: 3)
CNR / Groups High-pressure pump

Confidential
Without PR numbers
CNR 2374

.MY	CAMA CAMB CANA CANB CANC CAND CASA CASB CASC CASD CCWA CCWB CDYA CDYB CDYC CGKA CGKB								MY	Exchange	BD	SA 10	SA 17	SA 50	SA 18
	MIS 0	MIS 1	MIS 3	MIS 6	MIS 9	MIS 12	MIS 18								
2008	0,0	1,7	3,9	10,3	18,0	27,8	66,4	2008	100,0 %	78,2 %	74,4 %	15,4 %	7,1 %	2,6 %	
2009	0,1	0,9	2,0	4,2	7,7	13,7		2009	98,3 %	83,1 %	79,7 %	18,9 %	1,7 %	1,7 %	
Diff%		-47,14	-48,71	-59,55	-57,23	-50,83						MEC ERR	MAJOR	LEAK	MINOR



Vehicle: 3.389+12.041+4.481-19.911; Sold: 3.385+11.240+2.900-17.525; UP: 2.335+7.730+2.115-12.180 MY: 2008+2009+2010-(Total)

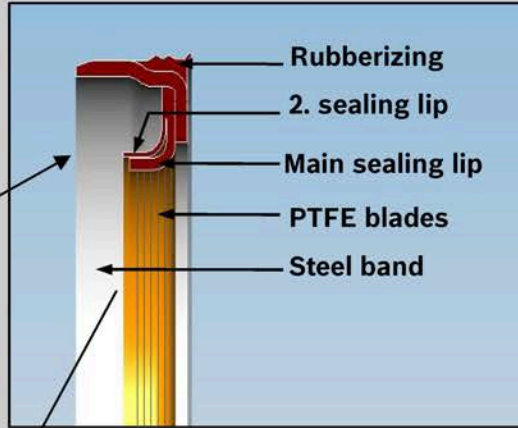
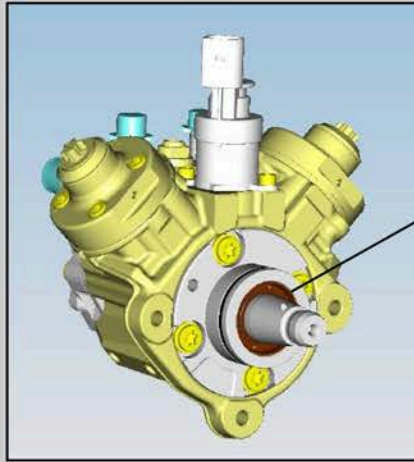
CP42 AU alle MKB V6 08-10

CP4 field situation

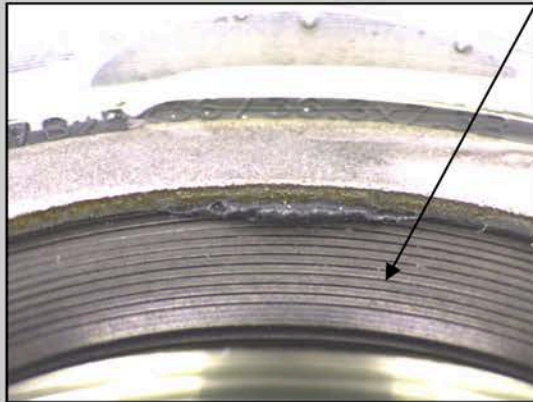
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Finding AUDI CP4

Installation of Bruss shaft seal on CP4



New part

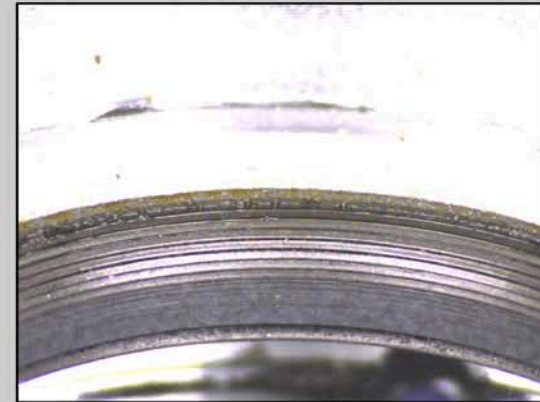


Vehicle endurance run
118,000 km



Mileage 2,212 km
Failure on 6/15/2009 in

Non-responsive content removed

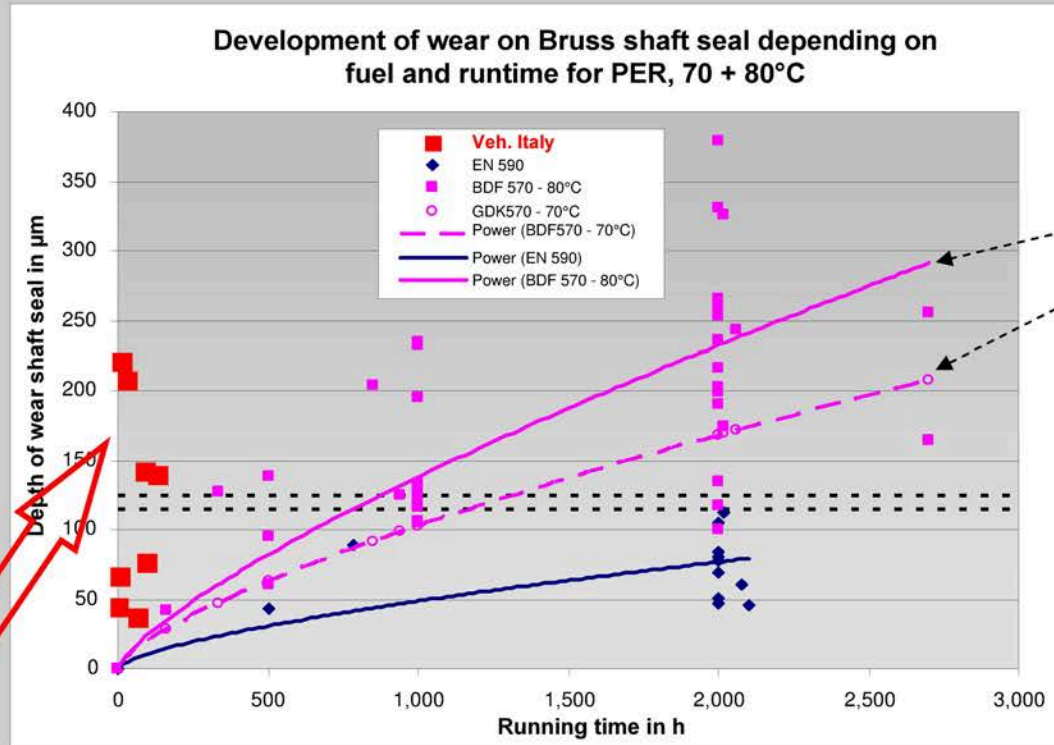


CP4 field situation Non-responsive content removed Finding AUDI CP4

Dependence of shaft seal wear on fuel and runtime

EN590: Viscosity_{40°C} = 2.5 mm²/s, HFRR_{60°C} = 420 μm

BDF570: Viscosity_{40°C} = 1.9 mm²/s, HFRR_{60°C} = 570 μm



Constraints

- Internal endurance run (variable profile)
- Runtime = variable
- Supply temp. 80
- Supply temp. 70 °C

Vehicle AUDI

Supply temp. 60 °C ?

- Depth of wear on shaft seal in the case of Audi Non-responsive content removed much greater than usual
- Clear indicator of poor quality fuel

EA11003EN-01826[7]

CP4 field situation worldwide VW 4-cylinder TDI

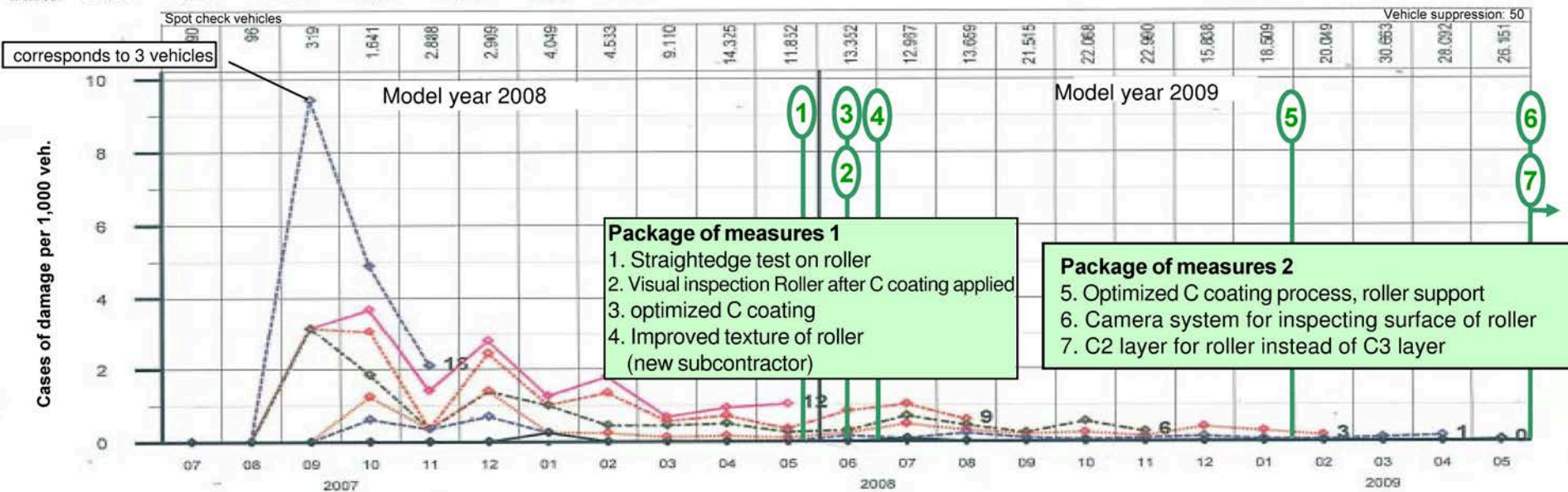
VW, market: **Non-responsive content removed**

AQUA, Active quality analysis
Status 09/09-11.09.09 12:06 PM
Source/user **Non-responsive content removed**

MY 2008 - 2010, MIS from/to : 0 - 24, Offset: 2 - 4
CNR / Groups High-pressure pump
EA 189 4-cylinder 2,0l

Confidential
Without PR numbers
CNR 2374

MY	MIS 0	MIS 1	MIS 3	MIS 6	MIS 9	MIS 12	MIS 18	MY	Exchange	BD	SA 10	SA 20	SA 50	SA 17
2008	0,0	0,1	0,2	0,6	0,8	1,1	1,9	2008	96,8 %	20,4 %	61,3 %	15,1 %	11,8 %	10,8 %
2009	0,0	0,1	0,3	0,4	0,7	1,9	1,9	2009	90,2 %	23,3 %	60,7 %	19,0 %	9,8 %	8,6 %
Diff%	-59,87	-0,12	10,01	-19,59	-14,51	65,86	-1,19				MEC ERR	NOISE	LEAK	MAJOR



Vehicle: 72.372+384.834+167.997=625.203; Sold: 71.676+386.679+117.081=555.436; UP: 48.739+244.925+100.898=394.562 MY: 2008+2009+2010=Total

Non-responsive content removed

CP4 field situation VW 4-cylinder TDI

Non-responsive content removed

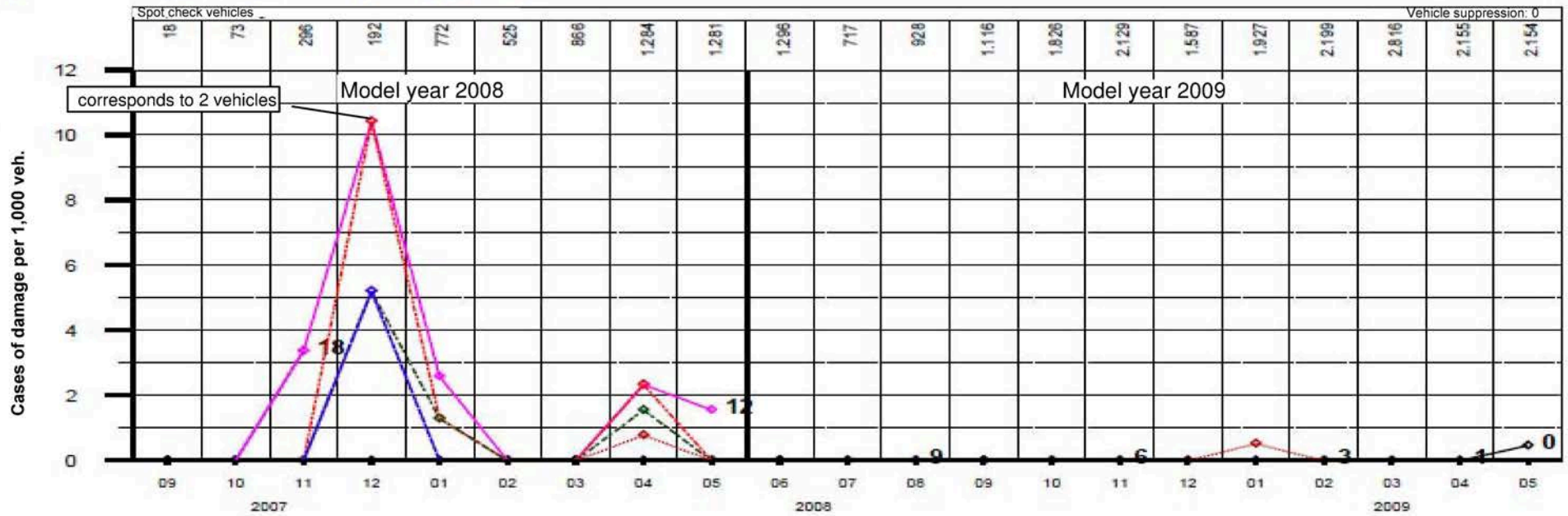
AQUA, Active quality analysis
Status 09/09-11.06.09 10:29 AM
Source/user Non-responsive content removed

VW, market: [redacted]
MY 2008 - 2010, Offset: all (Max: 4)
CNR / Groups High-pressure pump
Turbodiesel CR 4-cylinder

Confidential
Without PR numbers
CNR 2374

MY	MIS 0	MIS 1	MIS 3	MIS 6	MIS 9	MIS 12	MIS 18
2008	0,0	0,2	0,4	0,8	1,2	1,9	2,7
2009	0,0	0,0	0,1	0,2	0,3	0,3	
Diff%		-74,87	-73,79	-77,63	-70,90	-82,54	

MY	Exchange	BD	SA 10	SA 20	SA 50	SA 18
2008	100,0 %	33,3 %	66,7 %	9,5 %	9,5 %	4,8 %
2009	83,3 %	33,3 %	41,7 %	33,3 %	16,7 %	8,3 %
			MEC ERR	NOISE	LEAK	MINOR



Vehicle: 8.647+41.846+23.061-73.754; Sold: 8.619+40.026+13.915-62.762; UP: 5.146+20.478+11.802-37.426; MY 2008+2009+2010-(Total

CP41 VW R4-CR [redacted] 08-10

CP4 field situation Non-responsive content removed

Differences between CP4.1 and CP4.2.

Possible ways to interpret failure probability

CP4.2 to CP4.1 in Non-responsive content removed out of 30 : 1

- 2 : 1 Tappet modules factor 2-3
- Pump gear ratio $i = 1 : \frac{3}{4}$ factor 3

Other influential factors:

- Influence of load collective
- Influence of automatic v. manual gears
- Influence of supply temperature
- Filtering
- IV opening pressure
- ...

CP4 field situation Non-responsive content removed Further procedure (main activities)

- Deployment of Bosch field analysis team in Non-responsive content removed (importer's domicile) since 9/11/2009
Objective:
Analysis of special market-specific features in Non-responsive content removed
Tasks:
Analysis of the vehicle prior to repair (together with with Audi)
Analysis of the environment, e.g. fuel quality, etc.
Analysis of the process on the importer side (from receipt to delivery)
- 100% return of all worldwide Audi field complaints for 3 months 11/9/2009
- Analysis of production documents for pump, engine and vehicle for conspicuous veh. production data since 11/05/2009
- Procurement of 20 Non-responsive content removed "good pumps" from cars from conspicuous production date in progress
- Procurement of 20 Non-responsive content removed "good pumps" from remaining period in progress
- Analysis of system differences (application, load collective, low pressure circuit, etc.) from various vehicles A.12/2009

CP4 field situation worldwide

Backup



EA11003EN-01826[12]

CP4 field situation VW 6-cylinder TDI

Non-responsive content removed

AQUA, Active quality analysis

Status 09/09-11.06.09 4:12 PM

Source/user Non-responsive content removed

VW, Touareg, market:

MY 2008 - 2010, Offset: all (Max: 2)
CNR / Groups High-pressure pump

Non-responsive content removed

Confidential

Without PR numbers

CNR

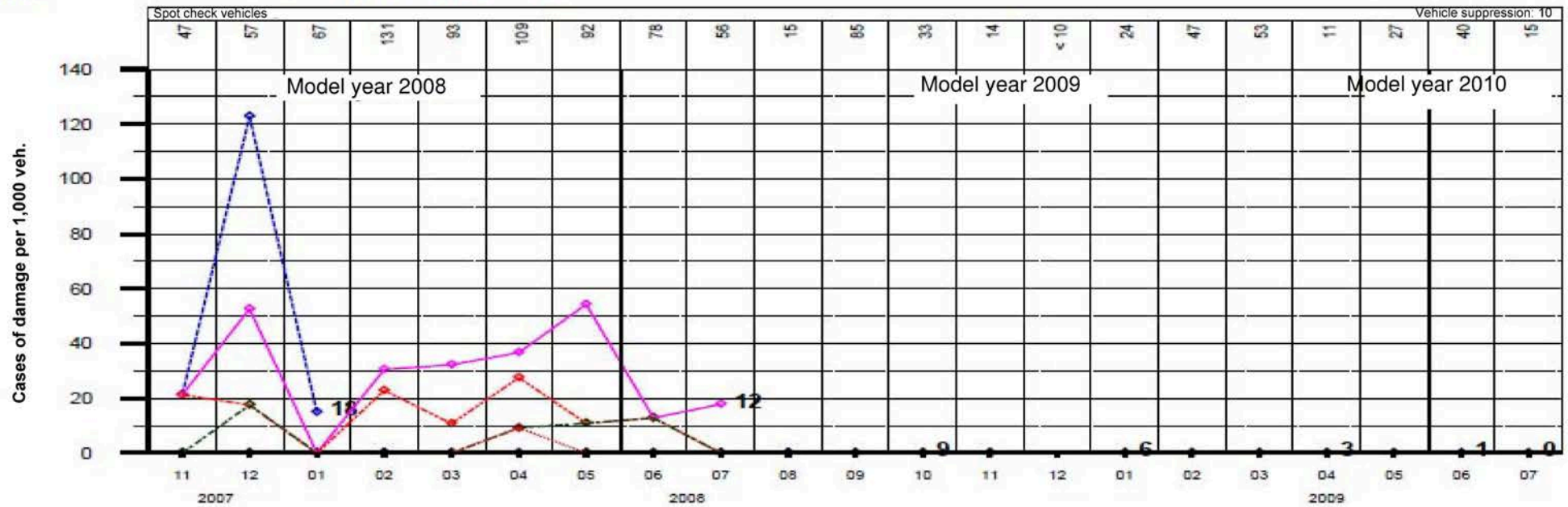
2374

CAMA|CAMB|CANA|CANB|CANC|CAND|CASA|CASB|CASC|CASD|CCWA|CCWB|CDYA|CDYB|CDYC|CGKA|CGKB

MY	MIS 0	MIS 1	MIS 3	MIS 6	MIS 9	MIS 12	MIS 18
2008	0,0	0,0	1,8	5,3	17,7	33,7	87,5
2009	0,0	0,0	0,0	2,6	2,6	12,4	
Diff%			-100	-51,30	-85,39	-83,27	

MY	Exchange	BD	SA 10	SA 17	SA 50
2008	97,8 %	50,0 %	69,6 %	23,9 %	6,5 %
2009	100,0 %	75,0 %	50 %	50 %	

MEC ERR MAJOR LEAK



Vehicle.: 993+916+265=2.174; Sold: 991+896+152=2.039; UP: 564+470+95=1.129; MY:2008+2009+2010=Total

CP42 Touareg MKB V6 08-10

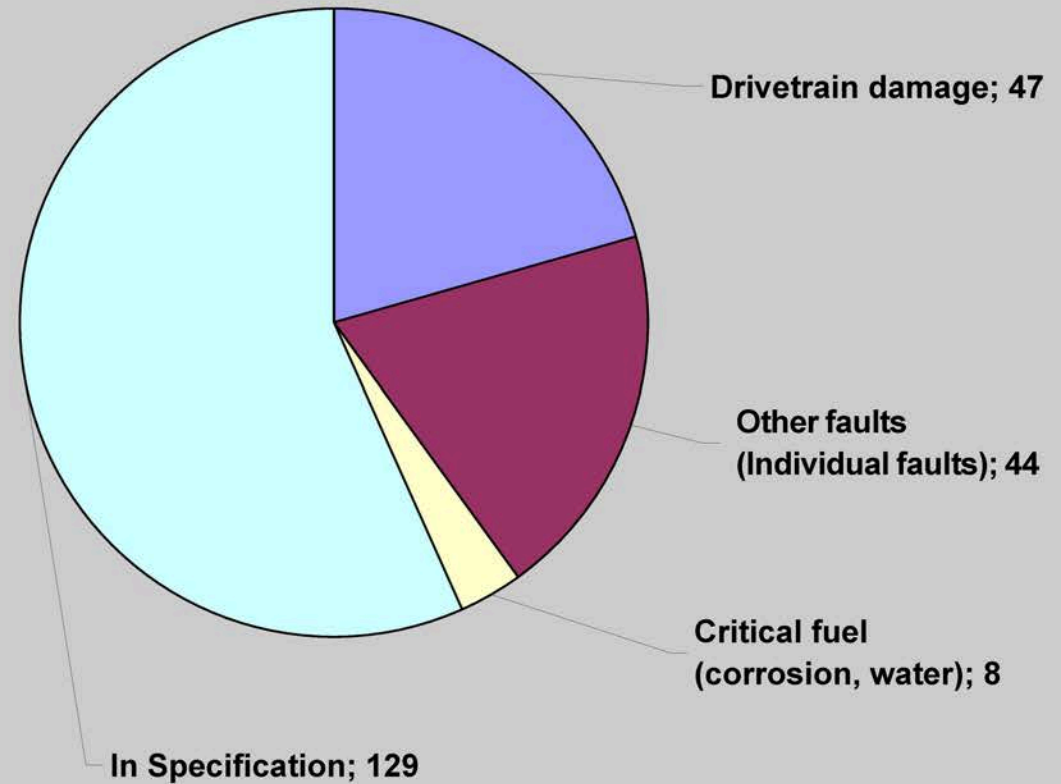
CP4 field situation worldwide VW CP4.1 complaints

VW CP4.1 commercial accounting for dealers

DC COUNTRY	Overall result
Non-responsive content removed	66
	65
	56
	28
	22
	11
	8
	7
	6
	5
	4
	4
	4
	36
Overall result	322

Source: VW purchased part list
Evaluation period 06/2006 - 09/2009

Results of findings for the pumps returned to Bosch (228)



Source: Bosch IQIS Warranty Database, status 11/03/2009

Summary

→ Status of new information since last update on 12/10/09:

Other analyses in the fuel samples from on-site actions in [REDACTED] support the results from the fuel survey in [REDACTED] and the analyses from the problematic pumps. Further detailed analysis of the fuel samples and fuel filters will be complete by 1/22/10.

Information gathered to date supports the failure mechanisms presented in the last report.

1. Tribochemical wear
2. Deposit / coatings from algae and oxidation products and therefore a significant deterioration in frictional coefficient.
3. Corrosion on the surface of cams and roller

The analysis of the reference samples from the problematic production period indicates nothing unusual in relation to drawing-related features. Other detailed analyses) will be completed by 01/13/10.

Summary

→ Further action:

For the purpose of practically confirming the damage hypotheses, reappear tests will be carried out on the hydraulic test bench with limit sample parts and fuels from 1/14/10 onwards. A test schedule has been drawn up.

Measures to increase) are defined and their effectiveness will be verified with the same test parameters. Detailed plans will be drawn up dependent on the reappear tests.

Return of the requested 40 good pumps from [redacted] and 20 good pumps [redacted] is agreed to WK 03/2010.

Mechanism whereby the tappet is turned, roller lifted from the camshaft depending on the engine vibrations on the pump drive, is to be examined on the engine with AUDI. Technical meeting for this purpose 01/12/2010

Operating conditions / Environment / System

Local FCT team in Non-responsive content removed

Status: 18 vehicles examined on-site and 4 systems received from damaged parts stores. Complete fuel injection systems including fuel filters and fuel samples have been sent to Bosch for analysis.

Result: 12/12 cases of drivetrain damage from local actions.
2/4 cases of drivetrain damage from damaged parts stores systems.
7/7 analyses of low pressure circuits showed nothing unusual.

Special features: In 3 vehicles, free water found in fuel.
4 vehicles with deposits in the tank (swirl pot)
- 1x reddish, sticky coatings,
- 1x white flocculation,
- 2x dark/ black particles





Fuels Findings

Status: 20 fuel samples analyzed from [redacted]
10 fuel samples analyzed from [redacted]

Result: Survey:
Oxidation stability was found to be outside the tolerance in 4 fuel samples and the TAN (acid coefficient) is generally 2-3 times higher than usual, probably due to spilled biodiesel.

FCT:
In 2 fuel samples oxidation stability was outside the tolerance.
In the first analysis of the coatings, algae were found in the fuel.
Other deposits from other pumps are under analysis and probably also contain algae. Fuels containing microorganisms always contain free water. This is also consistent with the slight acidification of another fuel sample from the same damage scenario. Algae develop acids as metabolized material.





Summary of analysis results

Result of analysis of [redacted] pumps

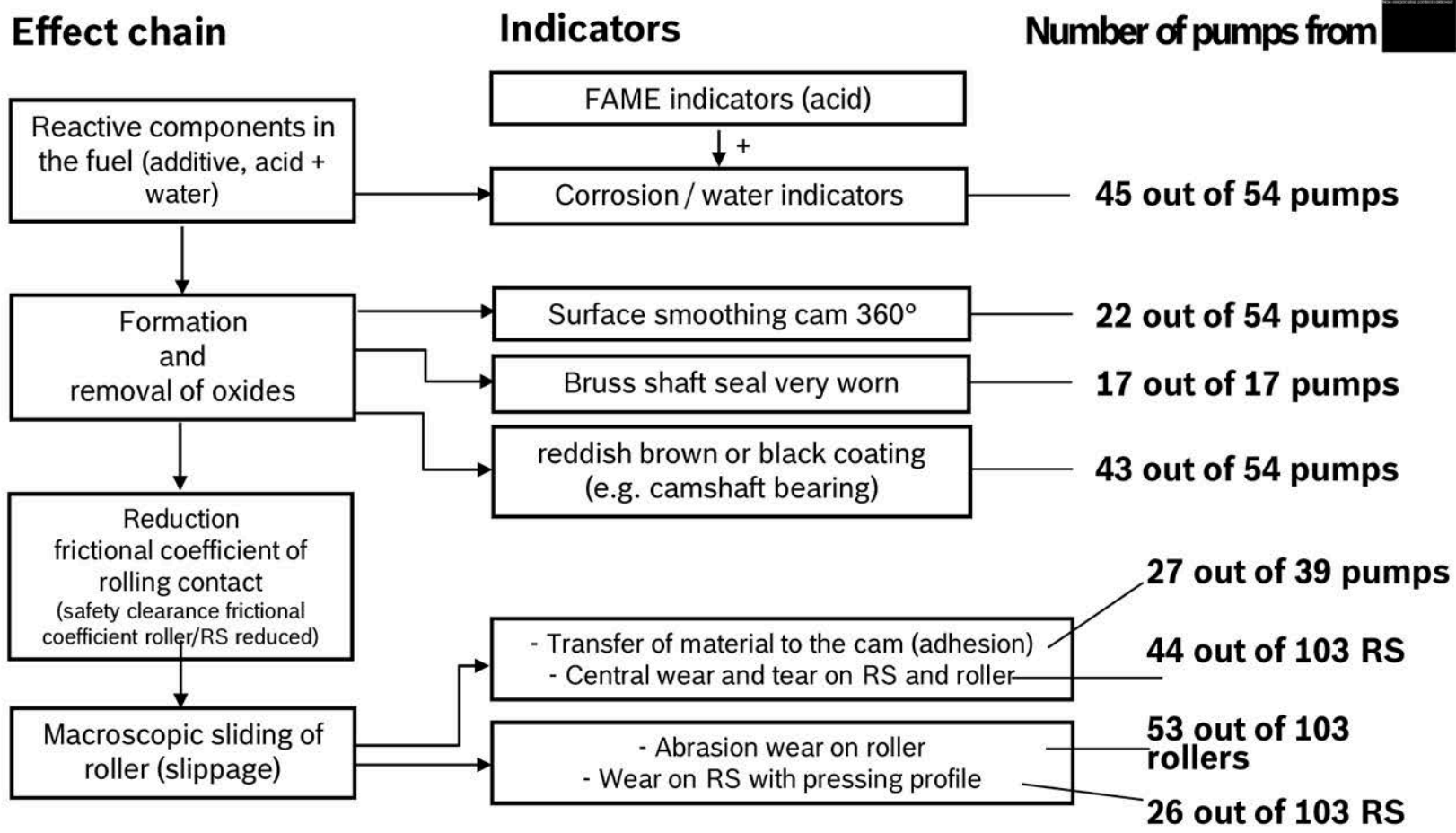
- 17 out of 17 Bruss shaft seals stronger worn than with EN590
- 45 out of 54 pumps have signs of corrosion
- 11 out of 54 pumps have brown fuel deposits

- 45 out of 52 drivetrain failures have turned tappet bodies
- 22 out of 54 pumps have surface smoothing on the cam
- 9 out of 52 drivetrain failures have fatigue damage on the cam
- 3 out of 54 pumps have pitting on the cam

- 44 out of 103 roller supports are worn in the middle
- 29 out of 103 roller supports are completely worn
- 26 out of 103 roller supports are worn in the shape of the press profile

- 1 x fuel sample tank: Algae
- 1 x wash mark with striations

Failure hypothesis 4: Fuel additives -> Tribochemicals



Failure hypothesis 6: Fuel viscosity -> Boundary friction

Effect chain

Fuel additives reduce viscosity e.g. water, additives

Threshold value components

Boundary friction Sliding/rolling contact

Sluggish roller Roller slippage

Indicators

Water indicators

Bruss shaft seal very worn

Sink marks in Kaco camshaft seal

Roller texture

Rz C coating RS

RS texture

RS straightness

Number of pumps from

45 out of 54 pumps

17 out of 17 pumps

8 out of 54 pumps

3 out of 54 pumps

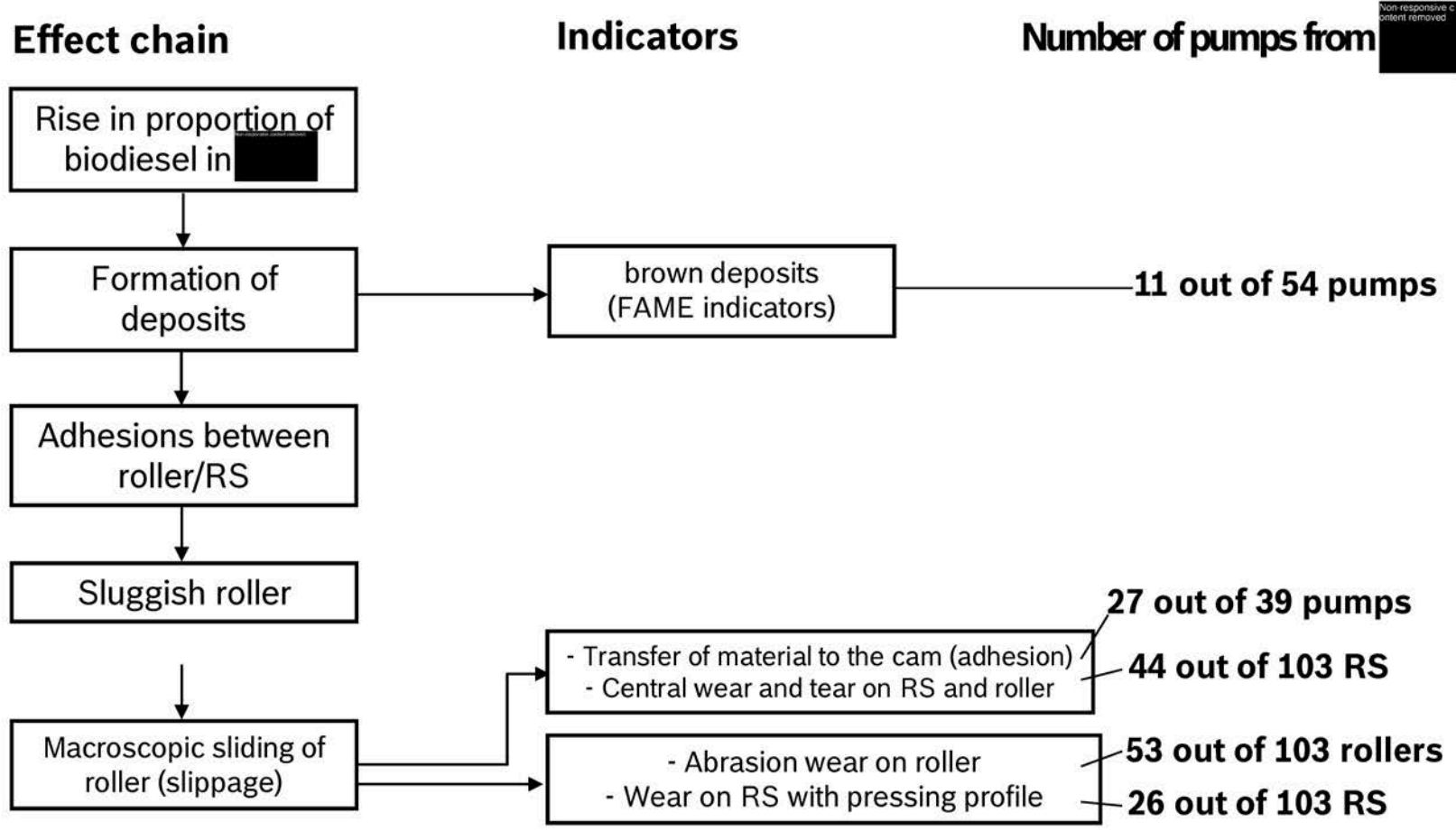
27 out of 39 pumps

44 out of 103 RS

53 out of 103 rollers

26 out of 103 RS

Failure hypothesis 3: Biodiesel -> adhesions



Non-responsive content removed

Operating conditions / Environment / System

Procure 40 good pumps

Status: Vehicles identified, importer to contact owners. Importer has new pumps for replacement.

Result: t.b.d.

Further action: First returns not expected before WK 03/2010.

Special features: none



AQUA: Active quality analysis
 Status: 10/09-20.11.09 09:14
 Source/user: [Redacted]

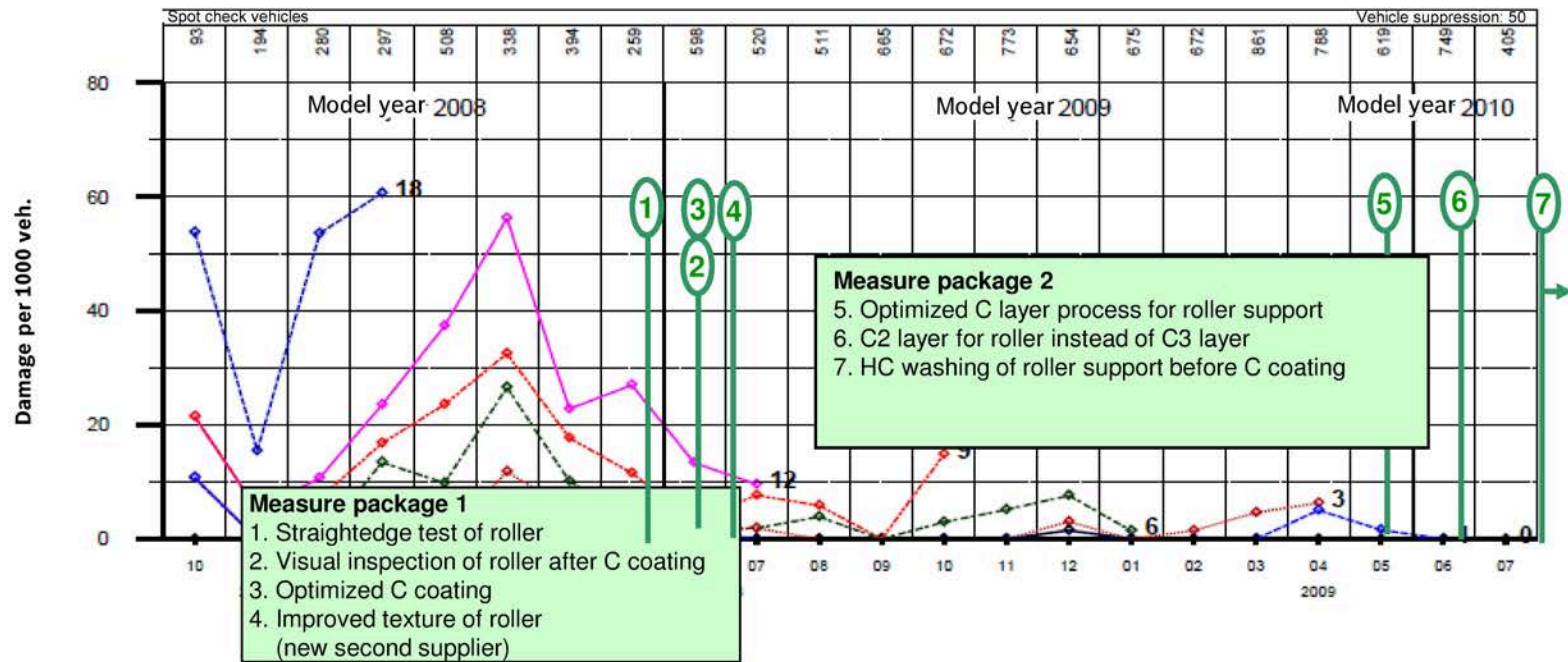
Audi, market: [Redacted]

Confidential
 without PR numbers
 CNR 2374

MY 2008 - 2010, Offset: all (max. 2)
 CNR / Groups: High-pressure fuel pump

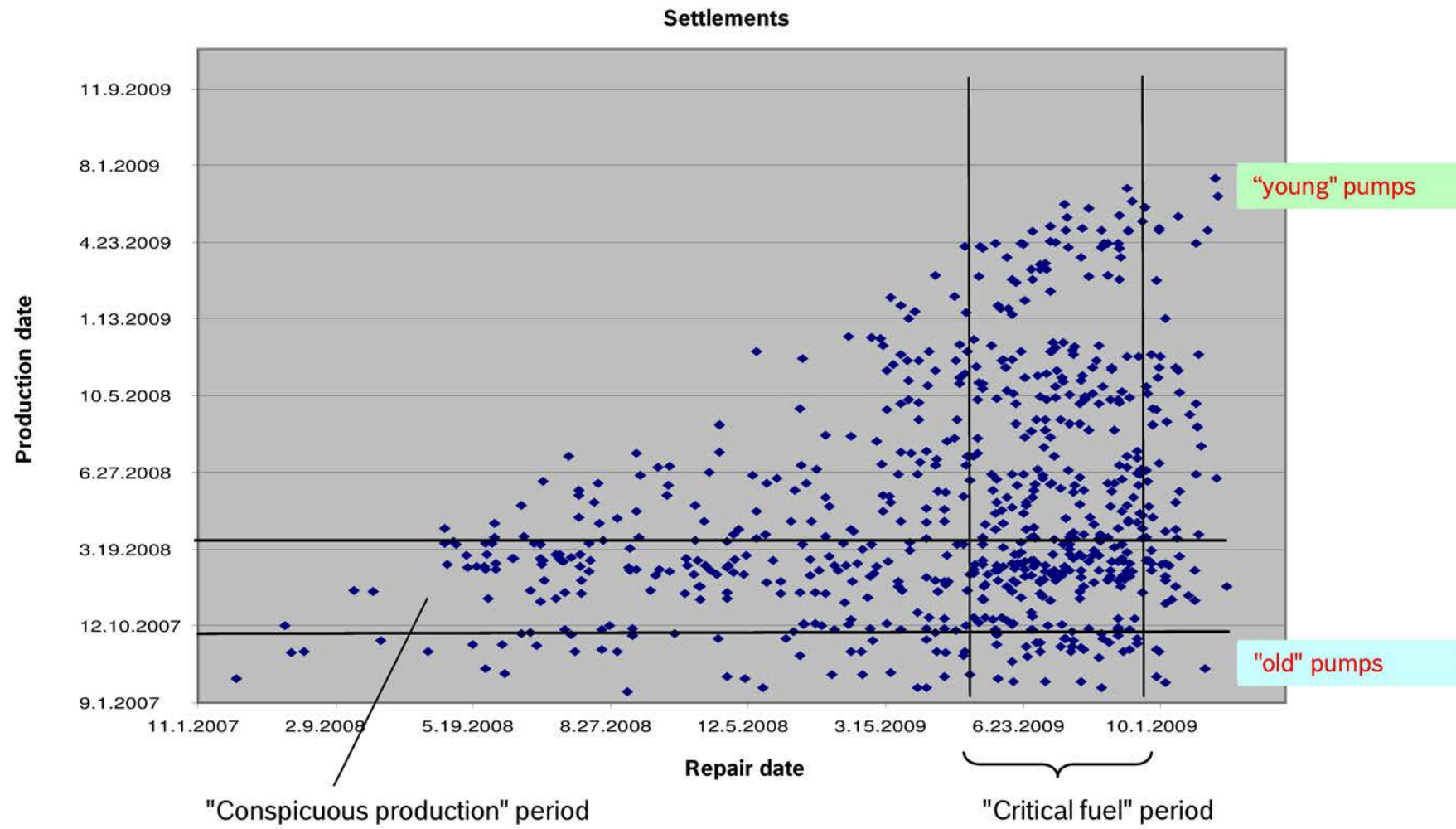
CAMA|CAMB|CANA|CANB|CANC|CAND|CASA|CASB|CASC|CASD|CCWA|CCWB|CDYA|CDYB|CDYC|CGKA|CGKB

MY	MIS 0	MIS 1	MIS 3	MIS 6	MIS 9	MIS 12	MIS 18	MY	Exchange	BD	SA 10	SA 17	SA 50	SA 18
2008	0,0	1,7	3,9	10,3	18,0	27,8	73,8	2008	100,0 %	79,7 %	74,9 %	15,0 %	7,5 %	2,1 %
2009	0,1	0,9	1,9	4,3	8,2	13,8		2009	96,0 %	85,3 %	81,3 %	14,7 %	2,7 %	1,3 %
2010	0,0	0,0	5,7					2010	100,0 %	100,0 %	50 %	50 %		
Diff%	-100	-100	194,41											



Vehicles: 3.389+12.041+5.434-20.864; Sold: 3.386+11.357+3.740-18.483; UP: 2.335+7.730+2.800-12.865; MY: 2008+2009+2010 = Total

CP42 AU all MKB V6 08-10



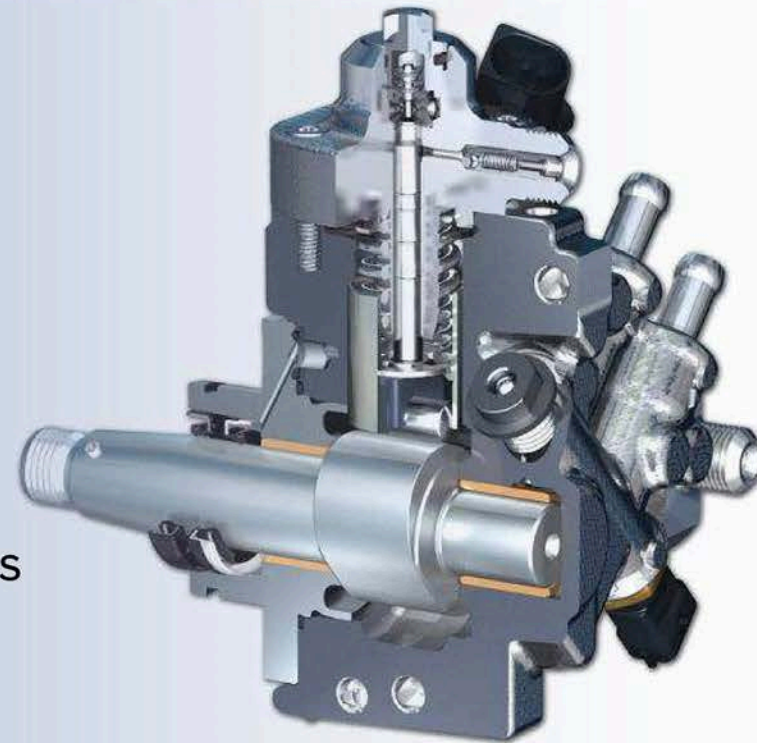
Diesel Systems



Audi meeting on 02/12/2010

Non-responsive content removed

1. Ishikawa of influencing factors
2. Analysis of failed pumps / fuels
3. Component sensitivity
4. Good pumps
5. Hypothesis
6. Anti-wear package 1
7. Proof of robustness: Stribeck curves
8. Assessment of measures



Diesel Systems

1

Confidential Non-responsive content removed

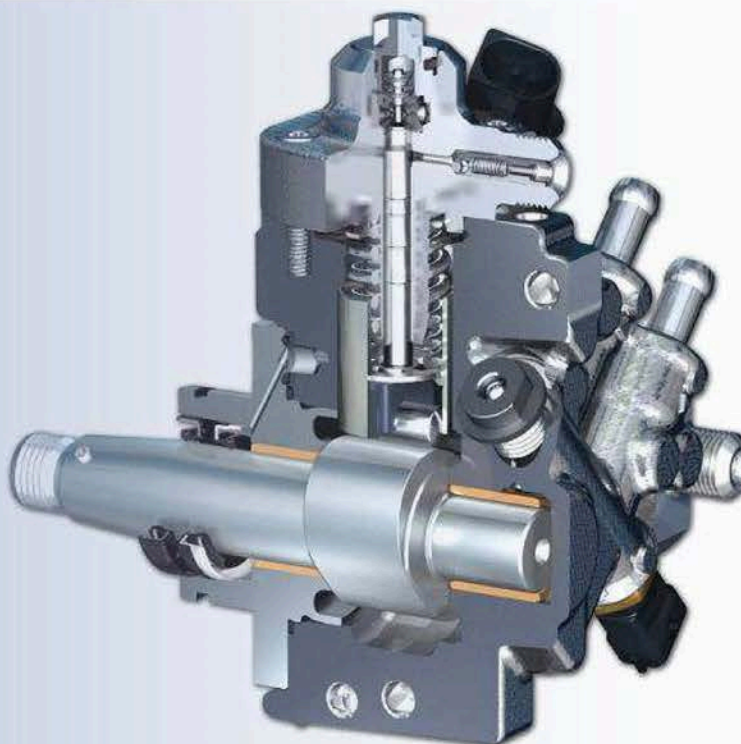
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BOSCH

1) Ishikawa of influencing factors

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Diesel Systems

2

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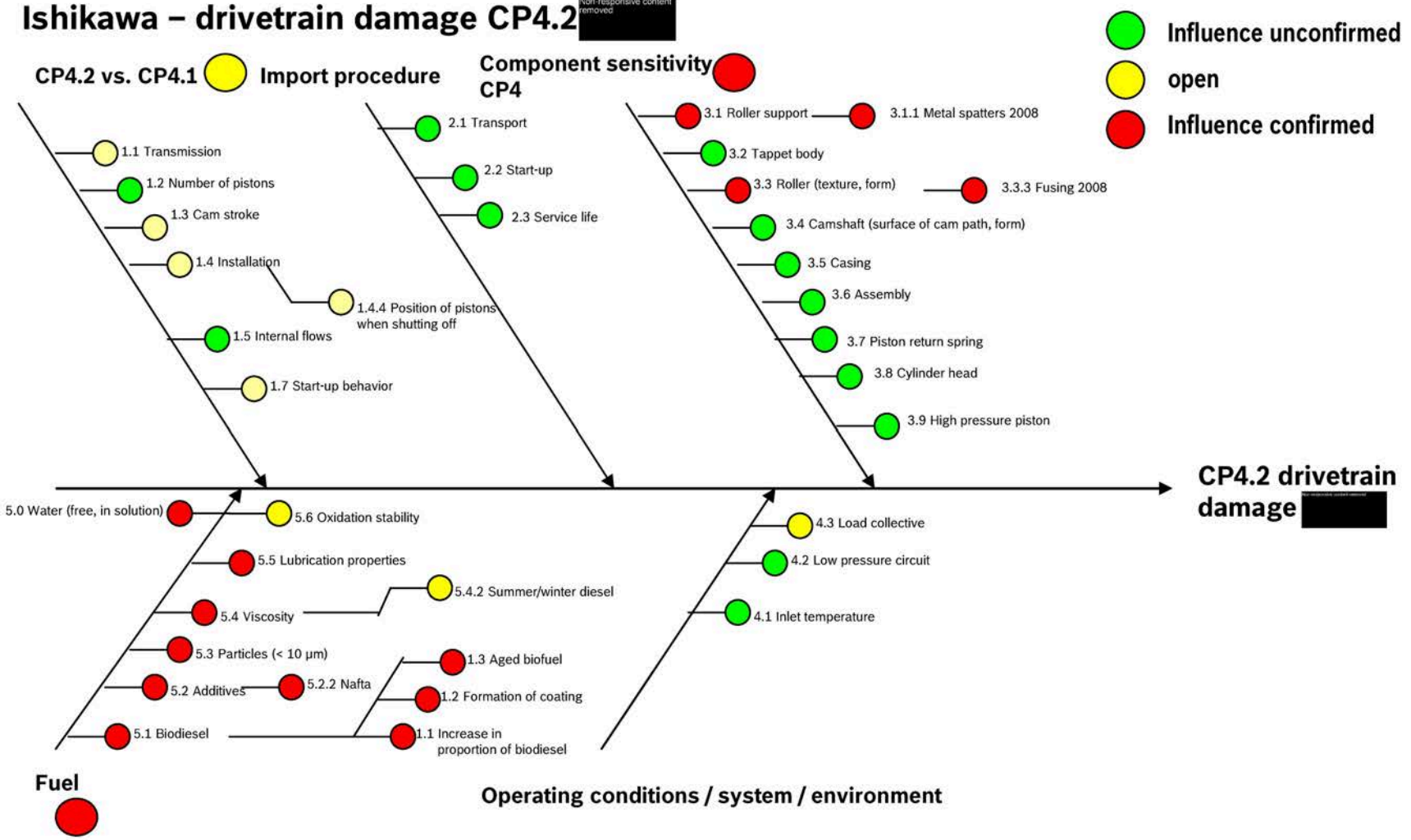


BOSCH

Audi meeting on 02/12/2010

Ishikawa – drivetrain damage CP4.2

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Diesel Systems

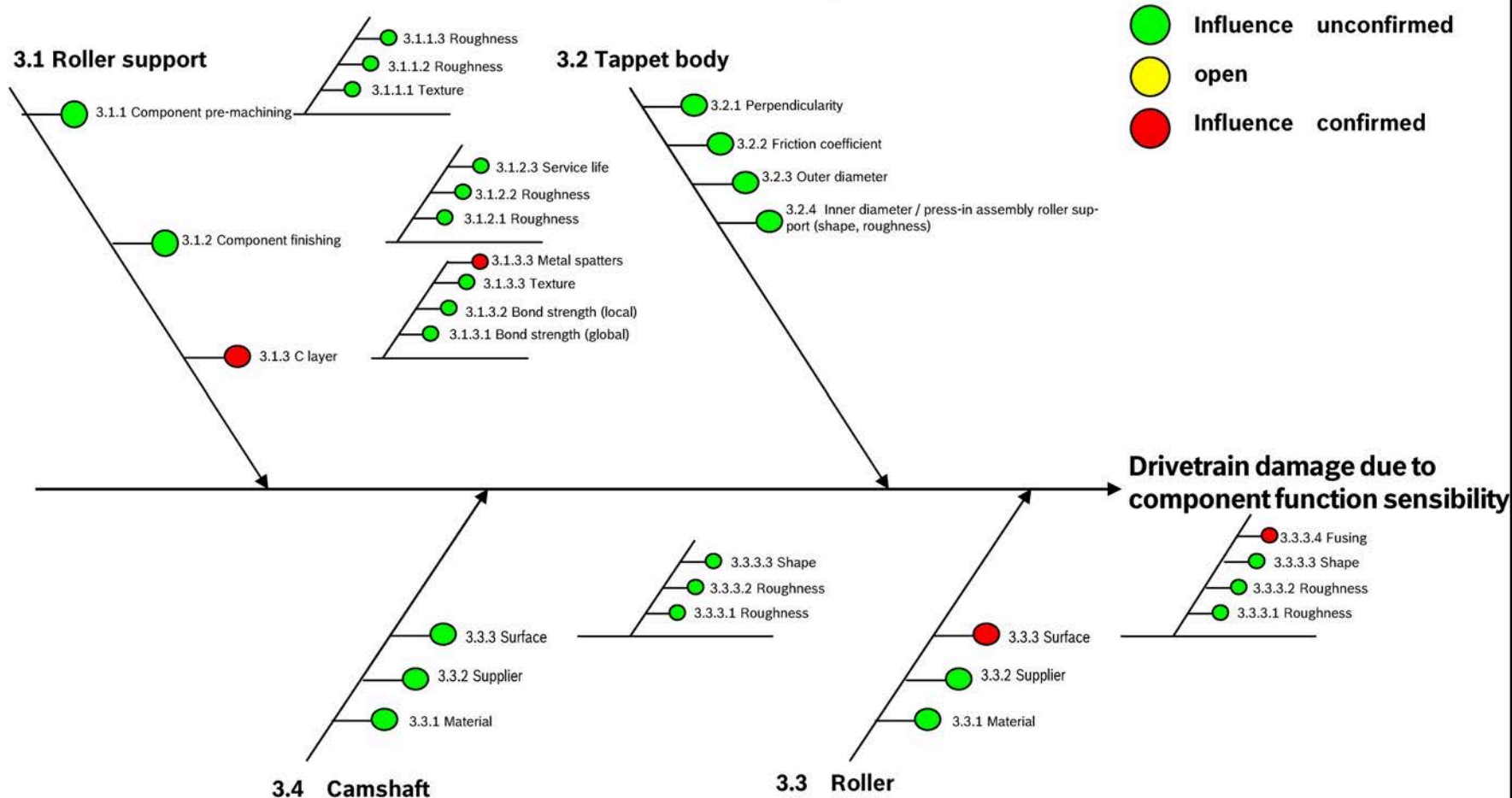


BOSCH

Audi meeting
Audi meeting on 02/12/2010

Ishikawa - drivetrain damage CP4.2

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Diesel Systems



BOSCH

Audi meeting on 02/12/2010

Summary of areas of action from Ishikawa:

1. Fuel influence
2. Component sensitivity: Metal spatters / fusing
3. Differences between CP4.2 – CP4.1 in application and design

Diesel Systems

5

Confidential **Non-responsive content removed**

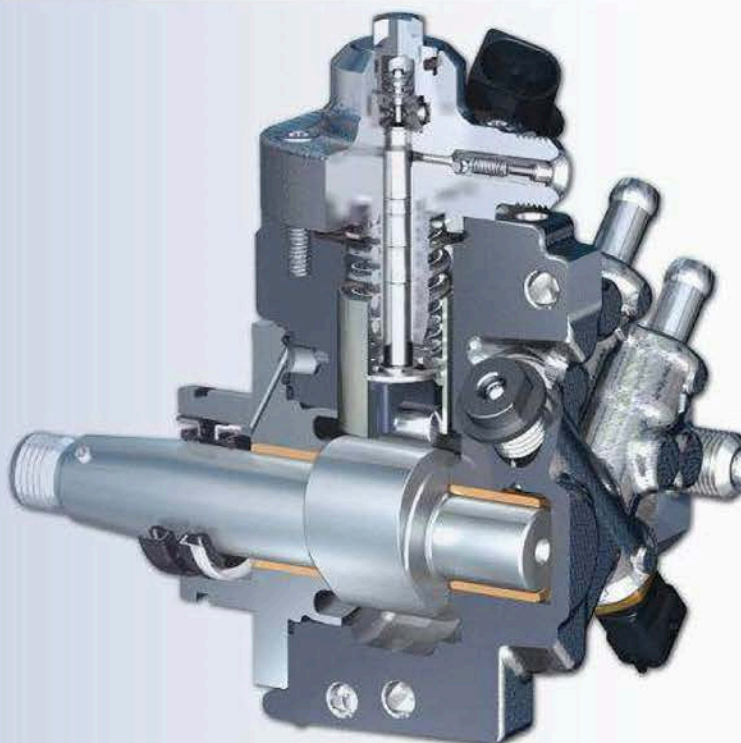
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BOSCH

2) Analysis of failed pumps / fuels

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Diesel Systems



Audi meeting on 02/12/2010

Determination of causes for failure focus Non-responsive content removed

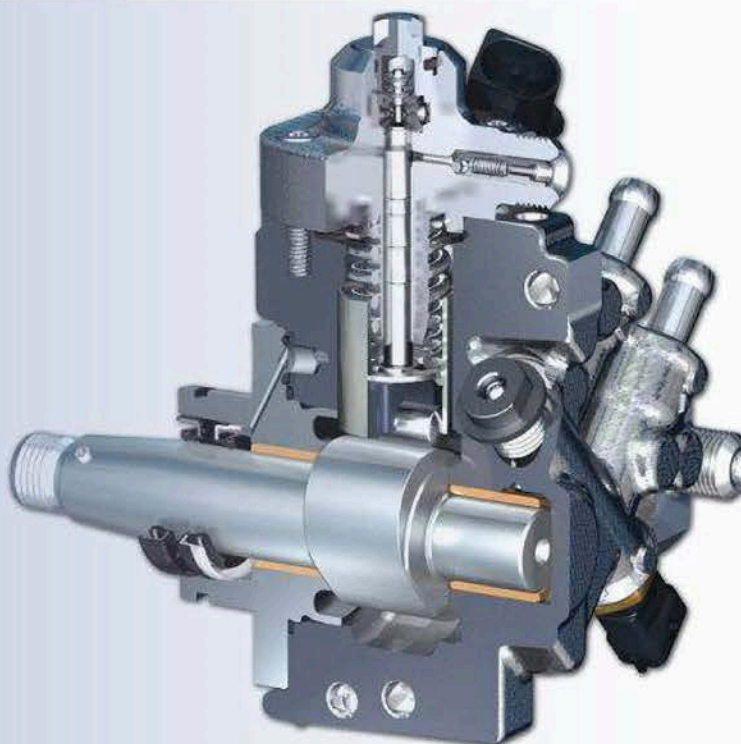
Analysis of field pumps and fuel samples from Non-responsive content removed

- FAME deposits 11 of 54 pumps
- Corrosion indicators, evidence of water 45 of 54 pumps
- Free water in fuel sample 4 of 24 samples
- Cellulose residue, algae, glycerin 9 of 24 pumps
- Heavy wear of shaft seal 17 of 17 pumps
- Good pumps with preliminary damage - Non-responsive content removed 6 of 13 pumps



3) Component sensitivity

Non-responsive content removed

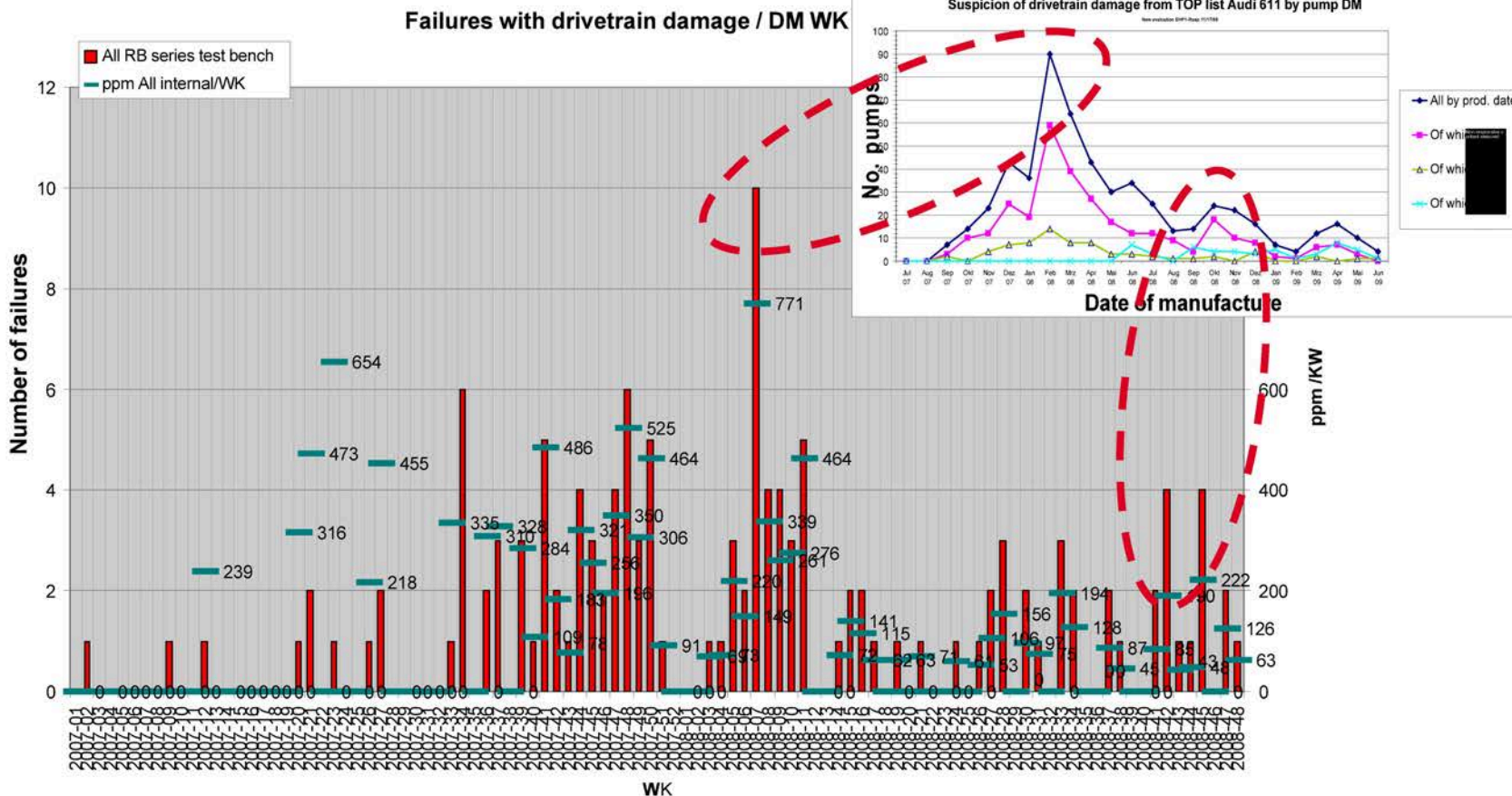


Diesel Systems



Audi meeting on 02/12/2010

Overview of failures, internal test bench & Field (failure peaks)



-> Increased internal test bench failures correlate with increased field failures

Diesel Systems



BOSCH

Audi meeting on 02/12/2010

Component sensitivity

1. Metal spatters in roller support C3 coating

Metal spatters significantly reduced through optimization of plants 5/2008 Sensitivity to small metal spatters with EN590/ BDF570 verified from 5/2008.

2. Roller with fusing

To select rollers with fusing, the straightedge test was introduced in 5/2008.

The conversion of the roller edge end to C2 in 5/2009 eliminated the fusing.

Diesel Systems

10

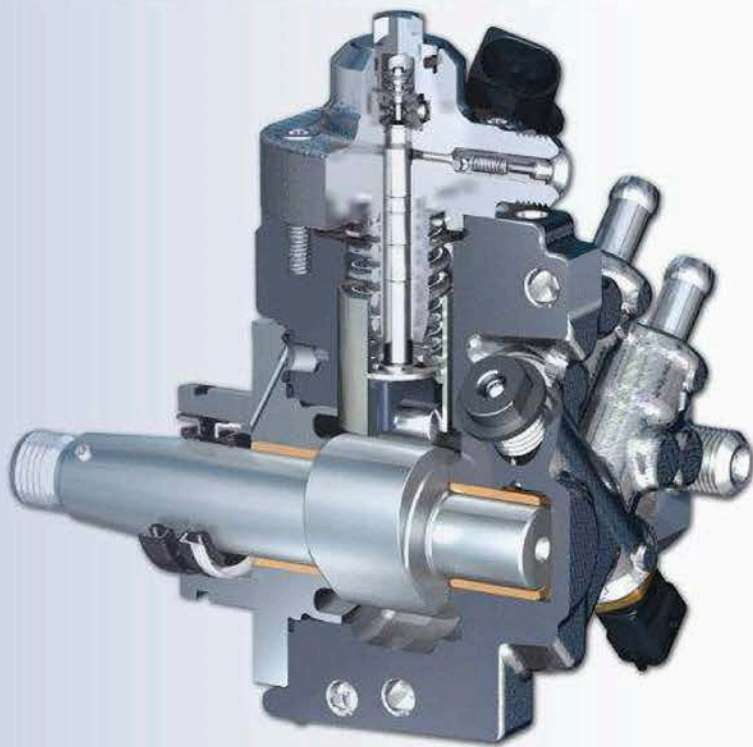
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BOSCH

4) Good pumps

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Diesel Systems

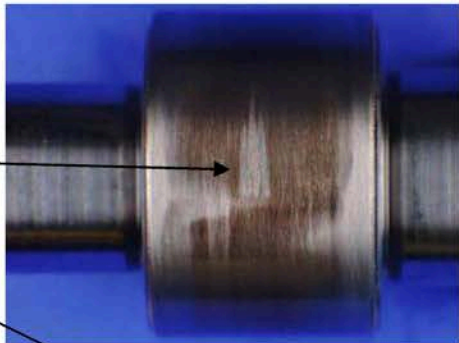
Audi meeting on 02/12/2010

TF AUDI [redacted] Good pump (2009-CP4_0685)

5,125 km (no failure)

Summary analysis results

- Transfer of material from roller to cam
- Braking flat from non-starter



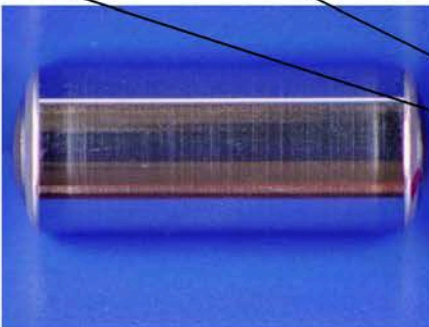
Interpretation:

Roll does not start when engine is started (sluggish)

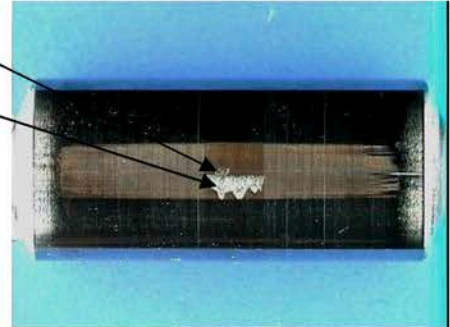
6 of 13 OK pumps from [redacted] have the same symptoms.

Preliminary damage does not necessarily result in failure (failure primarily due to continued driving with poor fuel).

Experience from initial reappear tests.



Left roller

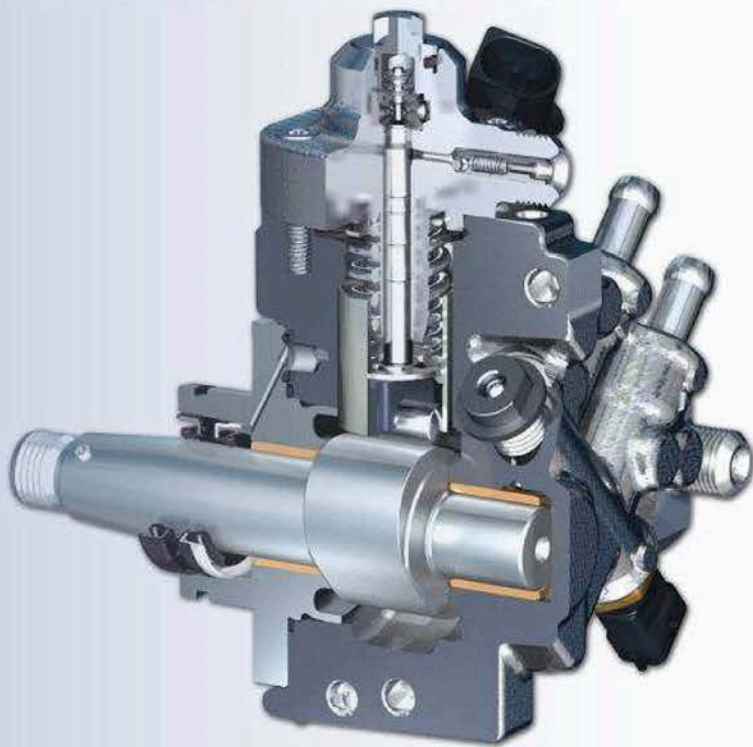


Right roller



5) Hypotheses

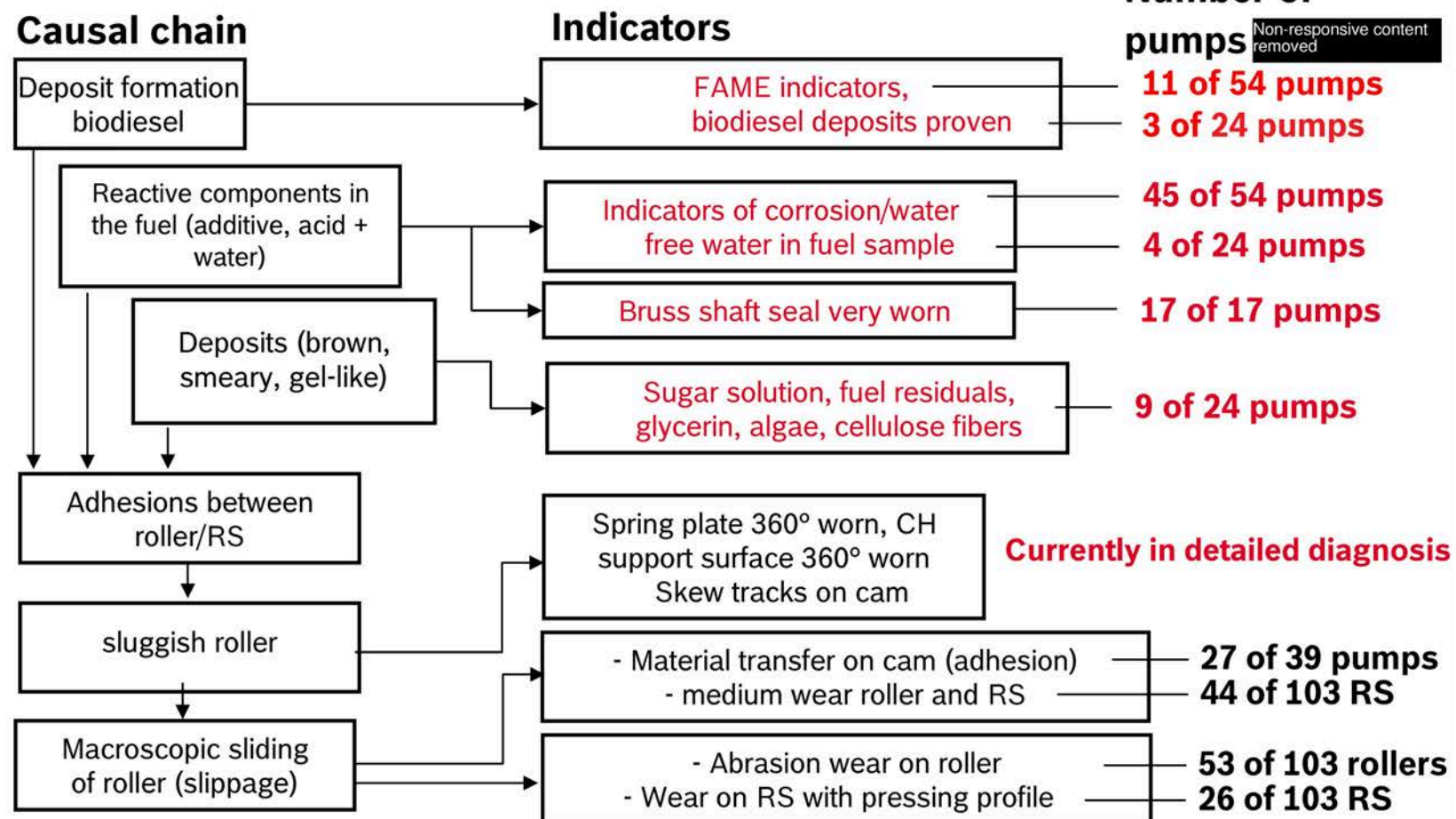
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Potential damage based on hypotheses 3 and 4 (aged fuel with presence of water)



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Differences between CP4.2 and CP4.1

Hypotheses: Based on poor start-up of the pump (analysis of good pumps), the following hypotheses for the differences can be examined:

1. Different start/pressure build up speed between 4-cylinder and 6-cylinder engine -> start-up worse with poor-quality fuels
2. Different position of roller on cam when shutting down engine. Mounting situation of pump on 4/6-cylinder engine
3. Belt tension during pump start-up (pre-tension)
4. Different flow patterns in pump interior (no influence)

Further work:

High-speed camera & start-up examinations with poor quality fuel 2/26/2010

Damage case with stopped (seized) roller can be reproduced with reappear test and Arctic Diesel.

Diesel Systems

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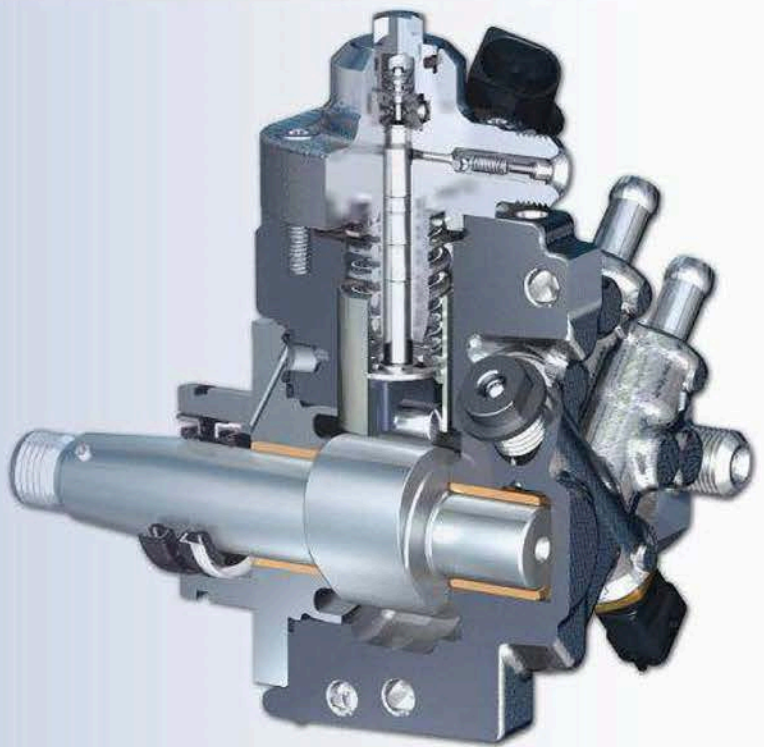
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6) Anti-wear package 1

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Anti-wear package 1 (task; features)

Assignment

Increase robustness of drivetrain by increasing the height of the lubricating film between roller support bore and roller.

Features of anti-wear package 1

- 1) Reduction of roller support roughness in combination with change to C2 layer on roller support.
- 2) Reduction of roller play by shifting average tolerance and tolerance range of roller support bore.

Results from simulation: Increase in robustness of ~ 50%*

(*compared to today's borderline tolerances)

Further work: Verification & RP1

by WK8

Diesel Systems

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Introduction of anti-wear package 1 in current series

Status

Basic test of C2.1 layer incl. release for 3 customers with EN590 & ASTM975 (US fuel) available. No engine start/stop test for ASTM975. Verification with poorly lubricating fuel (kerosene, Arctic, aged biodiesel, ...) started.

Open items

Verification of reduced play

- Risk assessment with DRBFMpositive done
- Borderline part provision done
- Functional & endurance runs see schedule



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Verification of RP1 in overload tests

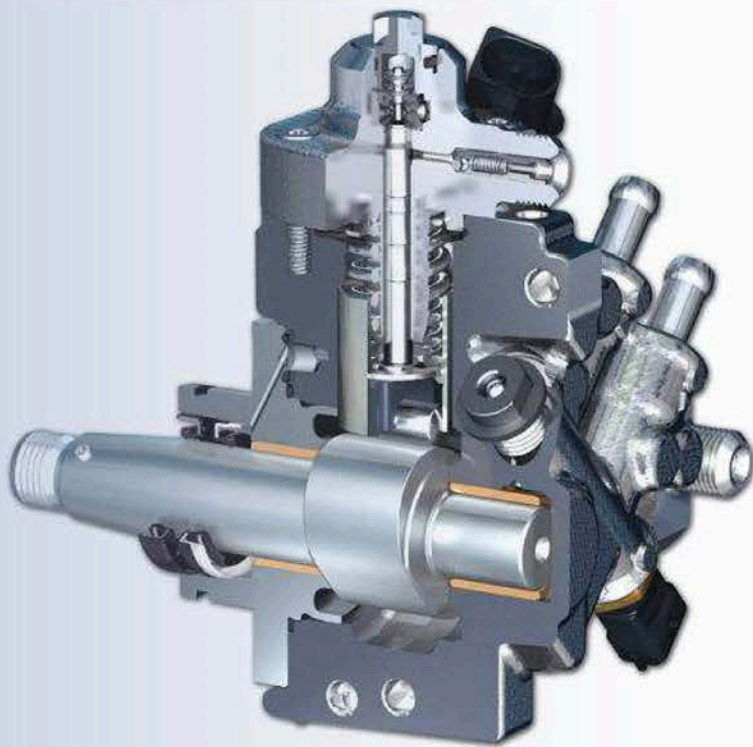
Level	Target number	Status	End date
Tappet "good" after visual inspection of C3 RS	2	150h	WK5
Tappet "bad" after visual inspection of C3 RS	2	150h	WK5
Best of series C2.1 with RP1 (24µm)	2	150	WK6
	20		WK
	36	400h	WK
	12	1,000h	WK
	24	2,000h	Done WK
	12	400 h	Done WK

Will be revised & submitted later



7) Robustness increase based on Stribeck curves

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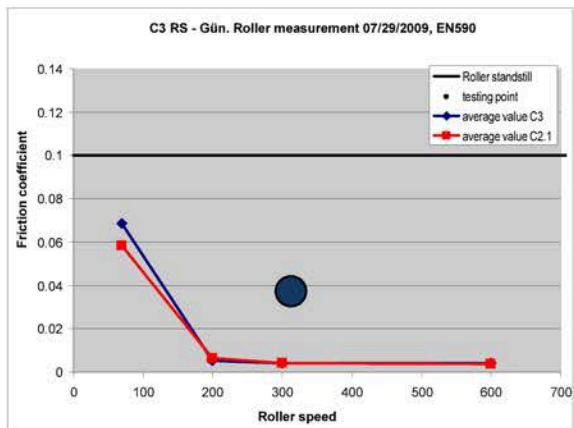
Diesel Systems



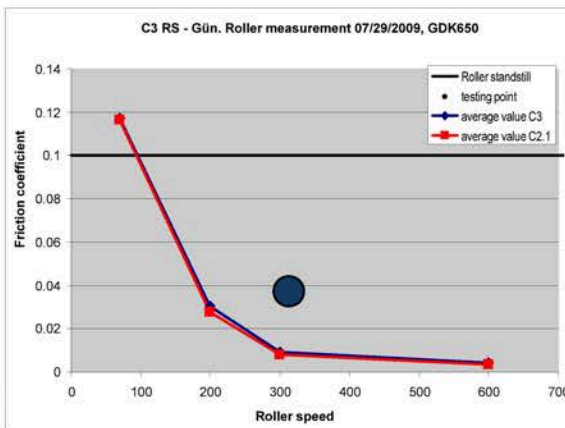
Audi meeting on 02/12/2010

Comparison of layer system* C3-C2.1 on friction coefficient test bench at

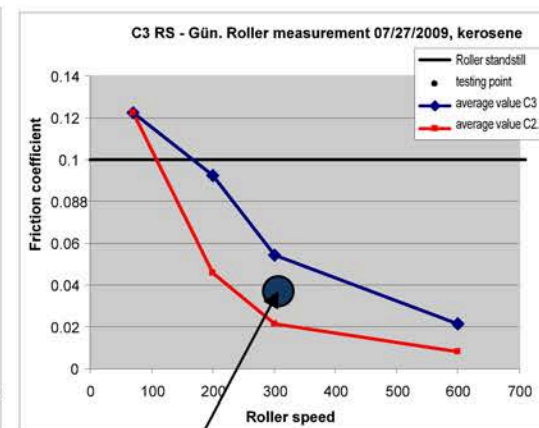
EN 590



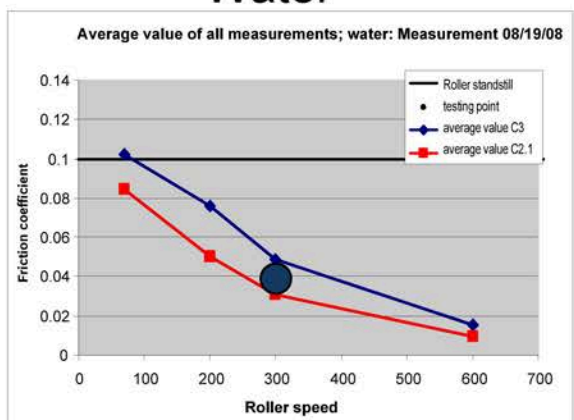
BDF 650



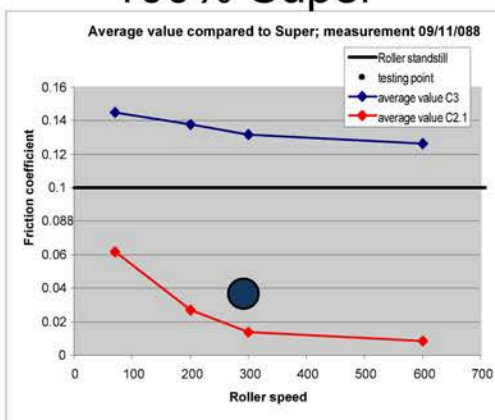
Kerosene



Water



100% Super



Assessment criterion:
friction coefficient

*average comparable play

Diesel Systems

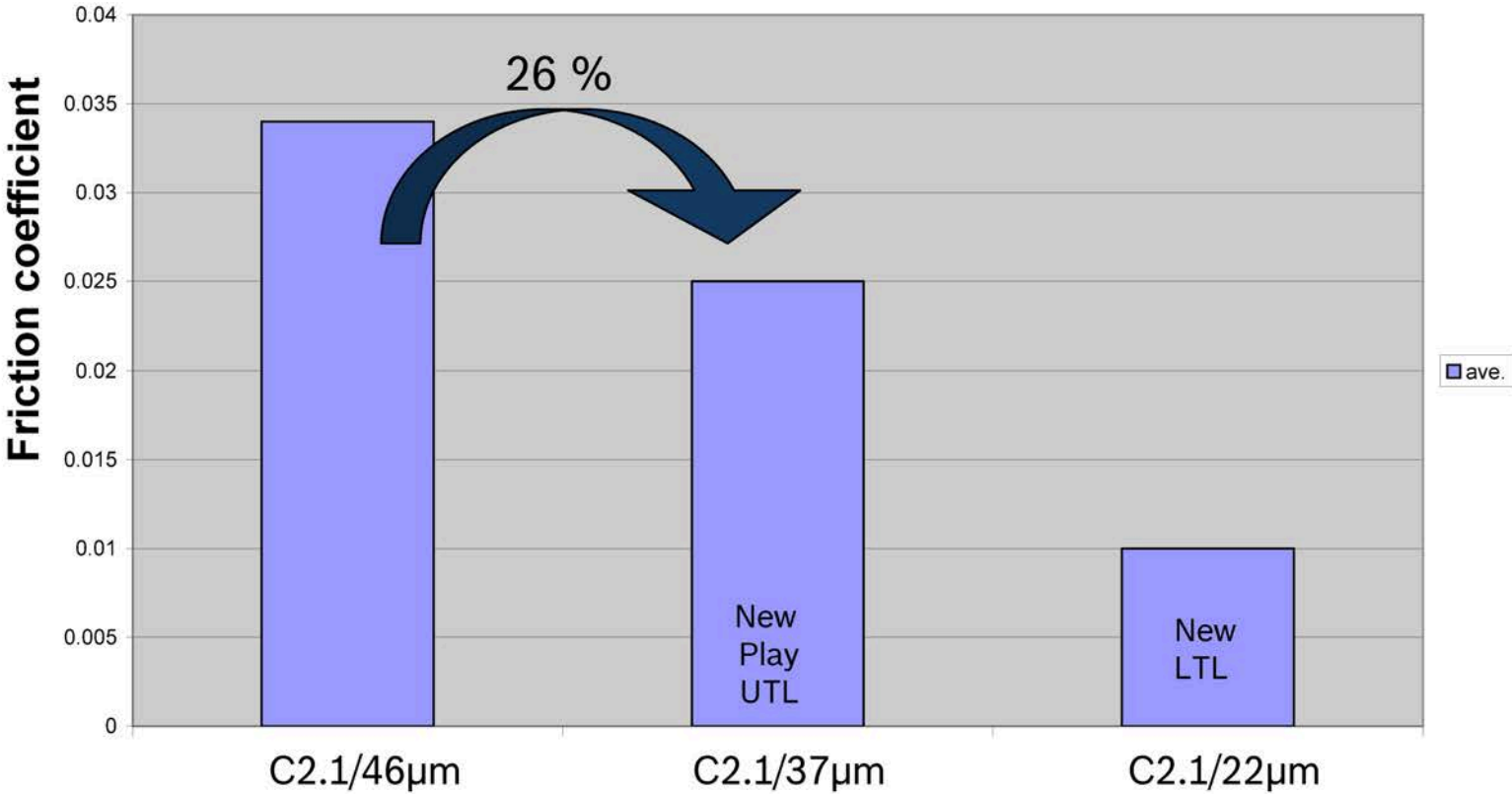


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Examination with viscosity 1.4mm²/s @40°C (Arctic Diesel)

Testing point 300rpm

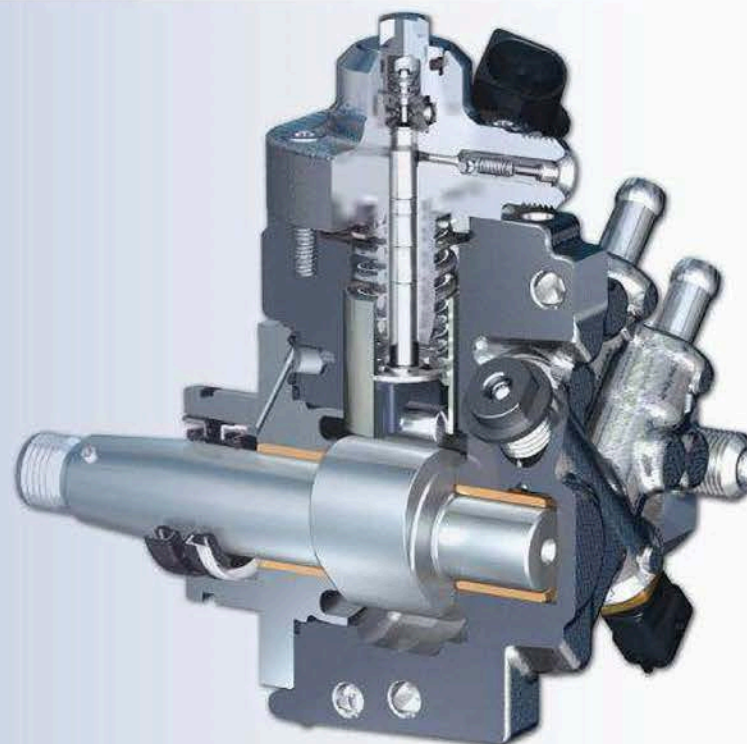


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8) Assessment of measures

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Audi meeting on 02/12/2010

Effectiveness of robustness system:

Fuel quality	Problem	Series production	RP1	LLPx*	Water separator
EN590 / BDF520		+++	+++	++	
BDF650	Lubricity	(+)**	+++	+	
Kerosene	Viscosity	-	(+)	+	
Aged fuel	Gumming Lubricity	-	(-)	+*	
Water > 200ppm	Viscosity Lubricity Corrosion	-	-	-	+

*LLPx: Dependent on examination of differences between Cp4.2 and CP4.1, as well as results of FCF and WCF test with RP1. Definition of measures in the next 8 weeks.

** with C coated piston (USA)



Summary: Task Force CP4 Drivetrain

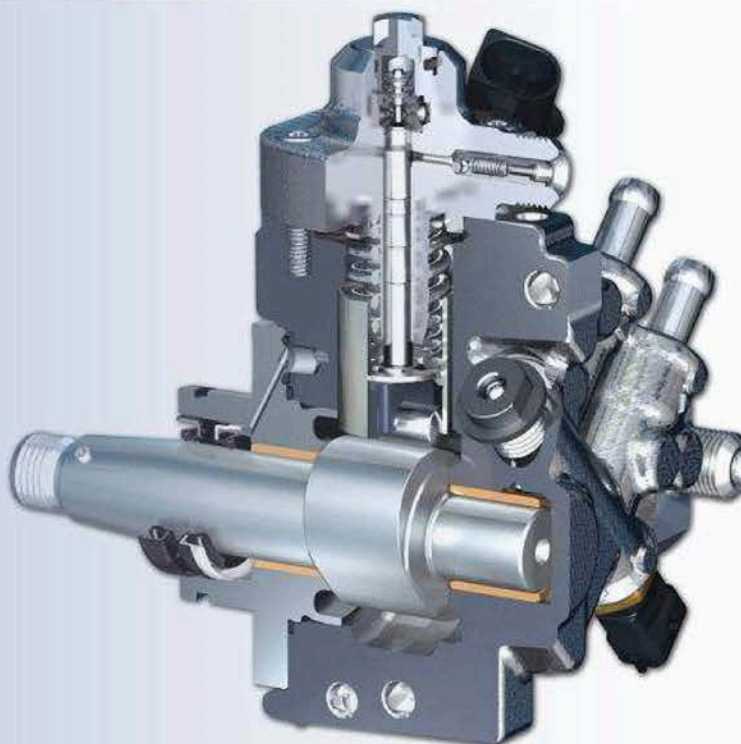
1. Audi field data
2. Field data / Ishikawa of influencing factors
3. Analysis of failed pumps / fuels in [REDACTED]
4. Component sensitivity
5. Good pumps [REDACTED]
6. Hypotheses [REDACTED]
7. Comparison CP4.2 and CP4.1
8. Possible measures (anti-wear package 2)
9. Anti-wear package 1 to improve durability with poor viscosity / lubricity
 - 9.1 Proof of robustness based on Stribeck curves
 - 9.2 Endurance runs with C2 / C3

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1) Field data Audi

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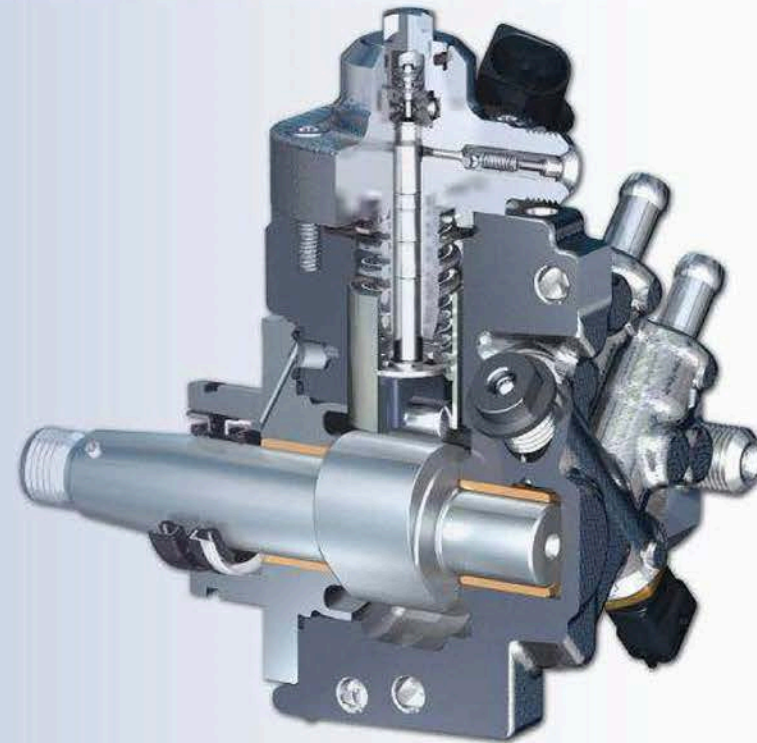
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2) Field data & Ishikawa of influencing factors

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AUDI - CP4 field situation in [redacted]

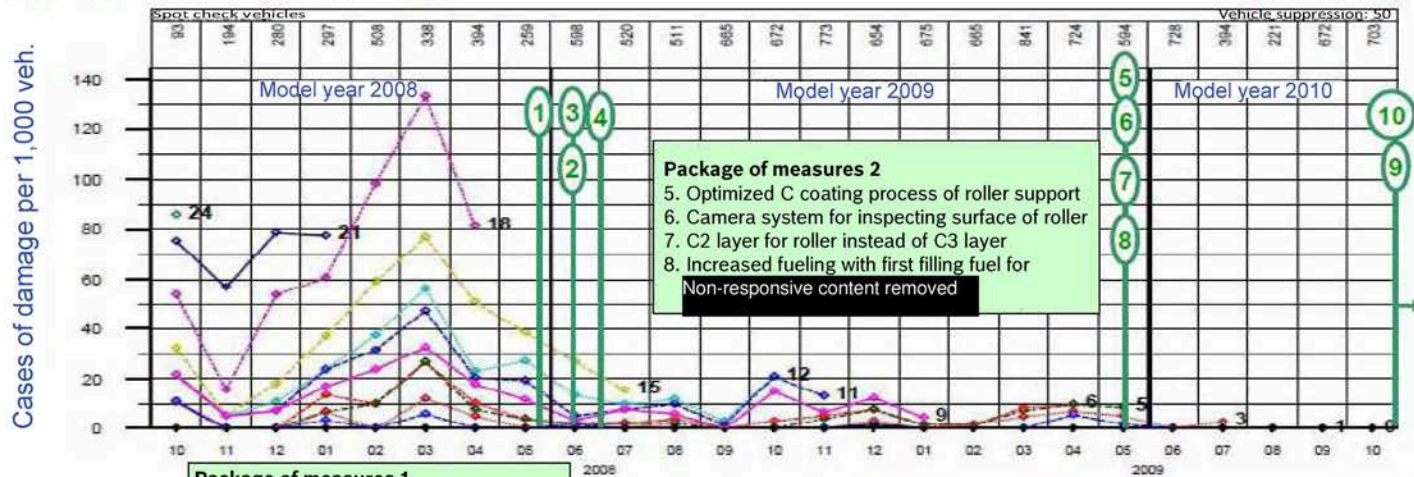
Status: 2/3/2010

AQUA, active quality analysis
 status 12/09-01/16/10 08:43
 Source/User [redacted]

Audi, *, market: [redacted]
 MY 2008 - 2010, Offset: all (Max: 2)
 CNR / Groups High-pressure pump

Confidential
 Without PR numbers
 CNR 2374

MY	MIS 0	MIS 1	MIS 3	MIS 5	MIS 6	MIS 9	MIS 11	MIS 12	MIS 15	MIS 18	MIS 21	MIS 24	MY	Exchange	BD	SA 10	SA 17
2008	0,0	1,7	3,9	9,0	10,3	18,0	23,6	27,8	44,5	78,5	103,2	119,7	2008	100,0 %	81,3 %	75,6 %	14,2 %
2009	0,1	0,9	1,9	3,8	4,4	7,8	11,7	14,3	23,0				2009	97,2 %	80,0 %	79,4 %	13,1 %
2010	0,0	0,0	2,1	3,1	3,1								2010	100,0 %	100,0 %	50,0 %	50,0 %
Diff%	-100	-100	8,53	-16,22	-28,13												



- Package of measures 1**
1. Straightedge test on roller
 2. Visual inspection of roller after C coating
 3. Optimized C coating
 4. Improved texture of roller (new subcontractor)

- Package of measures 2**
5. Optimized C coating process of roller support
 6. Camera system for inspecting surface of roller
 7. C2 layer for roller instead of C3 layer
 8. Increased fueling with first filling fuel for [redacted]

- Package of measures 3**
9. HC washing roller support (Jan 2010)
 10. Introduction of anti-wear package 1. SOP (March 2010)

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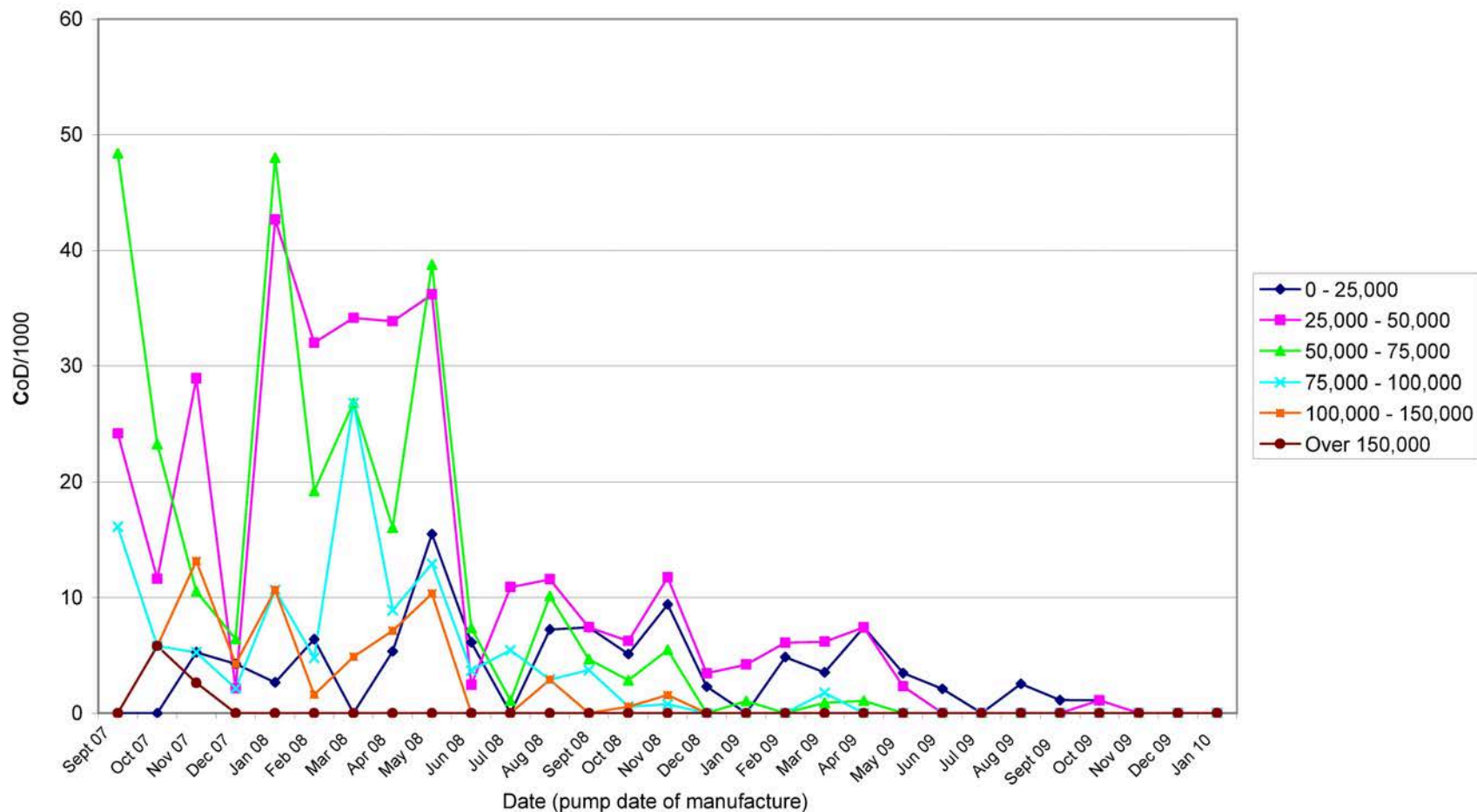
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Mileage contour lines, CP4.2



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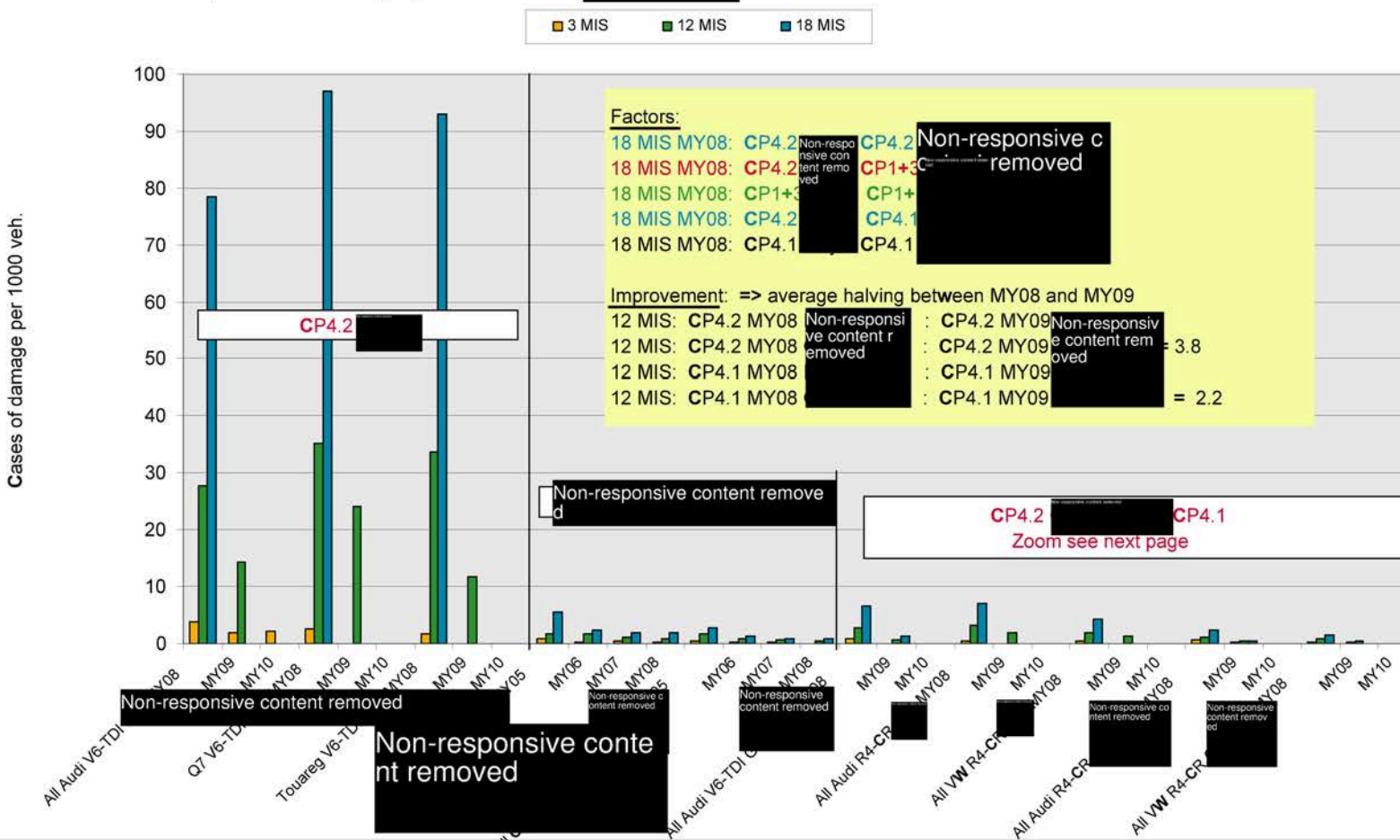


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Drivetrain damage high pressure diesel fuel pump CP4.2

Comparison of damage quotas Audi VW / V6 TDI to R4 CR / CP4 to CP1+3



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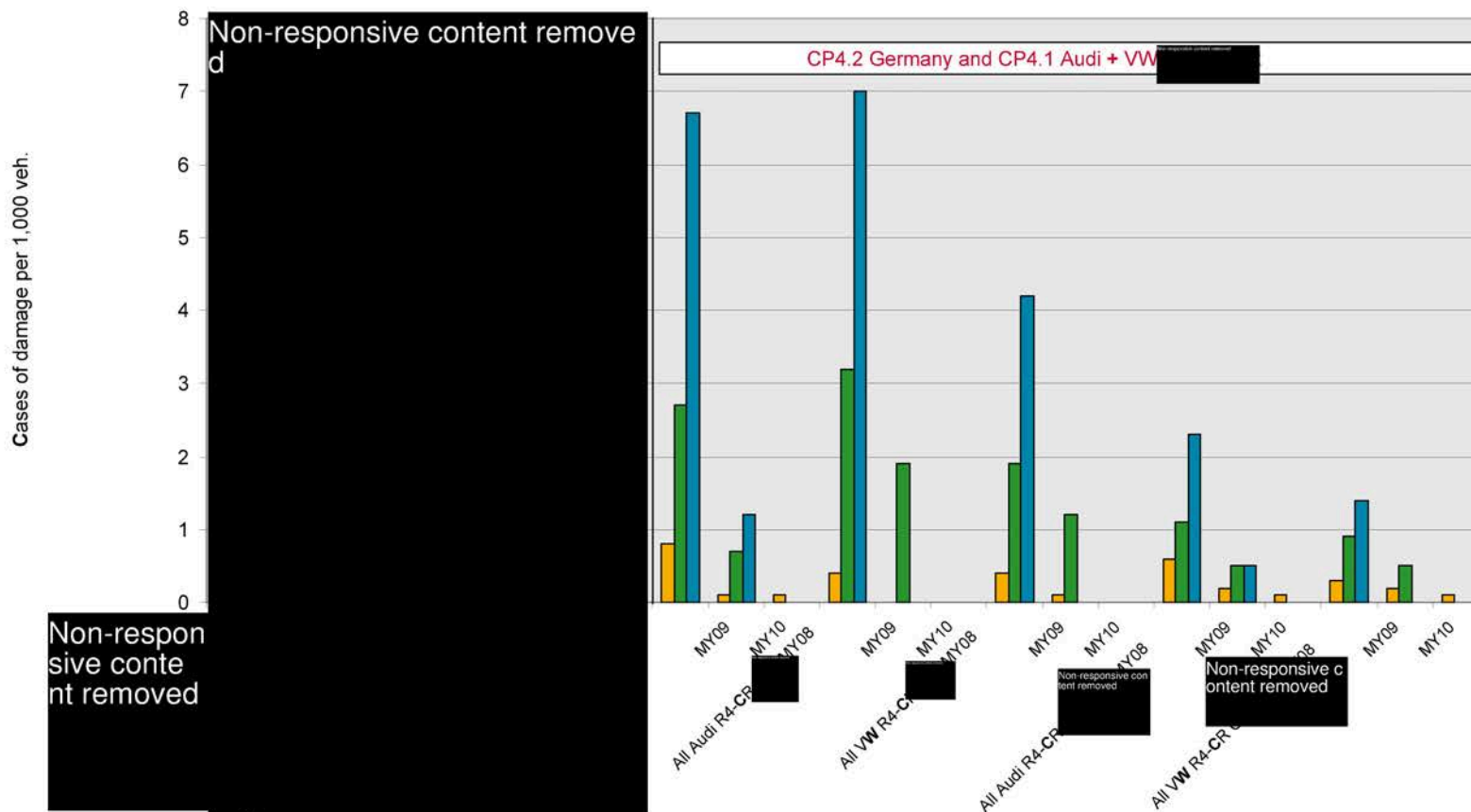


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Drivetrain damage high pressure diesel fuel pump CP4.2

Comparison of damage quotas Audi VW V6 TDI to R4 CR (without V6)

3 MIS 12 MIS 18 MIS



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Failure data Audi CP4.2 (basis: mid-February)

Distribution by country (basis: mid-February)

Total	Non-responsive content removed	Other
1125	594	313
	103	56
	59	

Distribution by model year - all (base: mid-February)

Total	2008	2009	2010
1179	687	458	34

6 MIS line by model years in Non-responsive content removed

2008	2009	2010	
10.5	4.8	2.8	x/1000 vehicles

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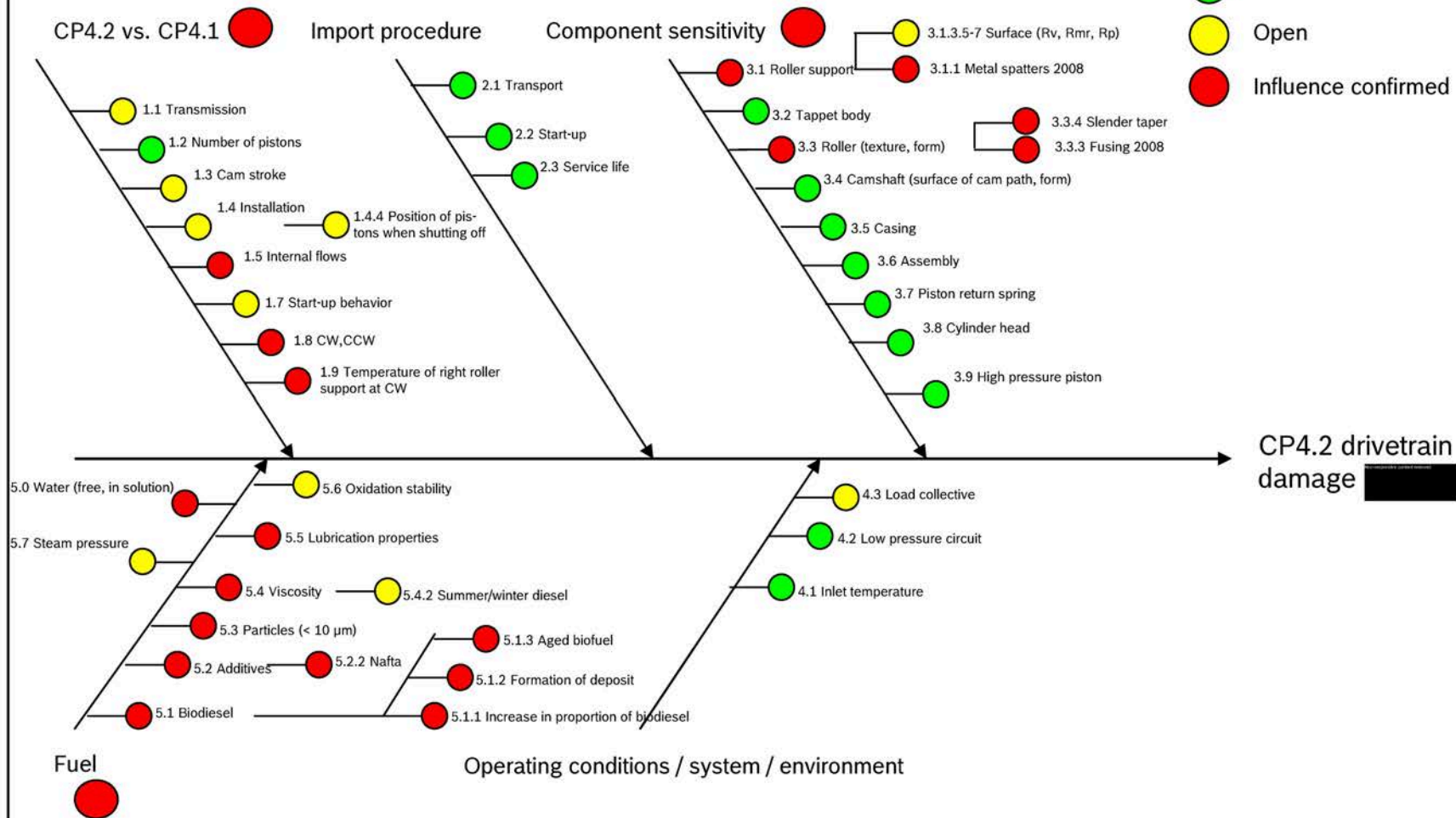


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Ishikawa – Drivetrain damage CP4.2

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- Influence unconfirmed
- Open
- Influence confirmed



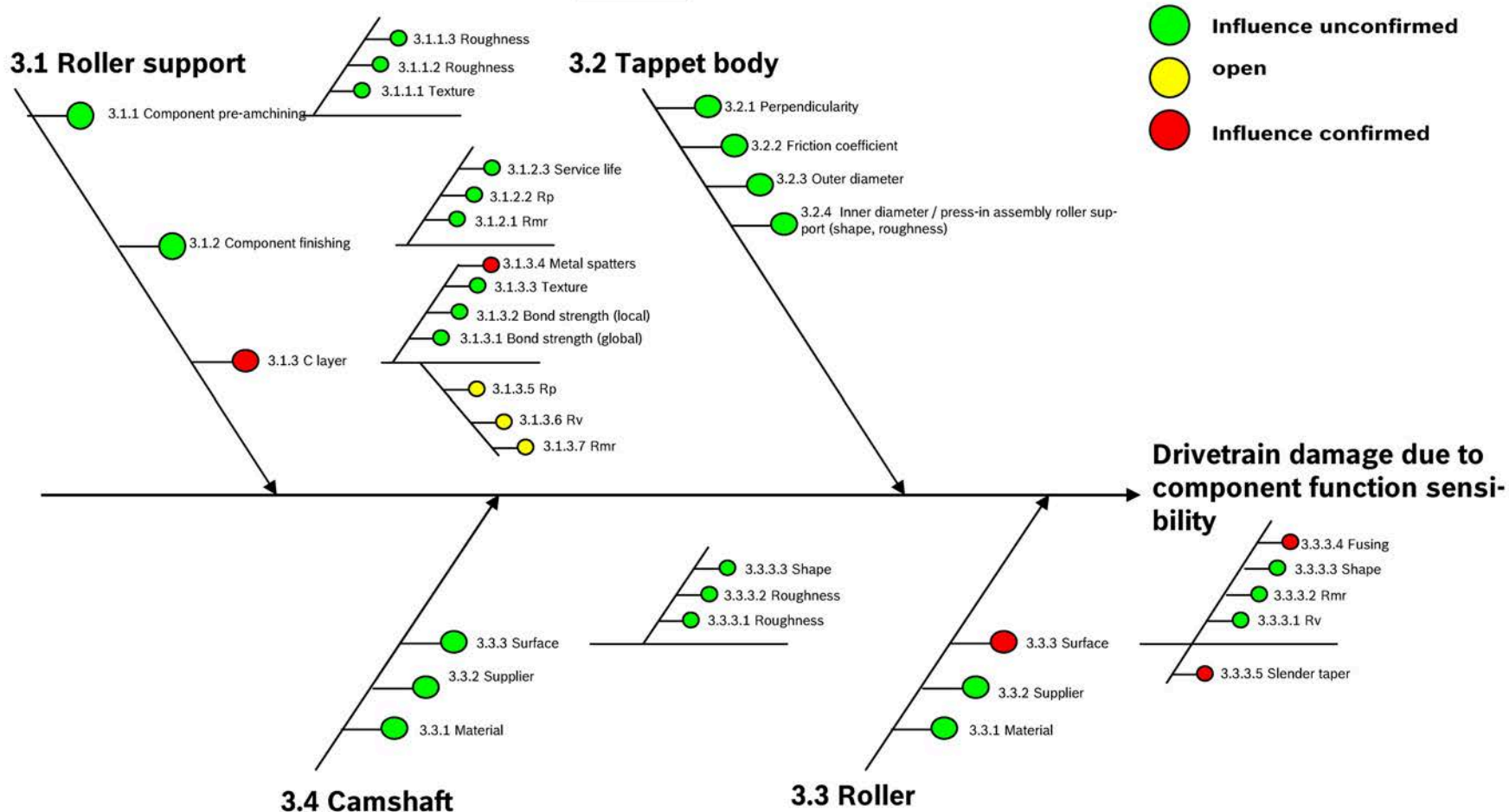
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Audi meeting Status Task Force CP4

Ishikawa – drivetrain damage CP4.2

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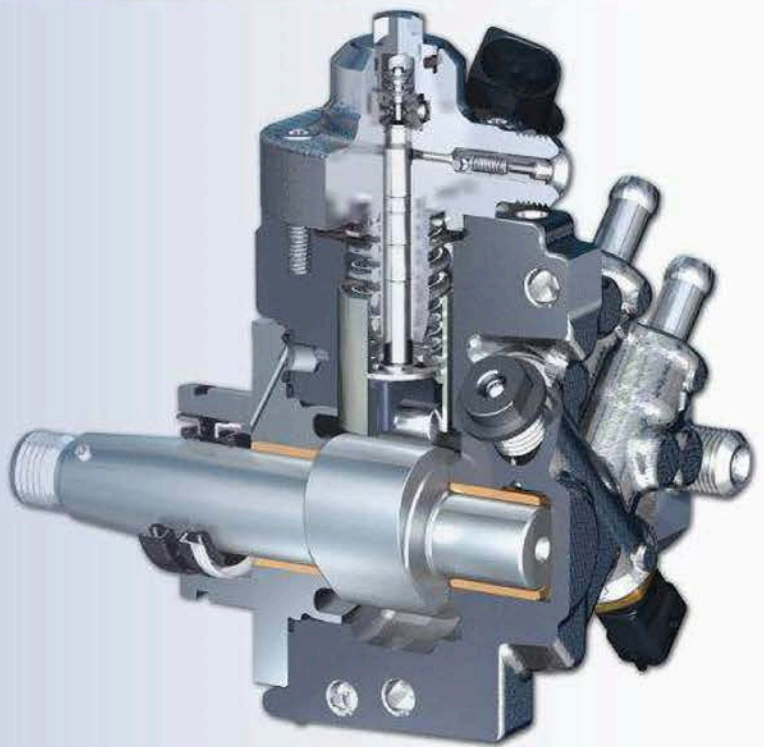
Status Task Force CP4**Summary of areas of action from Ishikawa:**

1. Fuel influence
2. Component sensitivity (metal spatters / fusing)
3. Differences between CP4.2 – CP4.1 in application and design



3) Analysis of failed pumps / fuels

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Analysis of field pumps and fuel samples from

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- FAME deposits 11 of 54 pumps
- Corrosion indicators, evidence of water 45 of 54 pumps
- Free water in fuel sample 4 of 24 samples
- Cellulose residue, algae, glycerin 9 of 24 pumps
- Heavy wear of shaft seal 17 of 17 pumps
- Good pumps with preliminary damage 6 of 13 pumps

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Determination of causes for failure focus

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Influence of fuel on Non-responsive content removed **market:**

Comprehensive switch from B0 to B7 from July 2009

Hypothesis:

- B7 fuel already stored in advance for changeover from July 2009, as a result, acidic, aged B7 fuel in circulation
 - Latent free water in fuel tank and LP system possible
- > Combination of aged biofuel with free water results in deposits
Deposits in the roller assembly prevent the roller from starting.
Primary damage: Braking flats on roller and camshaft in start case
- > Sloshing water results in sluggish, blocked roller.
Primary damage: Braking flats on roller and camshaft
(tank emptying trip vehicle test, customer B)

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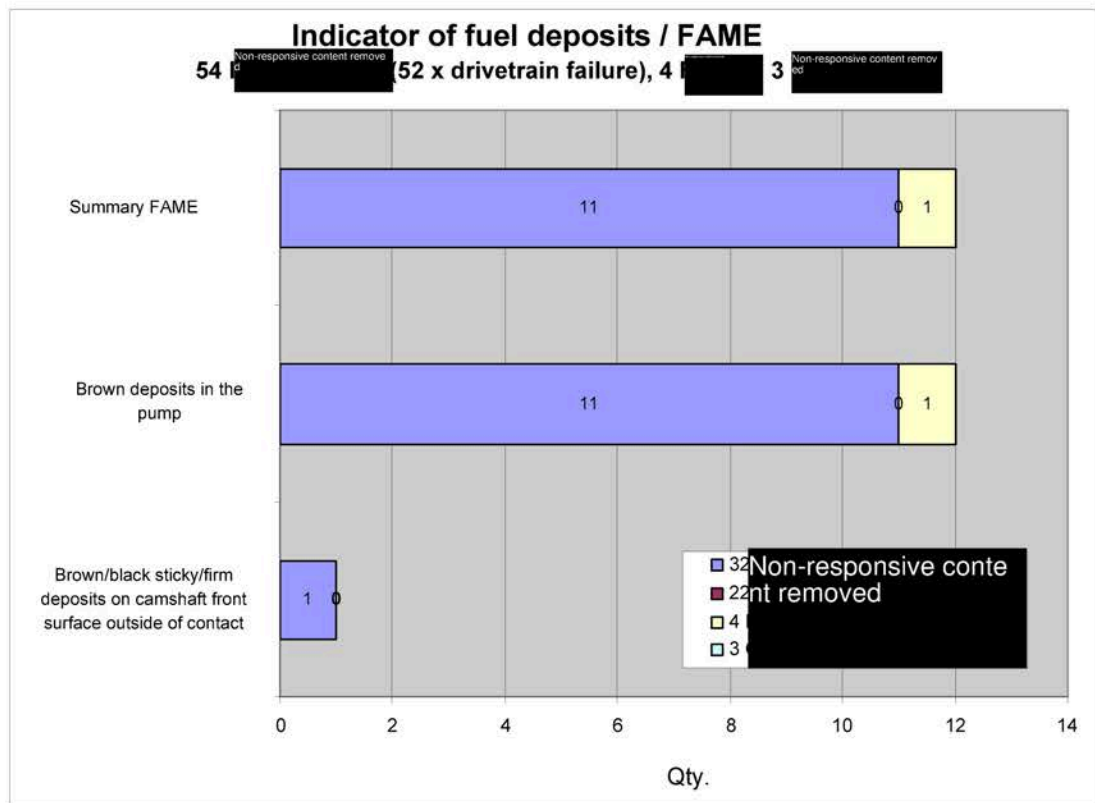
14

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Result from diagnosis for fuel aging indicators



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32 pumps

on-site action
22 pumps, 20 x drivetrain failure

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4 pumps

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3 pumps

4 x reference De OK,
2 x Audi
2 x VW

=> 11 out of 54 pumps have brown fuel deposits =>

On-site action: 0 out of 22 pumps

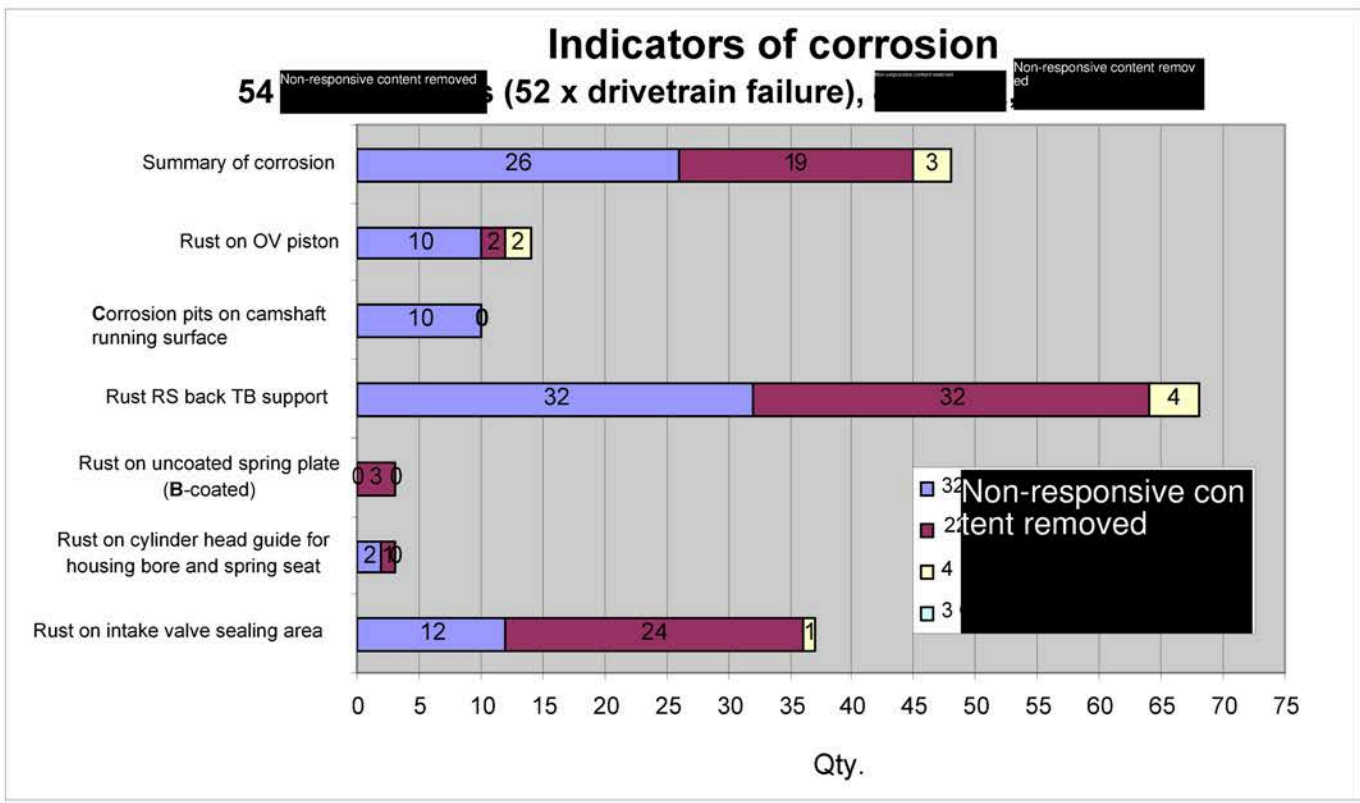
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Result from diagnosis for corrosion indicators



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32 pumps

on-site action
22 pumps, 20 x drivetrain failure

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4 pumps

Non-responsive content removed

3 pumps

4 x reference De OK,
2 x Audi
2 x VW

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=> on-site action 19 of 22 pumps with signs of corrosion



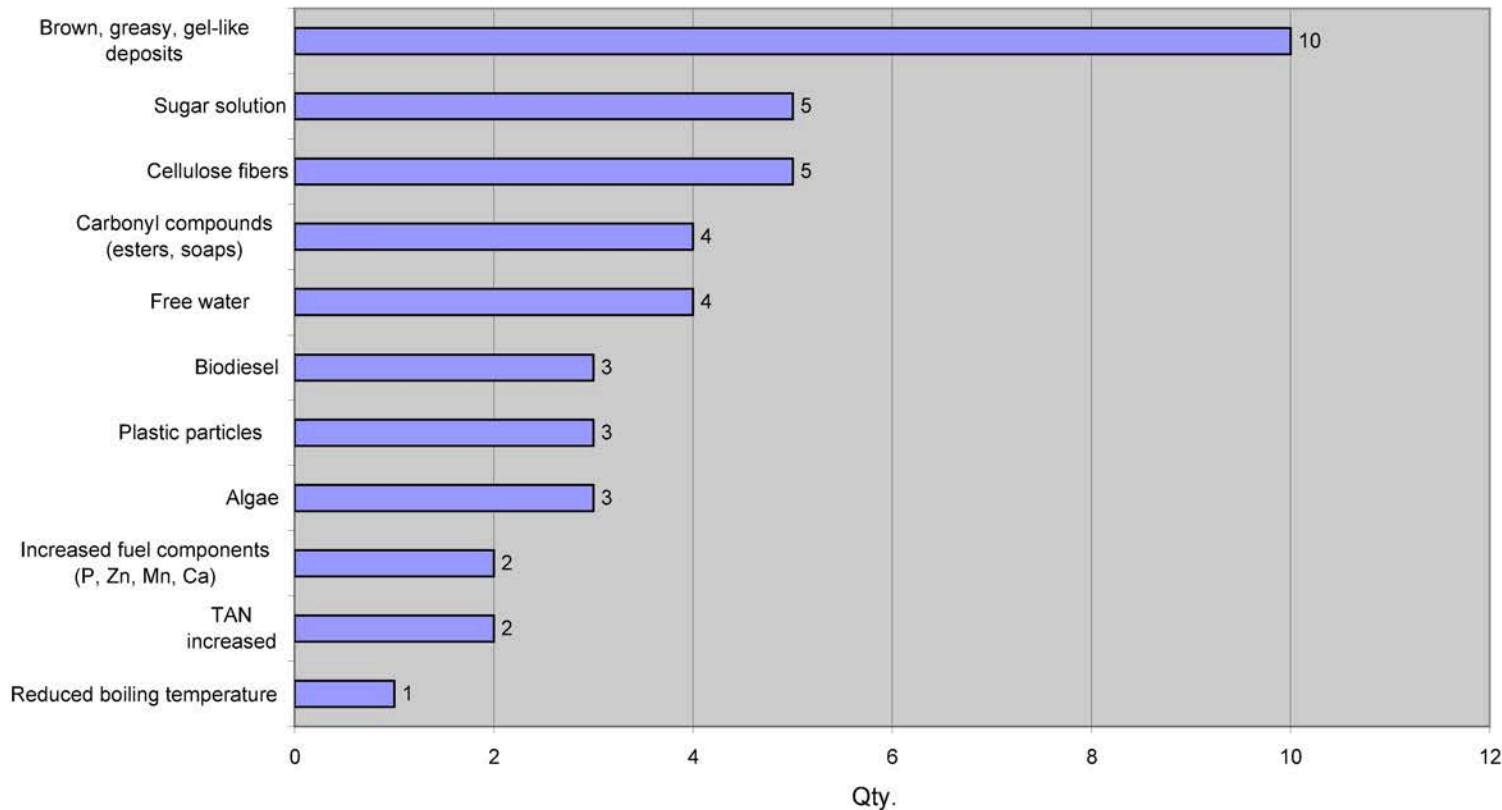
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Result of fuel analyses

Results of fuel analyses and deposits from 24 vehicles








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Audi).



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Indicators of fuel aging

Biodiesel	Component	Description/characteristics	Overview image	Description/characteristics	Overview image
A1	Roller	Brown/sticky to black/firm deposits on the roller end (outside the C layer)			
A2	Camshaft	Brown/sticky to black/firm deposits on the untouched front surfaces of the camshaft		Brown/sticky to black/firm deposits on the unprocessed surfaces	
A3	Intake valve	Brown/sticky to black/firm deposits on the shaft of the intake valve piston (outside the guide surfaces)		Brown/sticky to black/firm deposits on the adjustment ring of the MU	
A4	Roller support	Brown/sticky to black/firm deposits on the back of the roller support (outside the contact surfaces)		Brown/sticky to black/firm deposits on the mesh of the OV strainer OV strainer pressed in	



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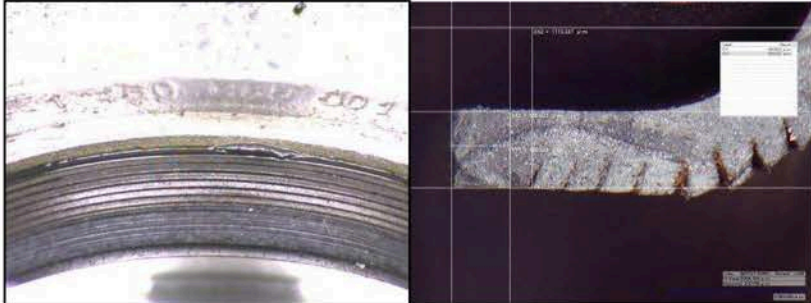
Indicators for corrosion (validated by WCF)

Corrosion	Component	Description/characteristics	Overview image	Detailed picture	Analysis picture
K5	Cylinder head	Rust in wear area due to tappet spring			
K6	Cylinder head	Rust on centering collar of cylinder head to housing			
K7	Tappet body	Rust deposits on bearing surface to spring plate			
K8	Spring plate	Rust in wear area on the bearing surface to tappet body or tappet spring			



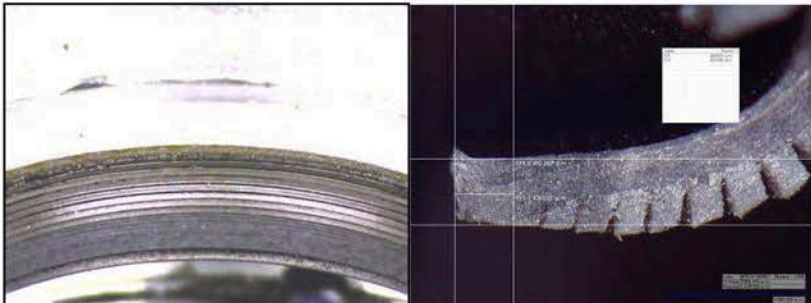
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Examples for wear of Bruss shaft seal



Wear depth approx. 74 µm

- > Project W19 EU6/BIN5
- > Report 2009-CP4_0122 ER end
- > SN 0 445 010 613
- > Pump DM 01/22/2008 No. 0893
- > Vehicle AU716 80219 engine 059.G VN6 121
- > Mileage **201,335 km**



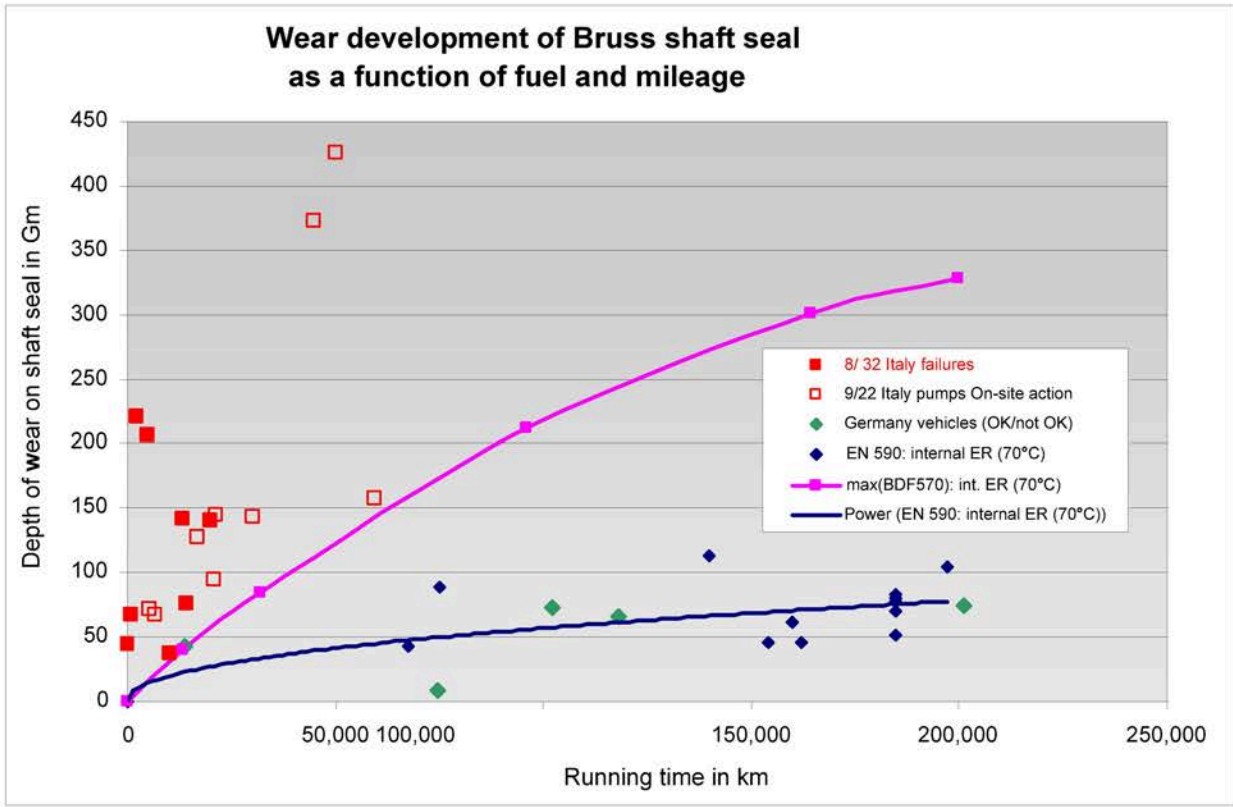
Wear depth approx. 221 µm

- > QC no. 230002542476 (4A203)
- > SN 0 445 010 611
- > Pump DM 10/30/2008 No. 0702 R2
- > Mileage **2,212 km**
- > Failure on 6/15/2009 in [REDACTED]



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Result of shaft seal wear measurement, Non-responsive content removed



- => Bruss shaft seal Non-responsive content removed (17x) worn more than with EN590 (= fuel influence)
- => No functional leakage of described shaft seal
- => No dependency on manufacturing or failure date



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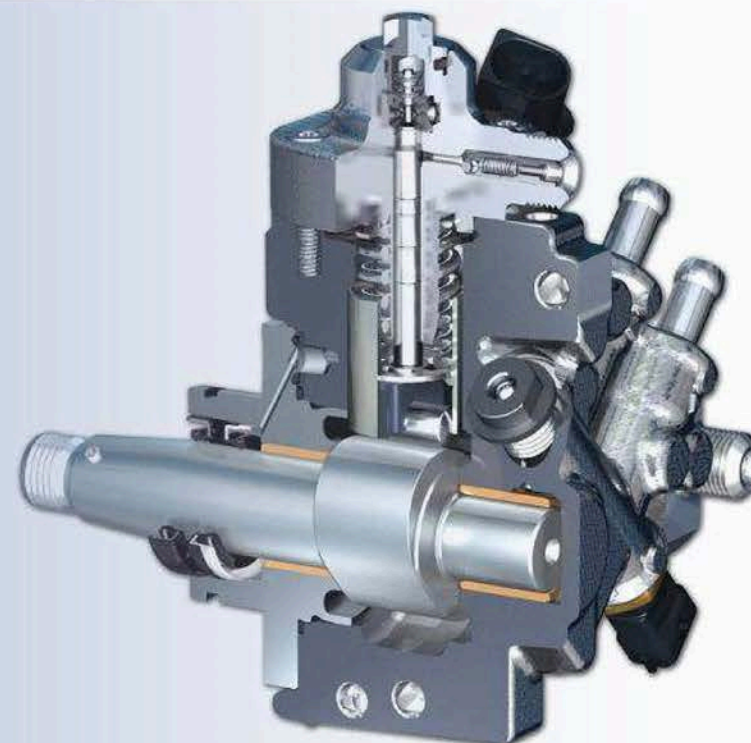
Analysis results of failure pumps / fuel investigations

1. Non-standard biofuels (aged)
2. Cellulose, sugar, acids, algae
3. Water (rust)
4. Field failures in Italy with turned tappet as aftereffect (field failures in Germany with abrasion wear as aftereffect)
5. The roller support is primarily worn in the middle



4) Component sensitivity

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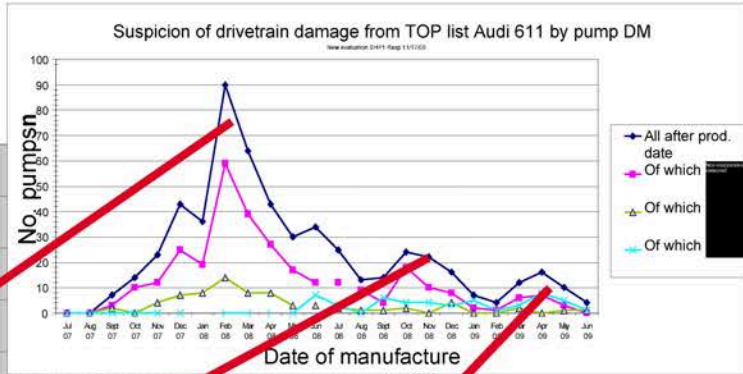
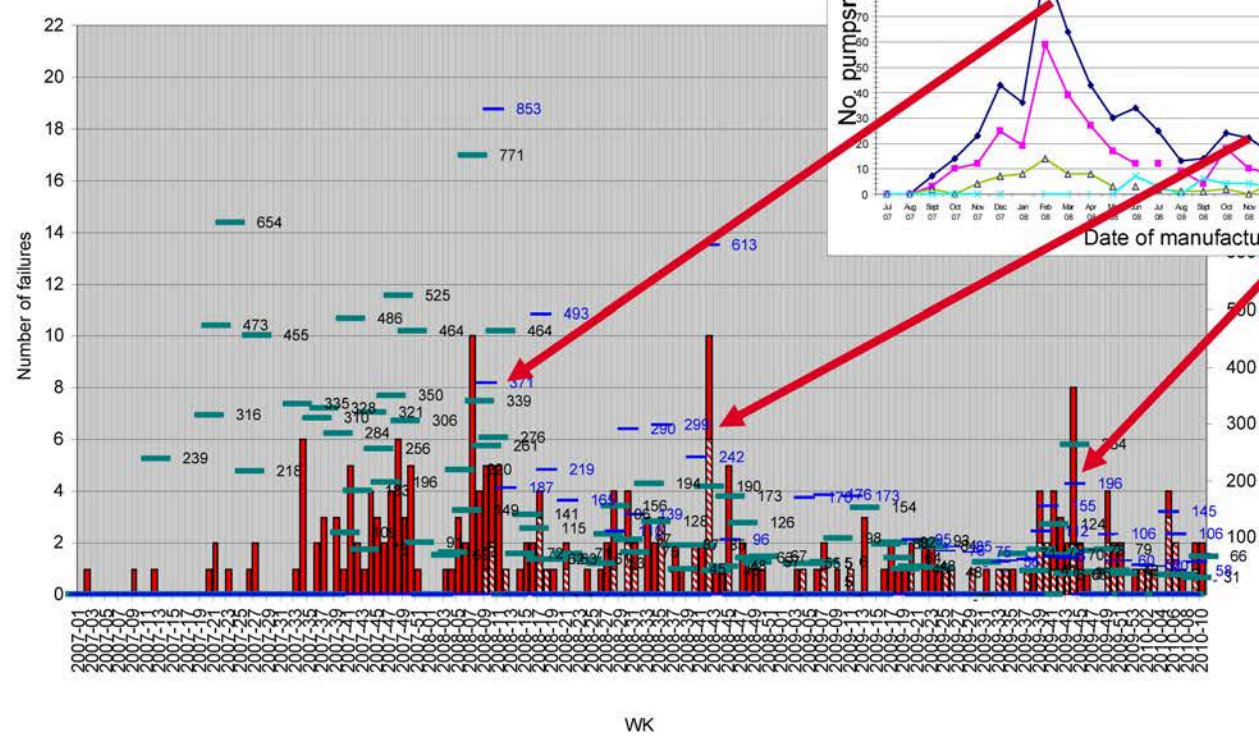
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Overview of failures, internal test bench & Field (failure peaks)

failures drivetrain damage DM WK CP4.1/C P4. 2 Internal



-> Increased internal test bench failures correlate with increased field failures



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Component sensitivity**1. Metal spatters in C3 coated roller support**

Metal spatters 5/2008 highly reduced through optimization of plants. Sensitivity to small metal spatters with EN590/ BDF570 verified from 5/2008.

Note: C2 does not have any metal spatters.

2. Roller with fusing

To select rollers with fusing, the straightedge test was introduced in 5/2008.

The conversion of the roller end coating to C2 in 5/2009 eliminated the fusing.



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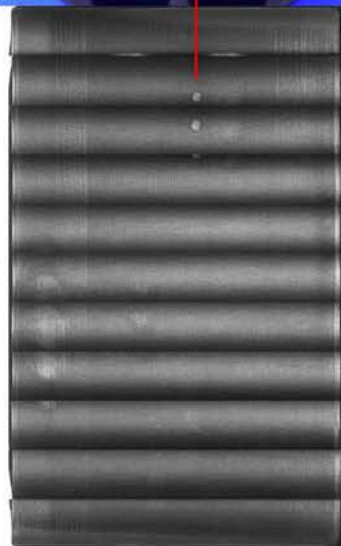
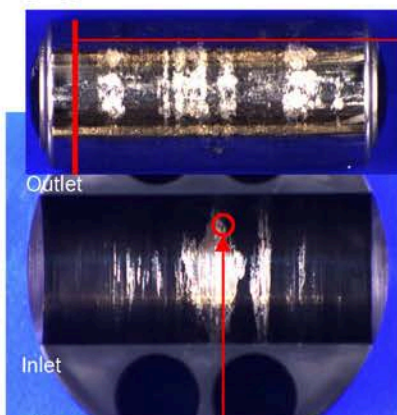
1. Test of component sensitivity

- > "Mixed friction" variant
- > 1x CP4.2, lift 5.25 mm (part no. ...617, VVT 2010-CP4_0065, ER 17319)
- > Arctic Diesel Class 4, 90° inlet temperature
- > 2,300 bar, 600 rpm (overload program)
- > Target: 15h run-in program (4,000rpm@2kbar) + 150h overload
- > C3 series RS, but with large metal spatters, i.e. scrap under current visual inspection
- > Roller with fusing
- > Failure after approx. 13 min. in run-in program with Arctic Diesel

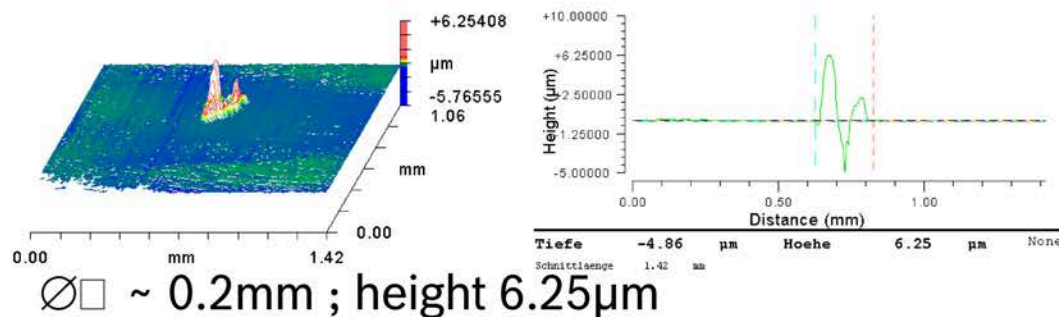


Status Task Force CP4

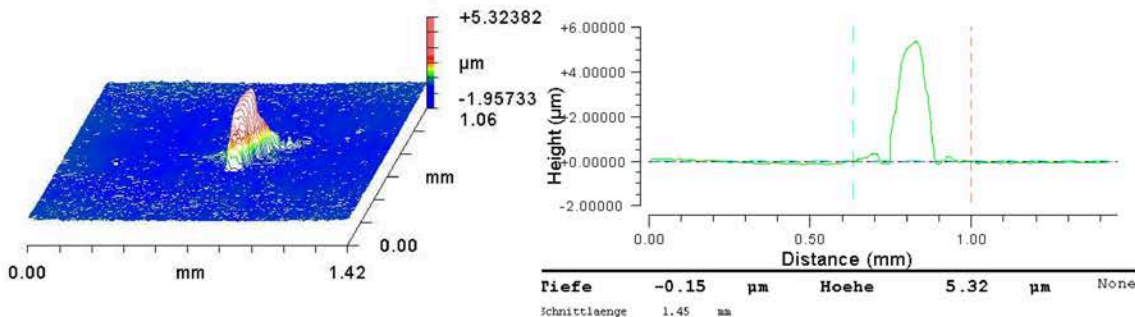
Tappet left RS 2949; roller 15



Location of fusing in roller end taper

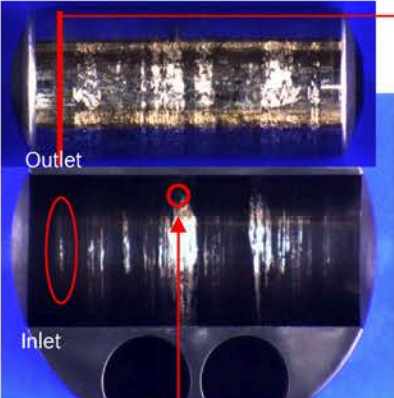


Metal chips in the roller support

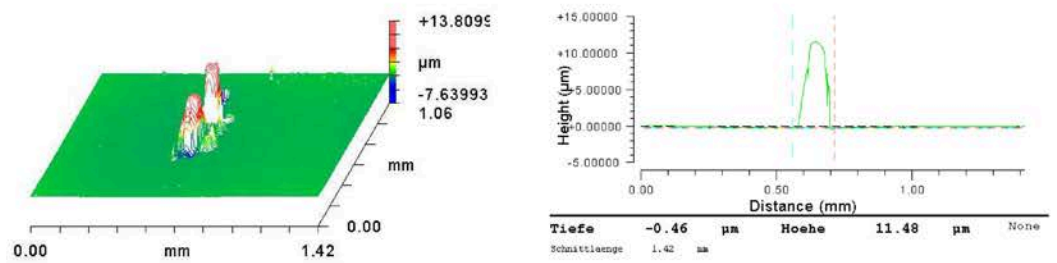


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Tappet right RS 5794; roller 07



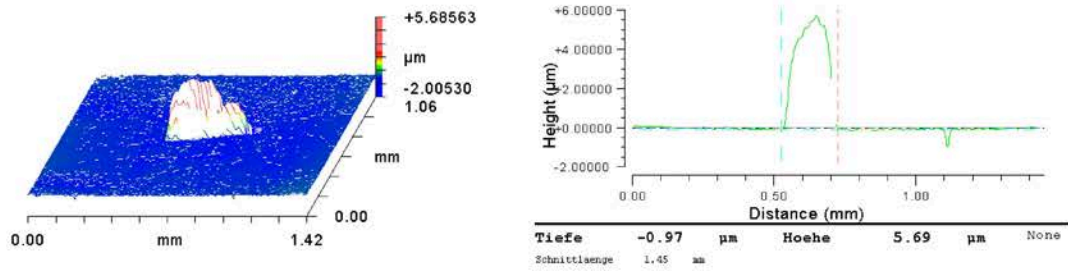
Location of fusing in roller end taper



∅□ ~ 0.3mm ; height 11.48µm



Metal chips in the roller support



∅□ ~ 0.2mm ; height 5.69µm



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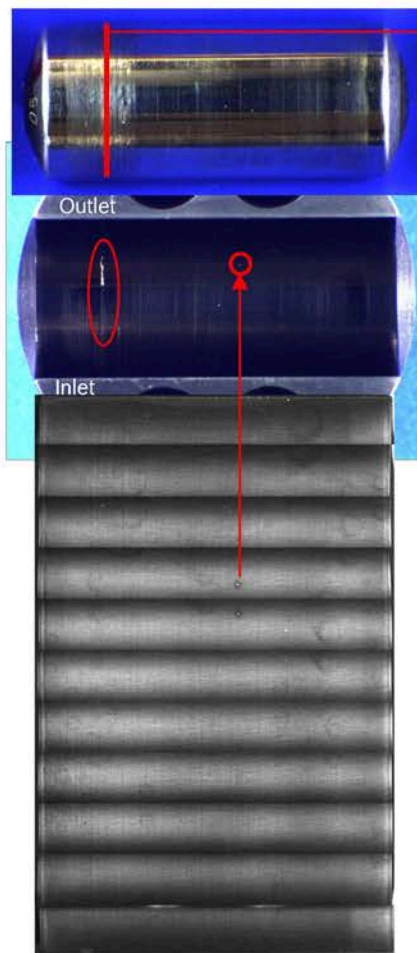
2. Test of component sensitivity

- > "Staged test" variant
- > 1x CP4.2, lift 5.25 mm (part no. ...617, VVT 2010-CP4_0066, ER 17320)
- > Run-in + two steps (target program):
 - Run-in: 15h, 3000 rpm, 1300 bar, EN590, 40°
 - Step 1: CER, 200h, 3000 rpm, 1300 bar, EN590, 40°
 - Step 2: CER, 150h, 600 rpm, 2300 bar, Arctic Diesel Cl. 4, 90°
- > C3 series RS, but with small metal spatter, i.e. scrap under visual inspection
- > Roller with fusing
- > Run-in + step 1 - EN 590 200h positive
- > Failure after approx. 2h in step 2 after change from EN590 to Arctic Diesel

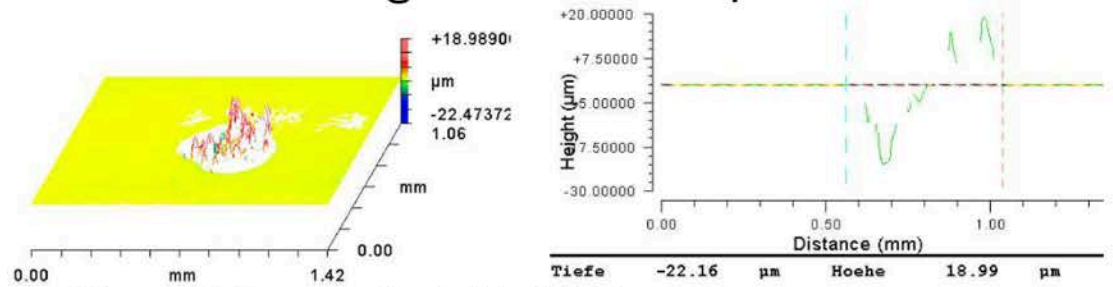


Status Task Force CP4

Tappet left RS 3566; roller 05

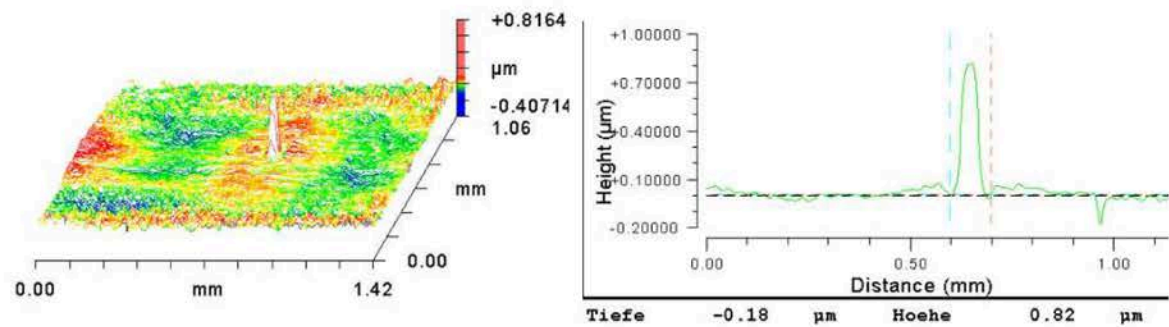


Location of fusing in roller end taper



$\varnothing \square \sim 0.5\text{mm}$; height 18.99 μm

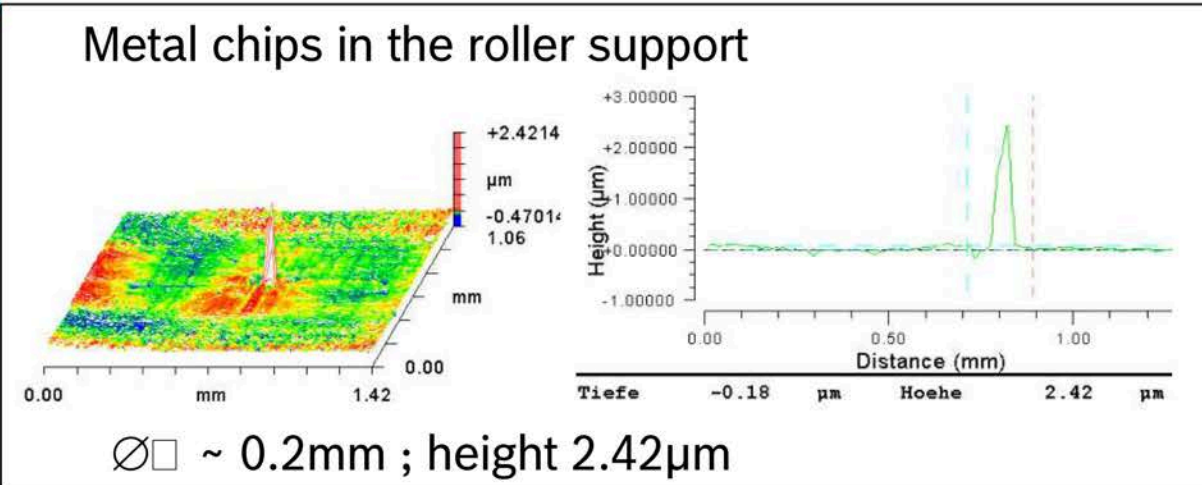
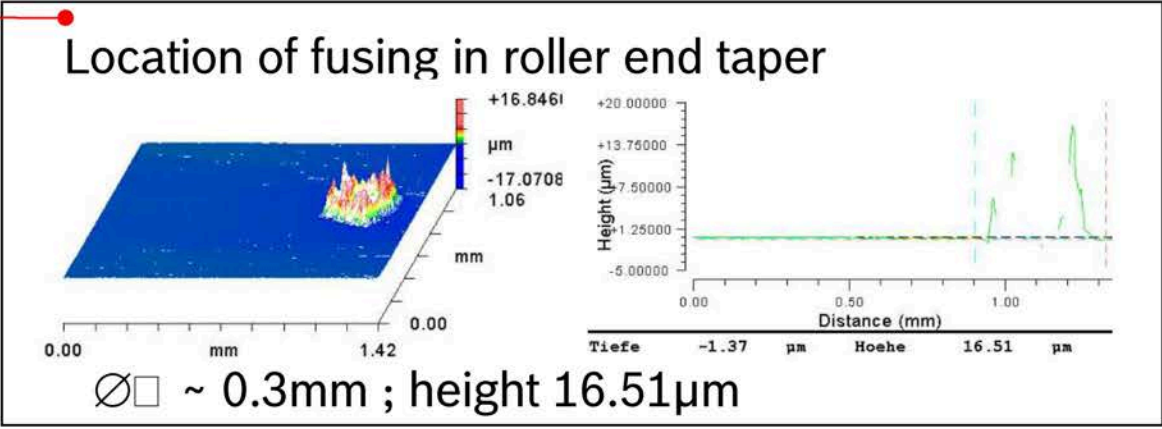
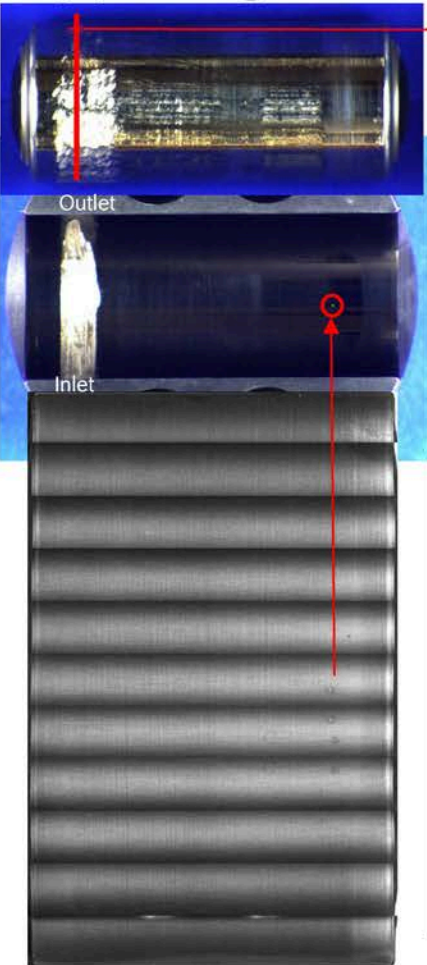
Metal chips in the roller support



$\varnothing \square \sim 0.1\text{mm}$; height 0.82 μm

Status Task Force CP4

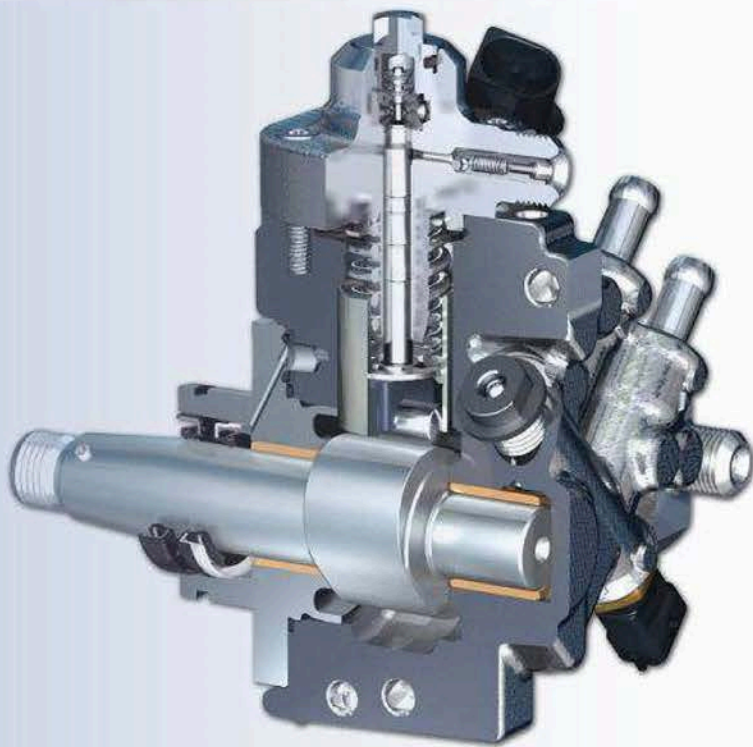
Tappet right RS 3874; roller 11



5) Good pumps from

Non-responsive content removed

Non-responsive content removed



Diesel Systems



BOSCH

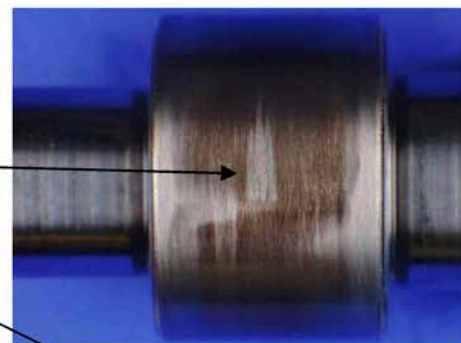
Status Task Force CP4

TF AUDI [Non-responsive content removed] Good pump (2009-CP4_0685)

5,125 km (no failure)

Summary analysis results

- > Transfer of material from roller to cam
- > Braking flat from non-starter



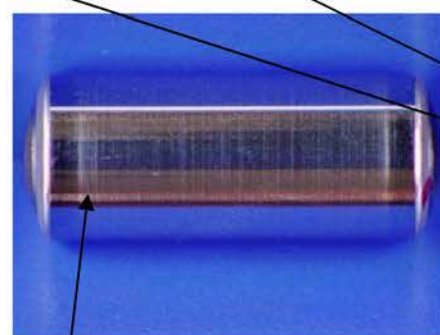
Interpretation:

Sluggish roller @ engine start

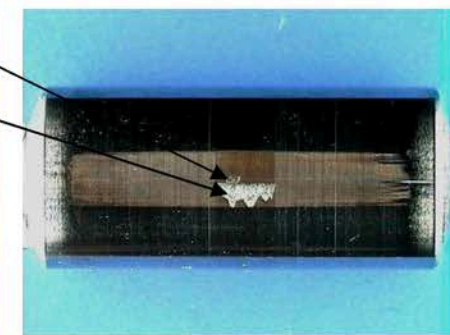
6 of 13 good pumps from [Non-responsive content removed] have the same symptoms.

Preliminary damage does not necessarily result in failure (failure primarily due to continued driving with poor fuel).

Experience from initial reappear tests.



Left roller
Edge wear

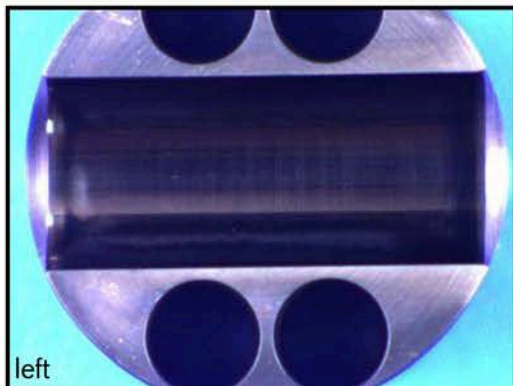


Right roller

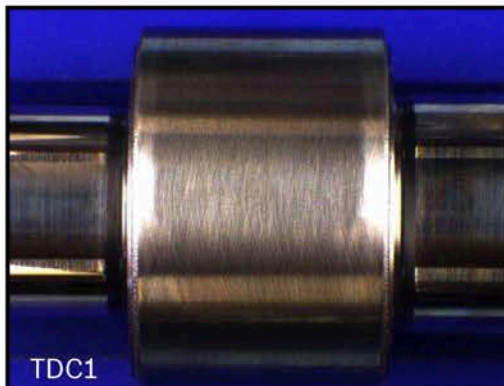


Status Task Force CP4

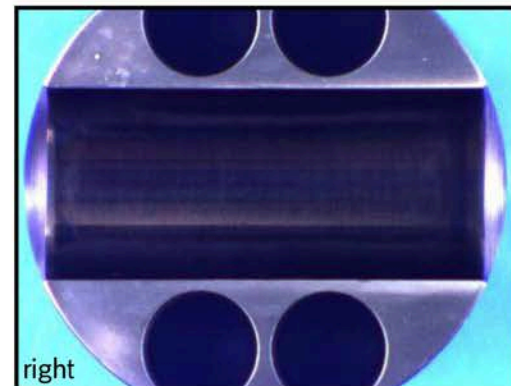
2010-CP4_0045 “Good pump” field [redacted] with 39,701km (vehicle 4L69D 007303) 0445 010 611; DM: 6/18/2008; Ch. index 0010



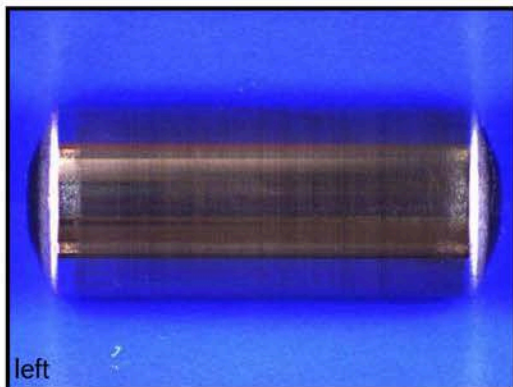
left



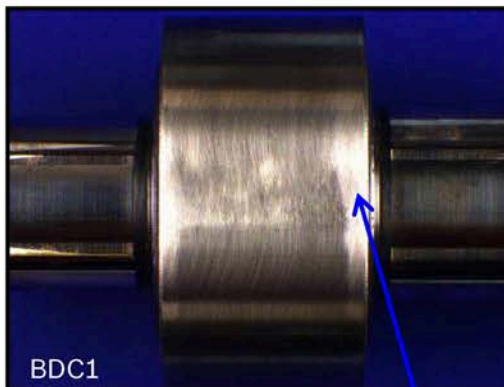
TDC1



right

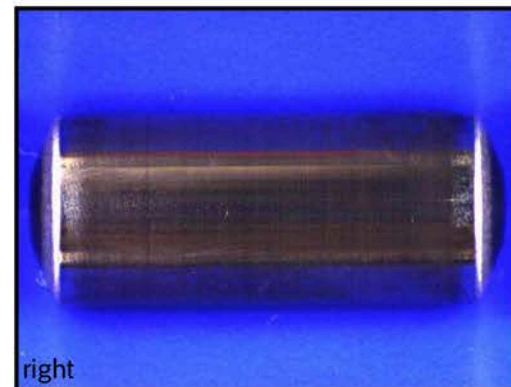


left



BDC1

Slightly asymmetric contact trail



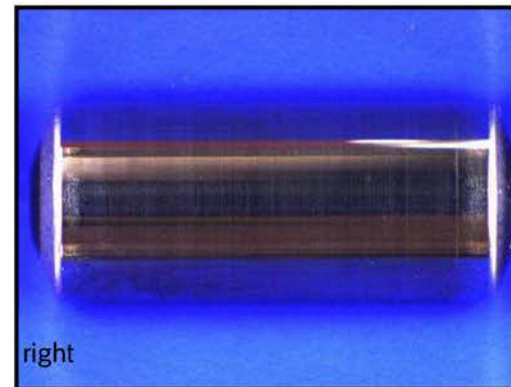
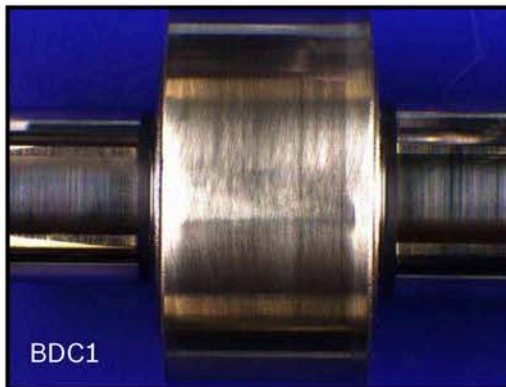
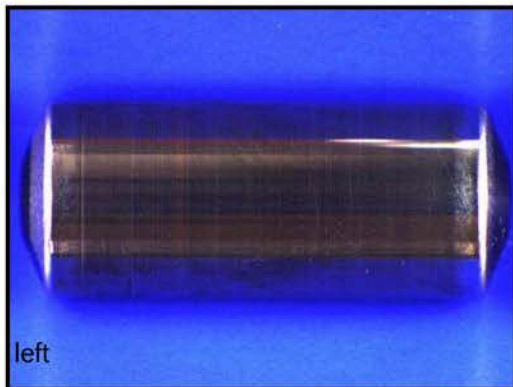
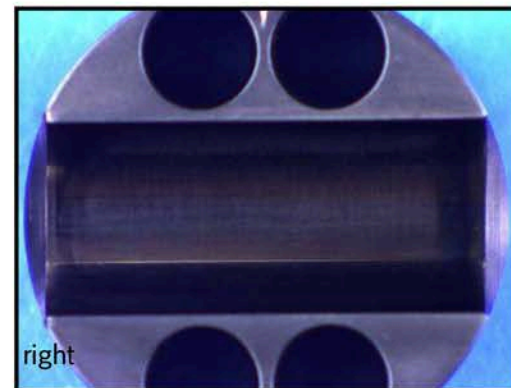
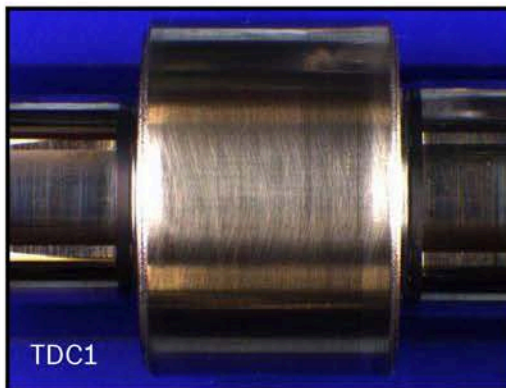
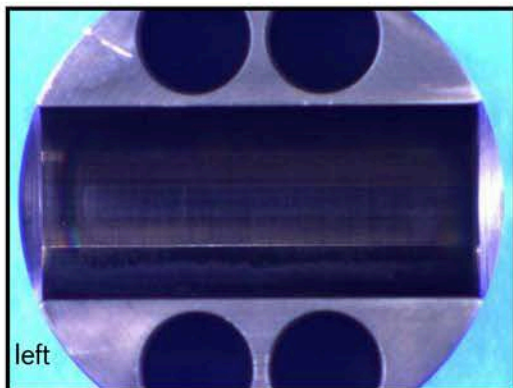
right

Diesel Systems



Status Task Force CP4

2010-CP4_0046 "Good pump" field Non-responsive content removed with 22,751km (vehicle 4L99D 006730) 0445 010 611; DM: 06/16/2008; Ch. index 0010

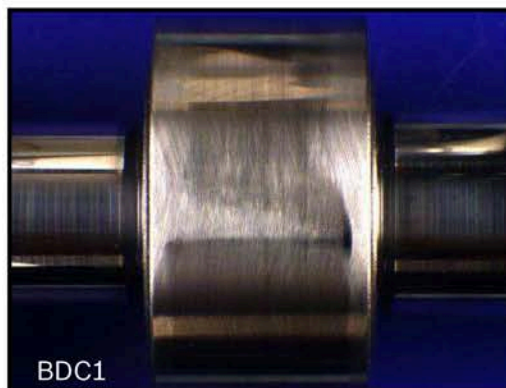
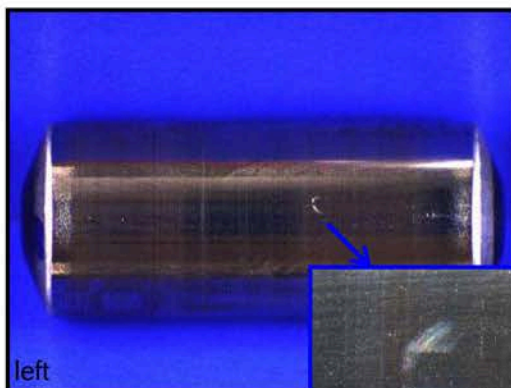
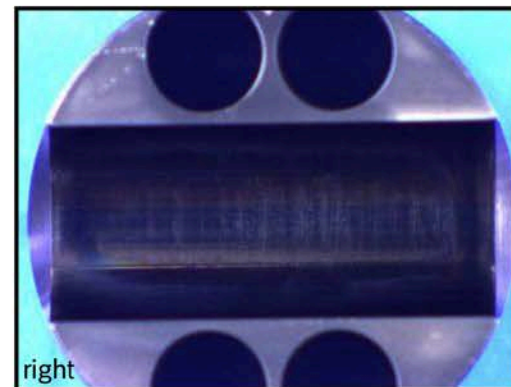
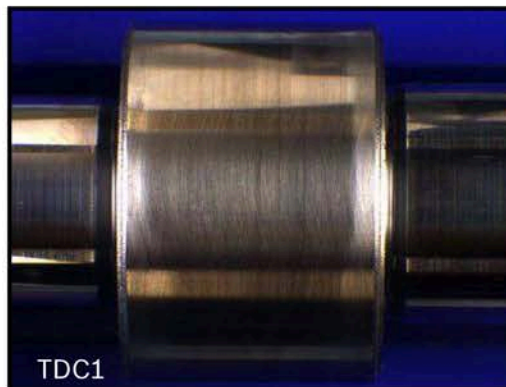
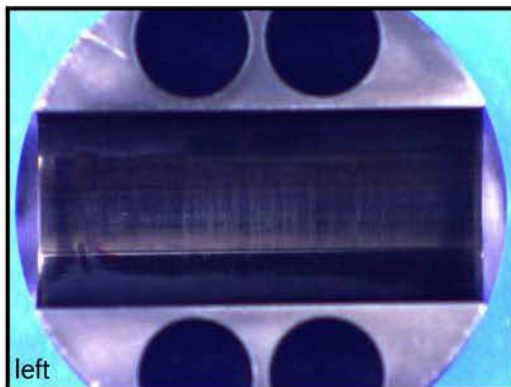


Diesel Systems



Status Task Force CP4

2010-CP4_0047 “Good pump” field Non-responsive content removed with 29,537km (vehicle 4L19D 016121) 0445 010 611; DM: 8/4/2008; Ch. index 0010

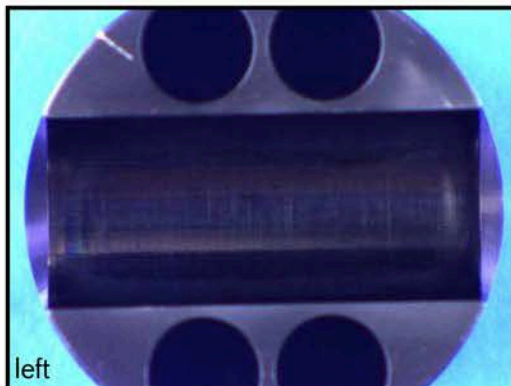


Diesel Systems

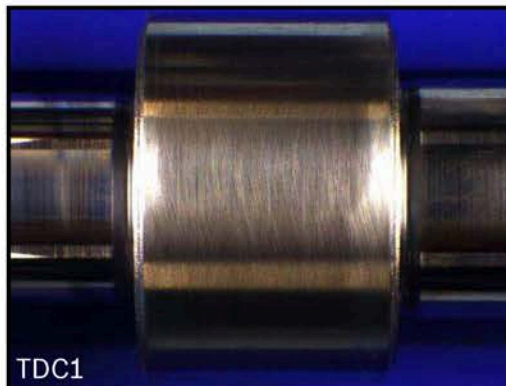


Status Task Force CP4

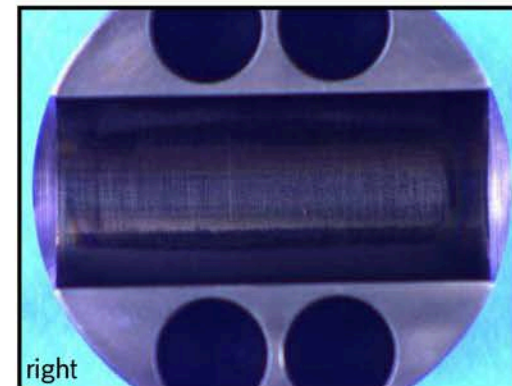
2010-CP4_0048 “Good pump” field Non-responsive content removed with 60037km (vehicle 4L89D 006380) 0445 010 611; DM: 6/12/2008; Ch. index 0010



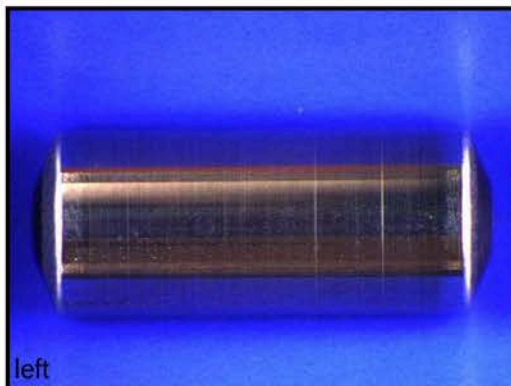
left



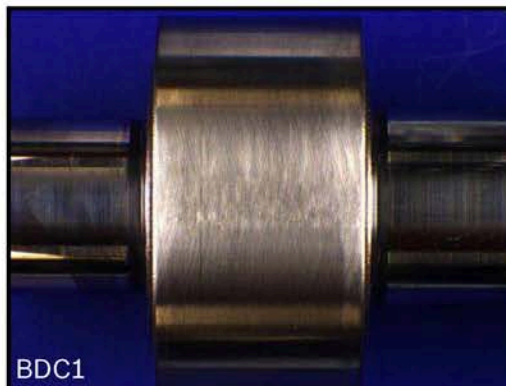
TDC1



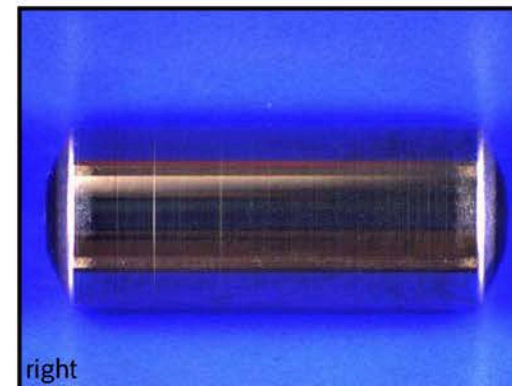
right



left



BDC1



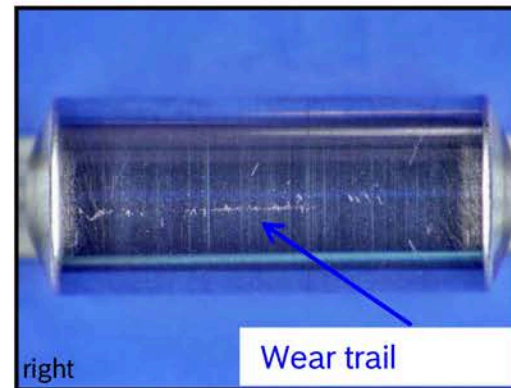
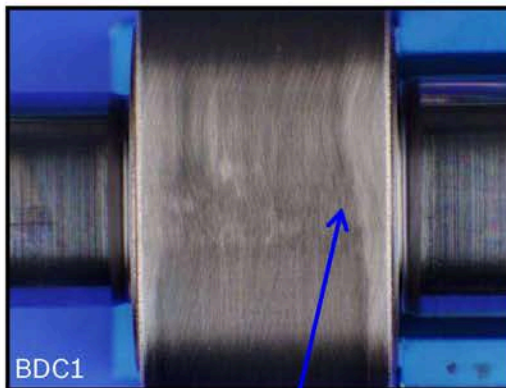
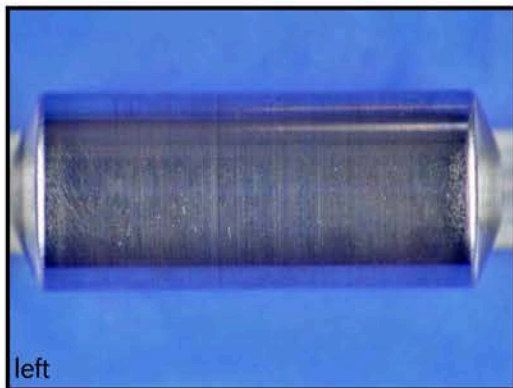
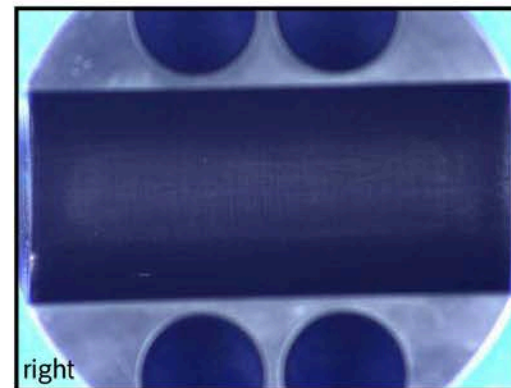
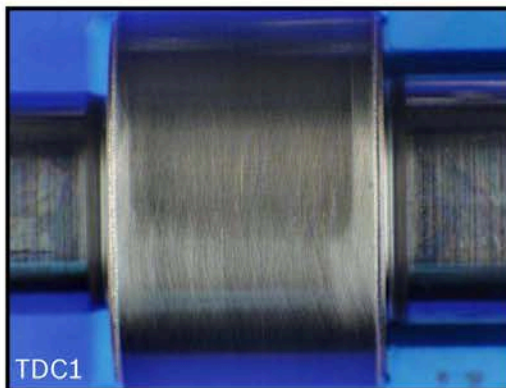
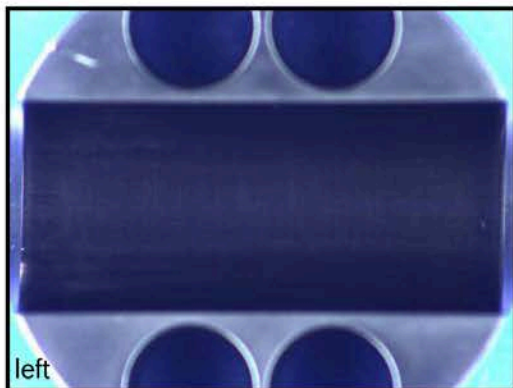
right

Diesel Systems



Status Task Force CP4

2010-CP4_0062 “Good pump” field Non-responsive content removed with 39,967km (vehicle 4L49D 009440) 0445 010 611; DM: 6/28/2008; Ch. index 0010



Asymmetric contact pattern on cam drop



Status Task Force CP4

Field failure Audi W26 after 1596 km in Non-responsive content removed

1) Failure pump: **2010-CP4_0013** (QMM 4A236) on bench 1
0445010619 LW; line 01; DM 090624; ser. no. 1403;
Ch. index 0003 (-> Roller end C2.1)

->Drivetrain damage

- Complete camshaft, roller, RS wear
- no final 90° turn
- Corrosion on intake valve plate left

2) Sibling pump on bench 2: 2010-CP4_0014 (QMM 4A237)
0445010619 LW; line 01; DoM 090505; seq. no. 0677;
Ch. index 0002 (-> Roller edge C3)

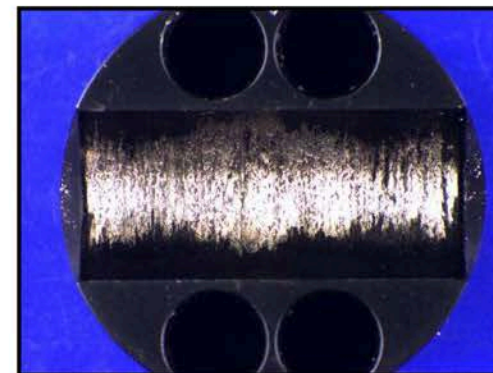
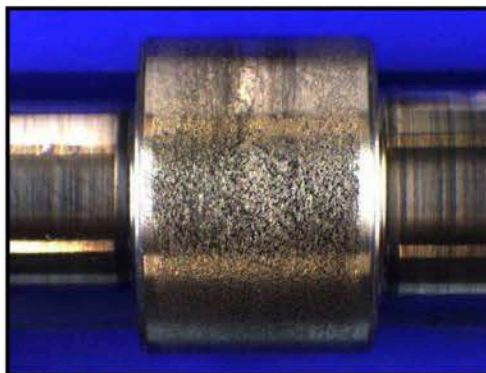
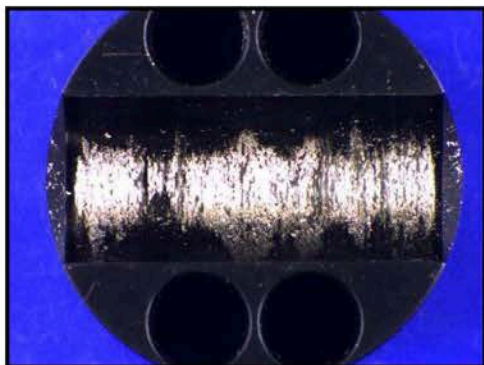
-> No drivetrain damage, but preliminary damage

- Braking flat on the roller
- tracks indicating a turned tappet assembly
- Corrosion on roller

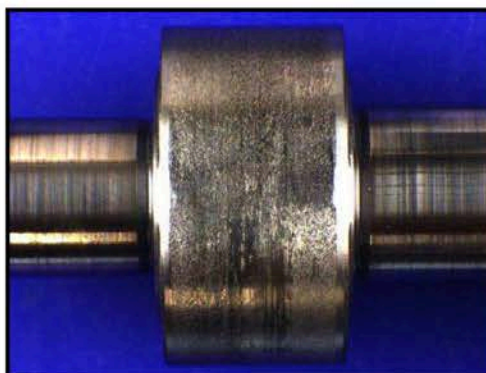


Status Task Force CP4

Field failed pump **W26** (bench 1) from Non-responsive content removed 2010-CP4_0013 (QMM 4A236)



Complete abrasive wear



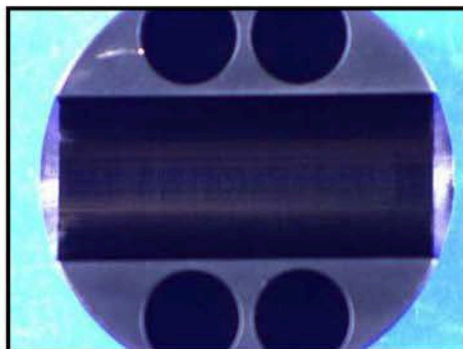
Diesel Systems



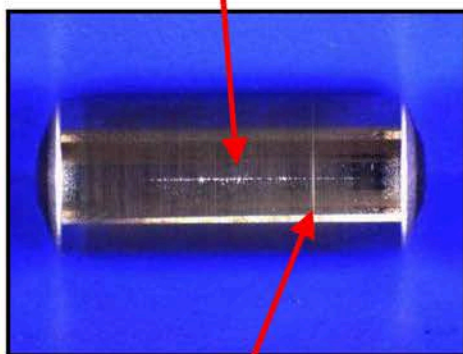
Status Task Force CP4

Sibling pump **W26** (bench 2) from Non-responsive content removed 2010-CP4_0014 (QMM 4A237)

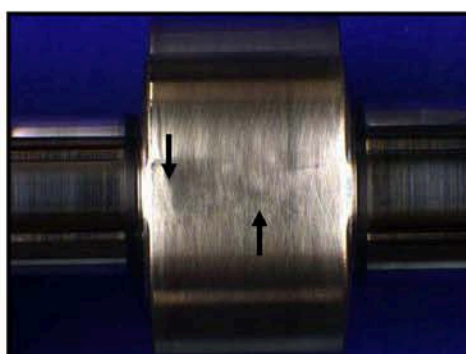
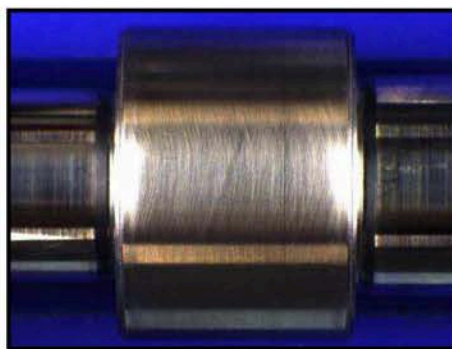
Left tappet assembly



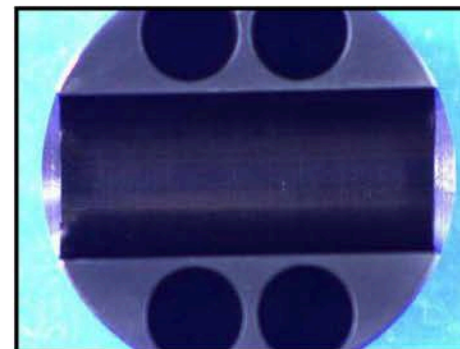
Braking flat



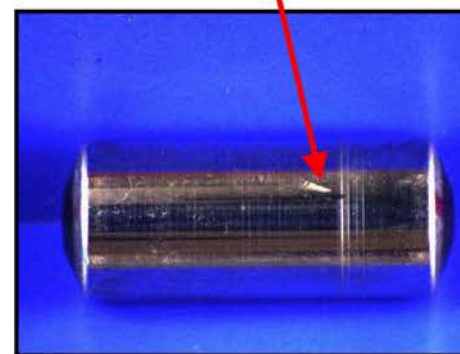
Particle wear



Right tappet assembly



Abrasive wear

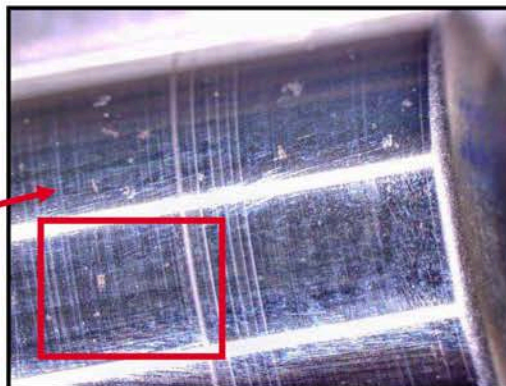
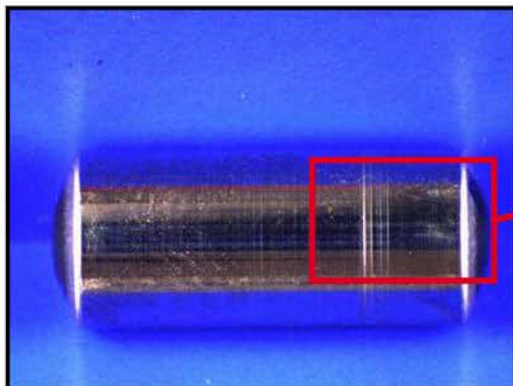


Diesel Systems



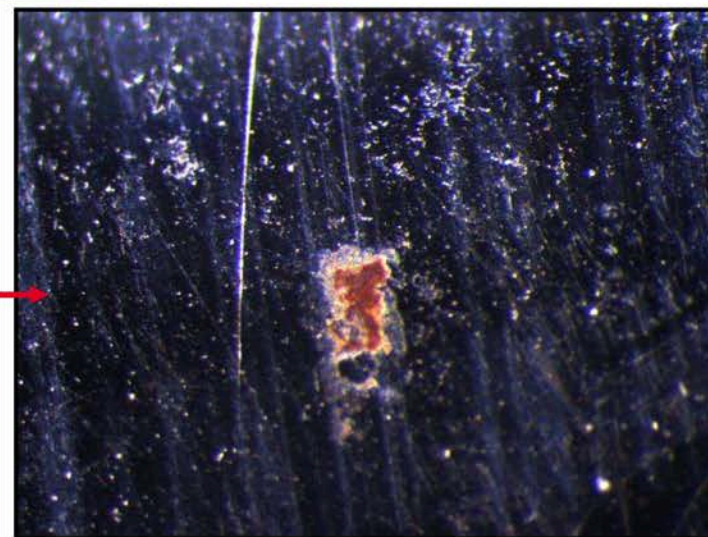
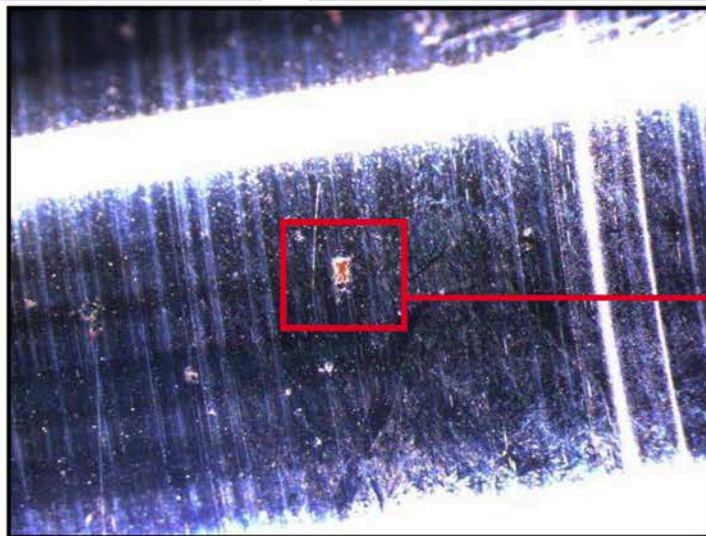
Status Task Force CP4

Sibling pump **W26** (bench 2) from Non-responsive content removed 2010-CP4_0014 (QMM 4A237)



Right roller

Corrosion in numerous places



Diesel Systems



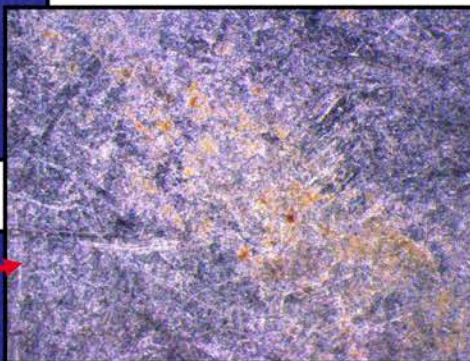
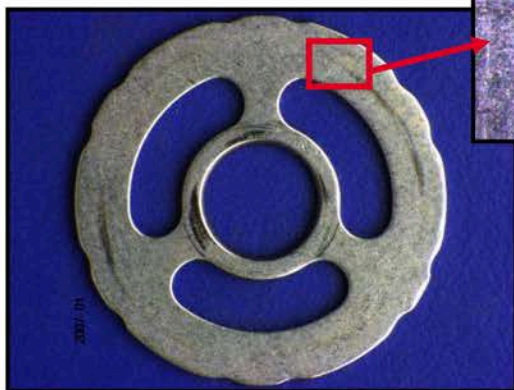
Status Task Force CP4

Sibling pump **W26** (bench 2) from Non-responsive content removed 2010-CP4_0014 (QMM 4A237)

Spring set



Piston set



Brownish fuel deposits



left

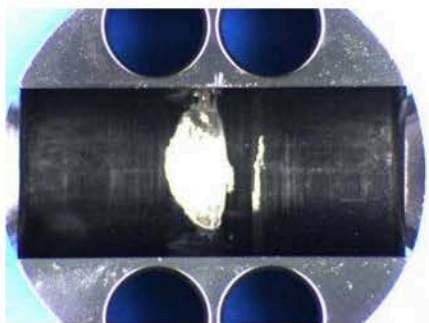
right

Diesel Systems

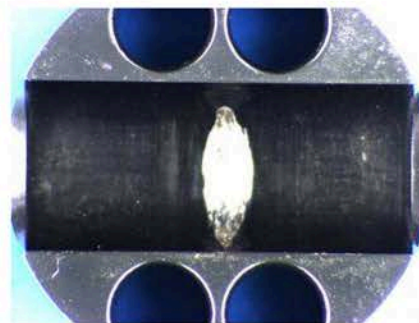


Status Task Force CP4

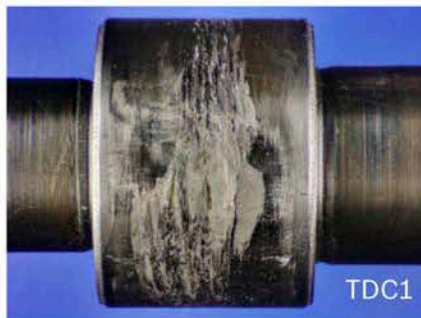
2010-CP4_0051 field failed pump **W26** Non-responsive content removed 22,270 km (vehicle) 0445 010 619; DM: 10/13/2008



left



right



TDC1



left

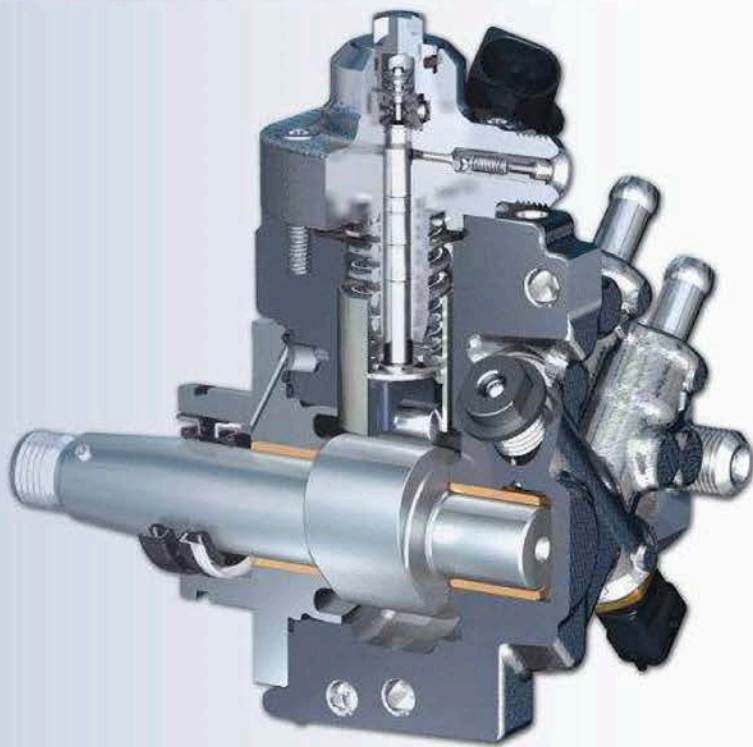


right



6) Hypotheses for Non-responsive content removed

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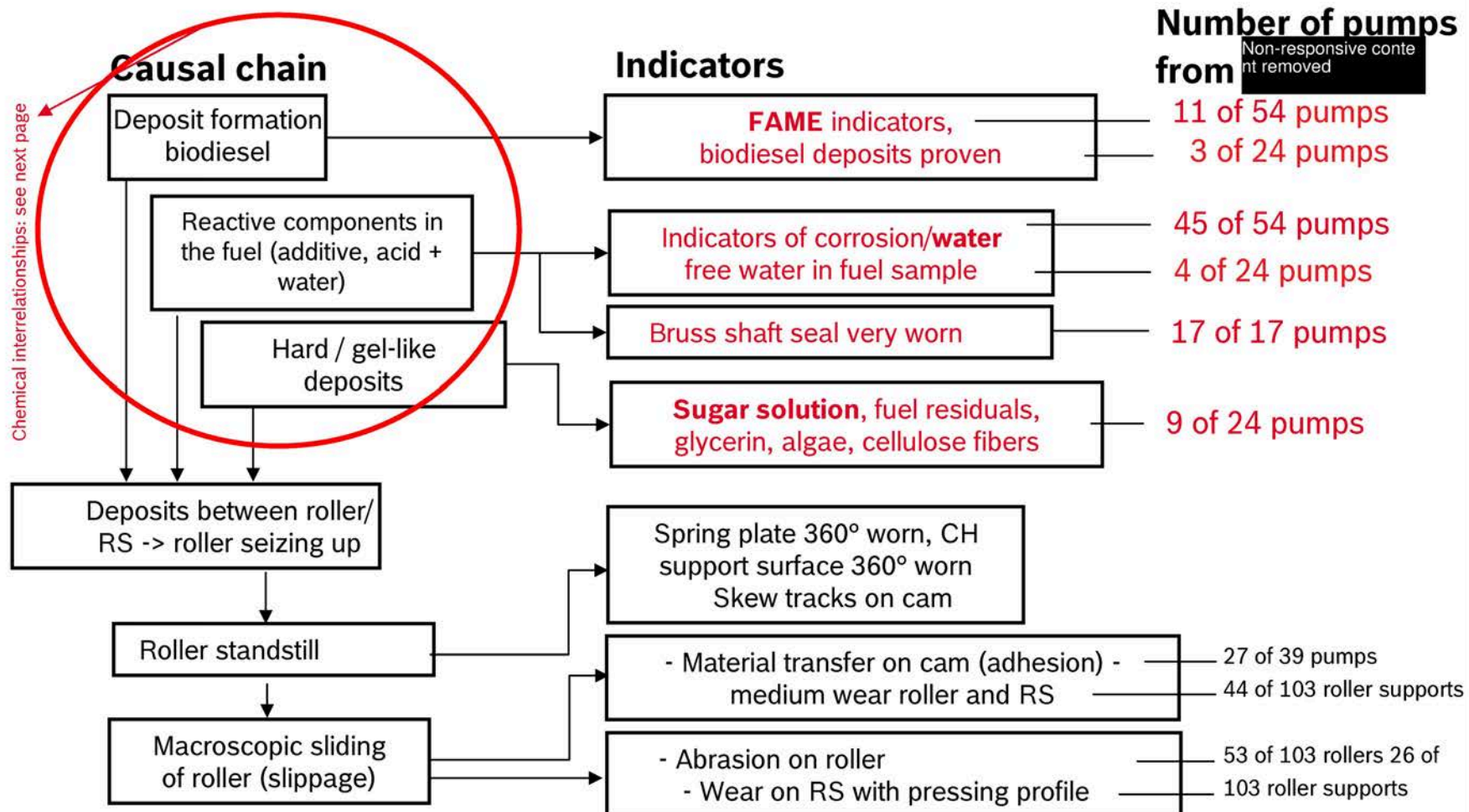


Diesel Systems

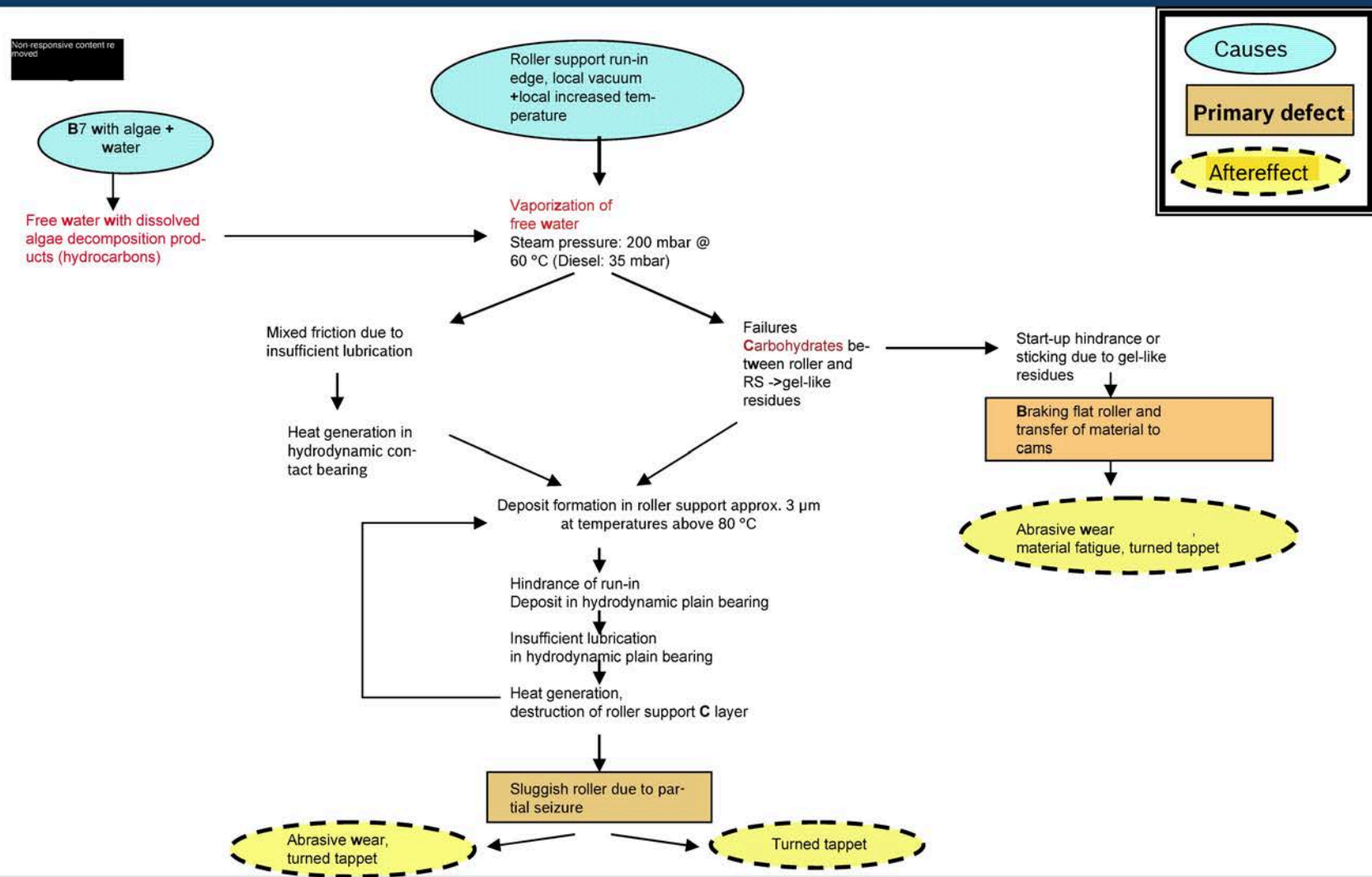


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Possible sequence of damage (fuel aging with the presence of water)



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Causes

Primary defect

Aftereffect



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Differences between CP4.2 and CP4.1

Deposits in roller support arise at increased temperatures.

Causes:

- Through additives at temperatures approx. 140°C
- Through hydrocarbons (algae residues) dissolved in water approx. 80-100°C

Increased temperatures in roller support result from mixed friction.

Causes:

- Fuel influence (viscosity / lubricity / steam pressure)
- Insufficient lubrication (steam pressure increased in presence of kerosene, gasoline, water)

Why is temperature in roller support higher with CP4.2 than with CP4.1?

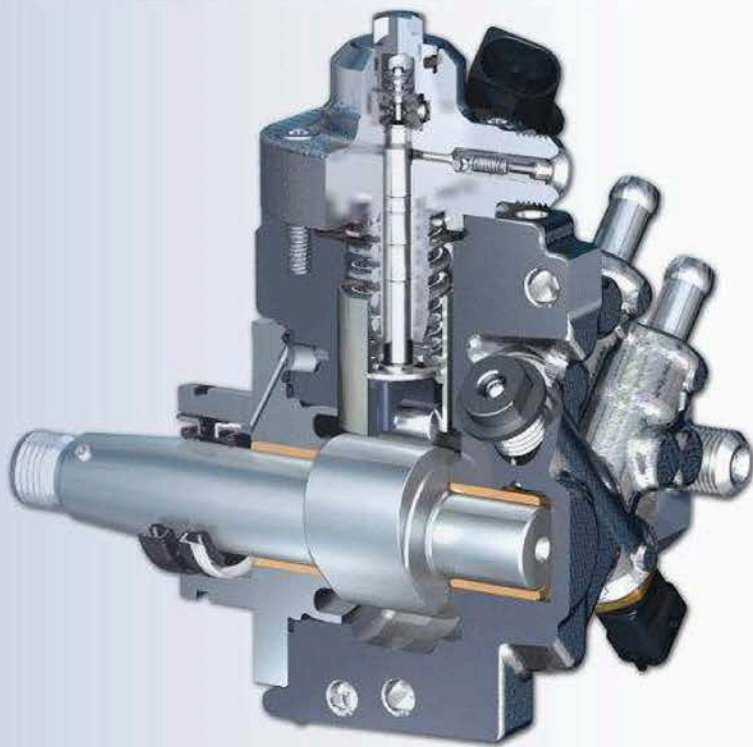
Why is temperature in roller support higher with ccw than with cw?

Differences must be sought in design & application.



7) Comparison CP4.2 vs. CP4.1

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For the CP4.2, the following picture is derived from good pumps with preliminary damage

	Non-responsive content removed	Non-responsive content removed	
W19	4 of 6 right 1 of 6 both sides 1 of 6 left	1 of 2 right	CW
W26		1 of 2 left	CCW

- > The right roller support is primarily affected
- > Disadvantage of the CP4.2 on the right roller support due to “shadowing” of the cam movement
- > This shadowing is not present in the CP4.1 due to handles



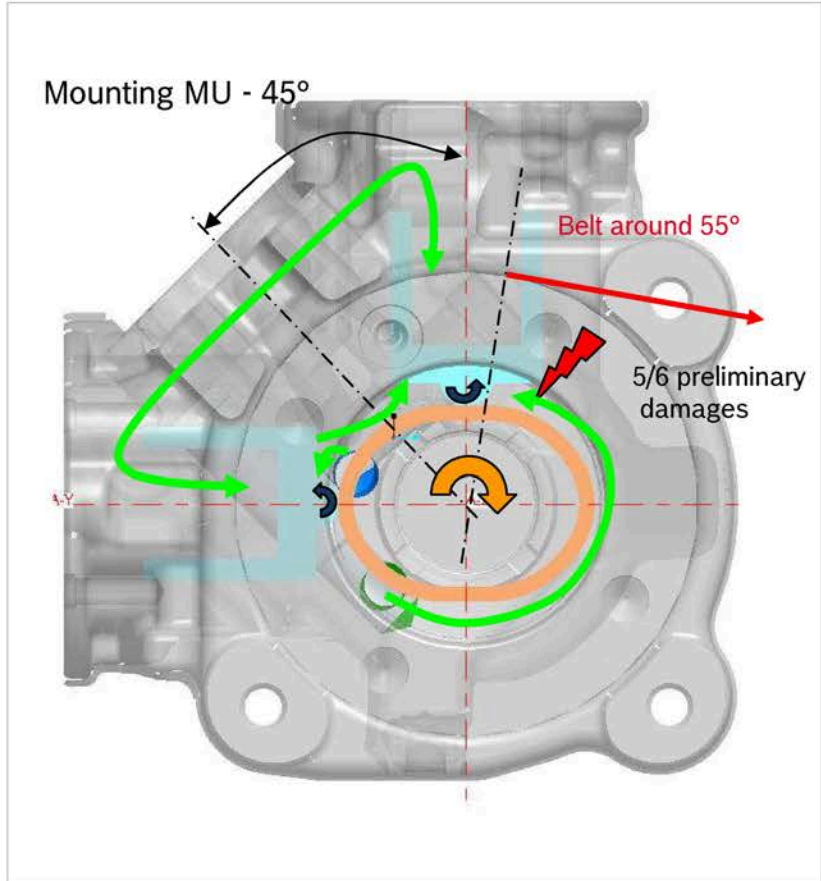
Status Task Force CP4

Comparison of geometry CP4.2 to CP4.1

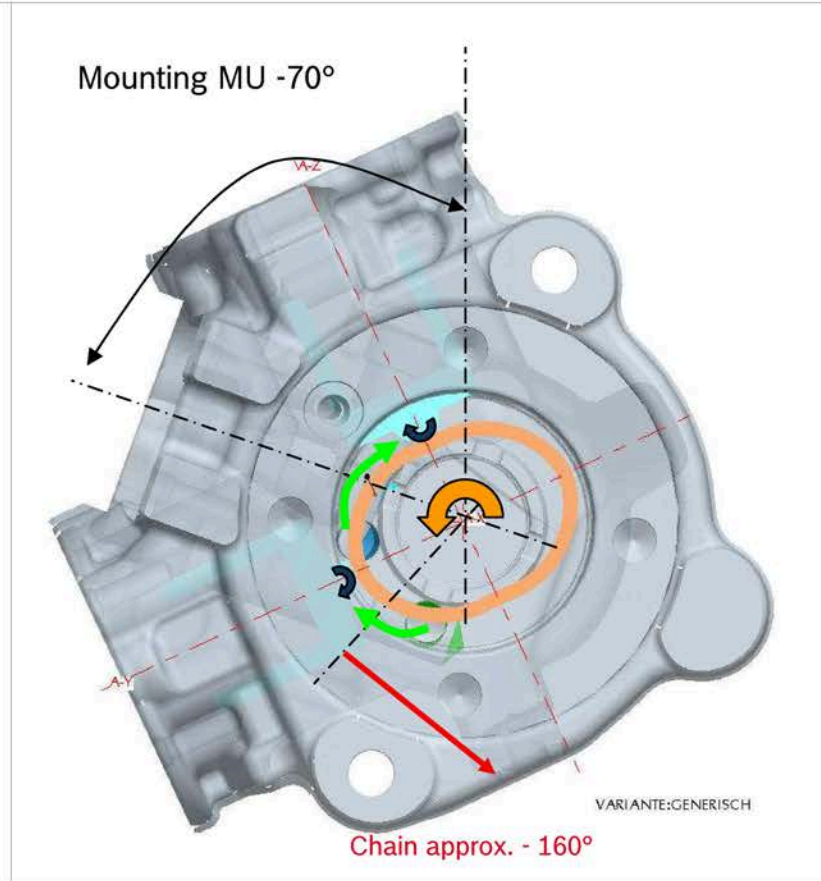
1. Design comparison (inlet/return position)
2. High-speed film (steam pressure)
3. Steam pressure curves
4. Application comparison (inlet/return pressure)



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CP4.2 EFP cw Audi 0 445 010 611 (W19)

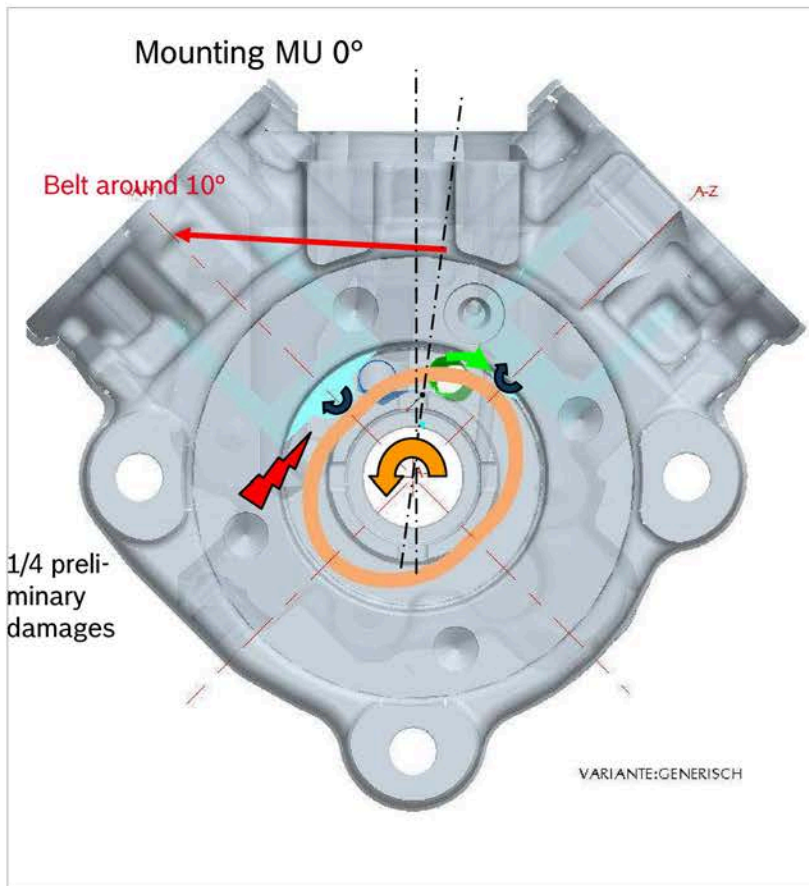


CP4.2 EFP ccw BMW 0 445 010 6xx

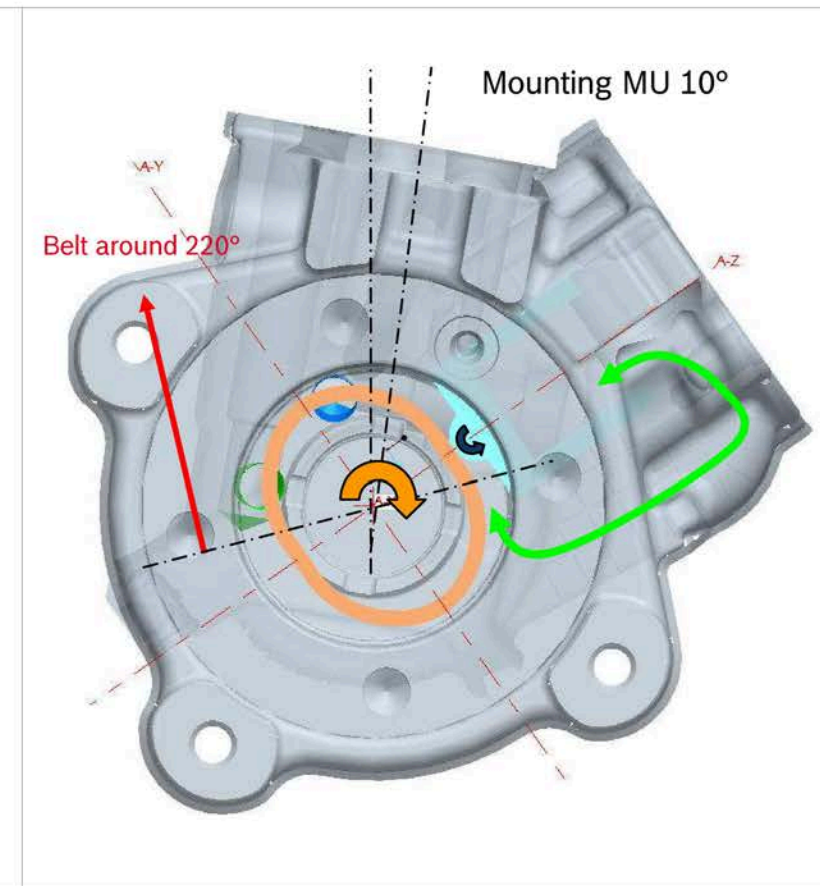
Diesel Systems



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CP4.2 GP ccw Audi W26/W24



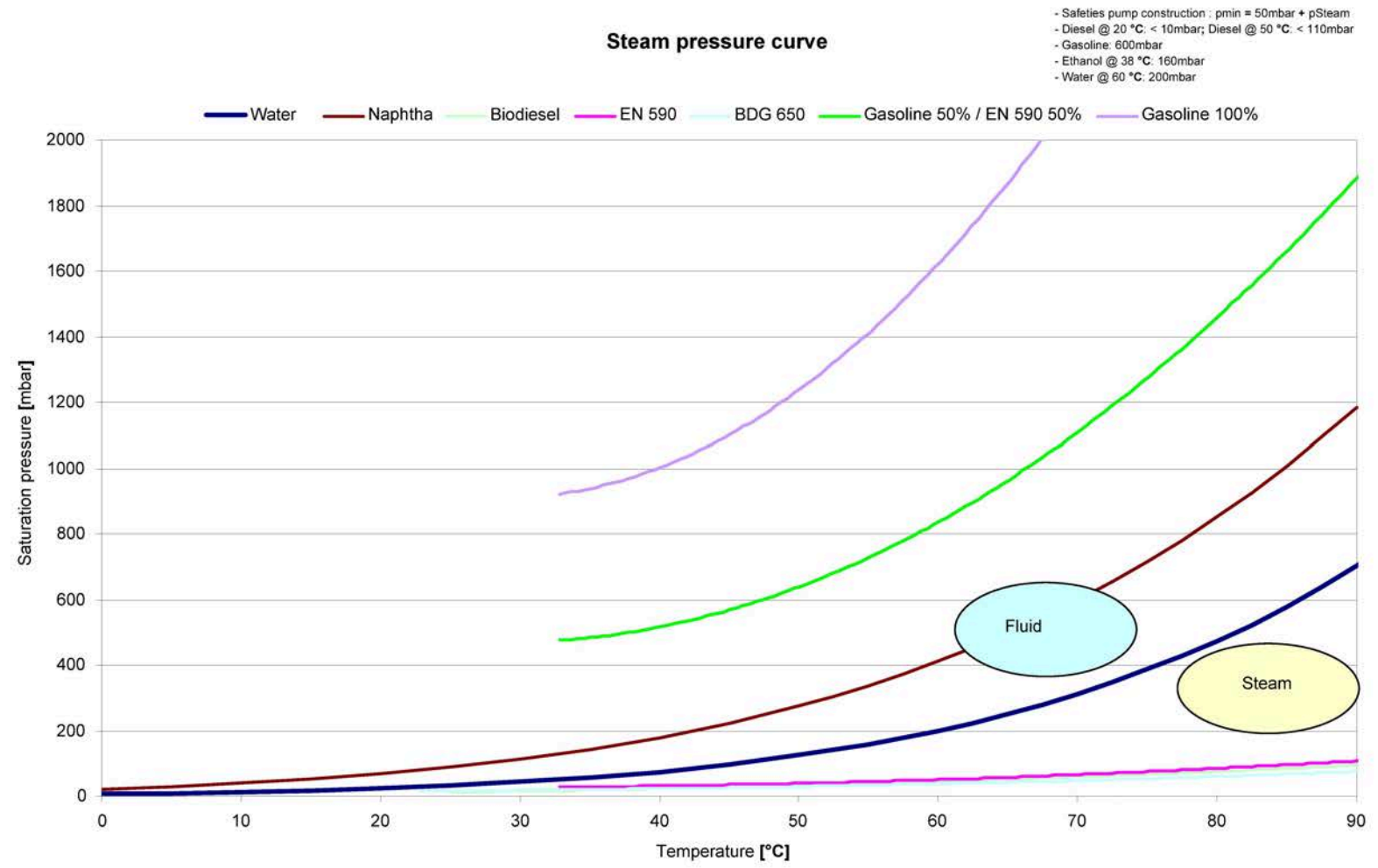
CP4.1 EFP cw VW / Audi

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Status Task Force CP4**3. Application comparison**

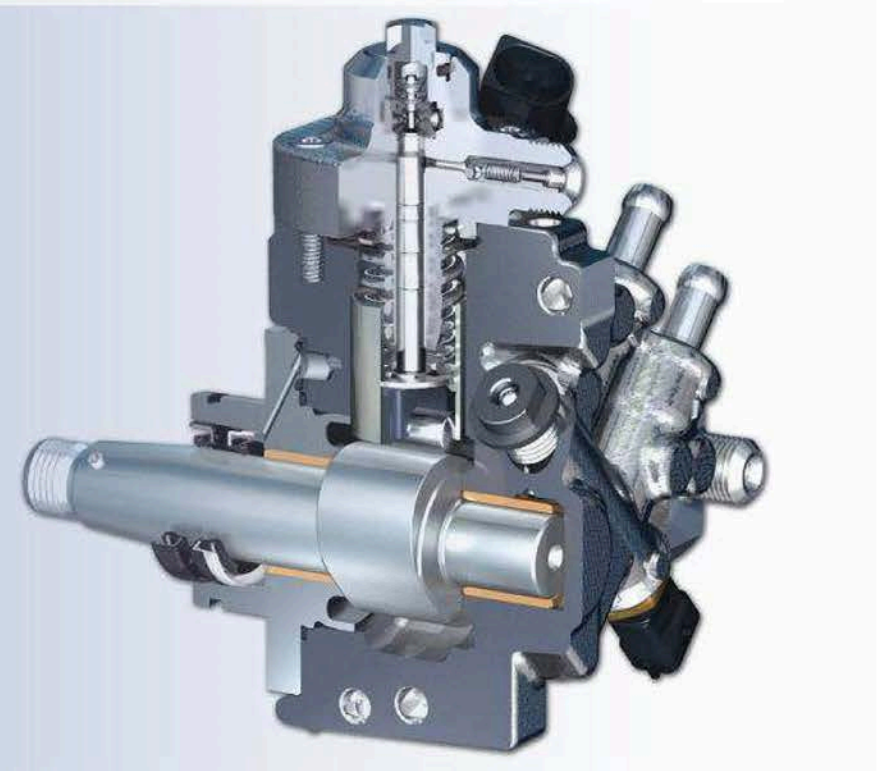
Comparison of **inlet/return** pressure and **differential pressure** via the pump

- 1) W19 vs. W26 (mech. supply pump)
- 2) W19 vs. W24
- 3) W19 vs. R4 with CP4.1 in B8 (with inline EFP)
- 3) W19 vs. W19 with 6 bar low-pressure circuit (non-restricted pump return)
- 4) W19 vs. BMW N57 (inlet pressure-regulated)



8) Possible measures: Anti-wear package 2

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Anti-wear package 2 (RP2)

Objective

Improve start-up behavior of roller, improve robustness with regard to fuel components with lower boiling points (high steam pressure/ absolute)

Characteristics in examination and assessment

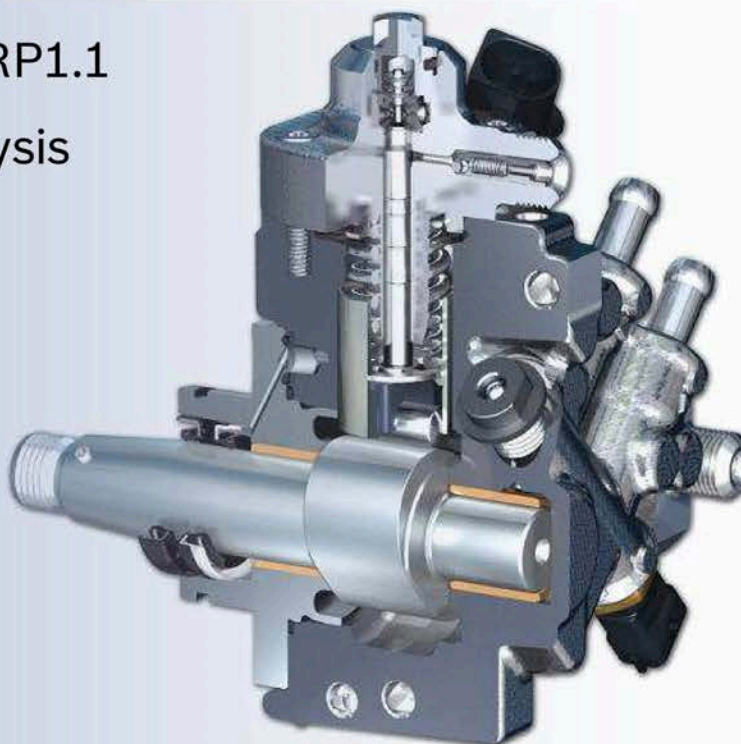
- Roller support with reduced wrap angle
- Position-optimized inlet bore (CP4.2 cw vs. CP4.2 GP)
- Increase of pump interior pressure > 5 bar (overflow valve/governor)
- Cylindrical roller



9) Anti-wear package 1

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- 1) Objectives & characteristics of RP1.1
- 2) Endurance run overview & analysis



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1) Objectives & characteristics of anti-wear package 1.1

Objective

Increasing robustness of drivetrain through increase of lubricating film height between roller support bore and roller.

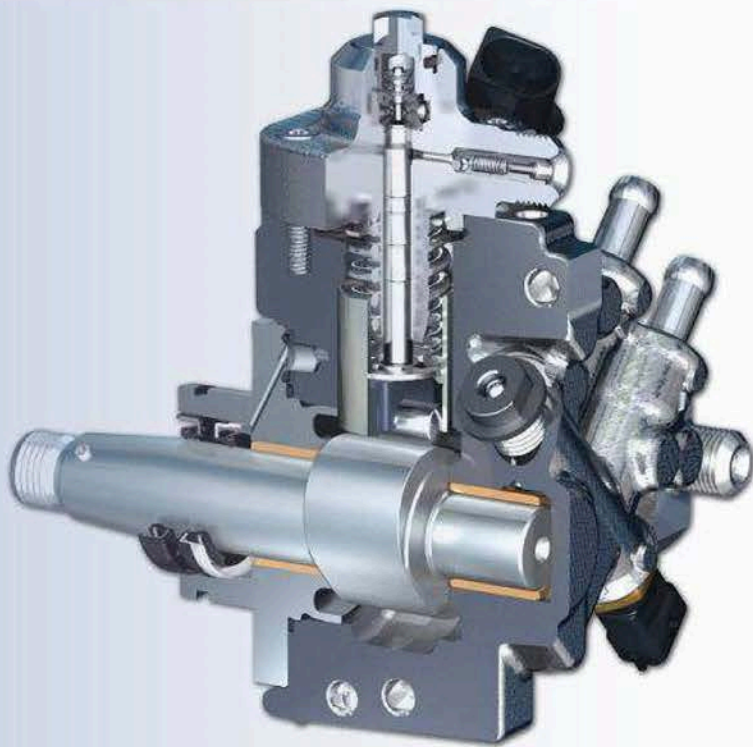
Features of anti-wear package 1.1

- 1) Reduction of roller support roughness in combination with change to C2 layer on roller support.
- 2) Reduction of roller play through smaller roller support bore
- 3) Reduced roller surface through opt. finishing process
- 4) Optimized definition of fine geometry (edge taper) of roller



9.1) Robustness increase based on Stribeck curves

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Diesel Systems

Confidential Non-responsive content removed

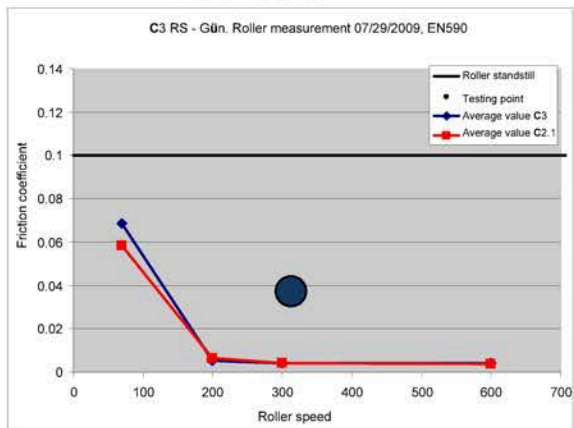


BOSCH

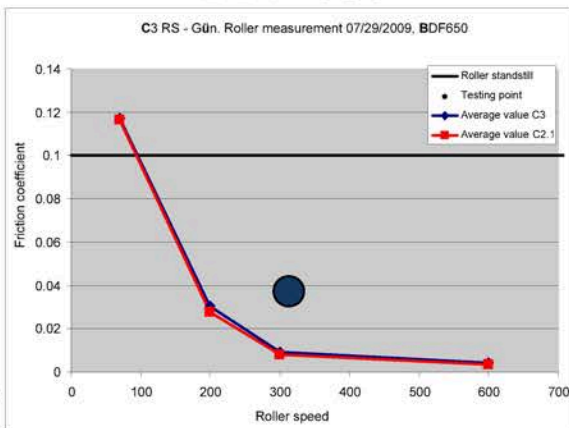
Status Task Force CP4

Comparison of layer system* C3-C2.1 on friction coefficient test bench with

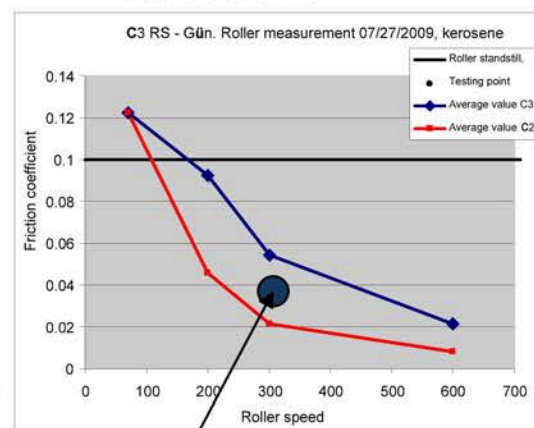
EN 590



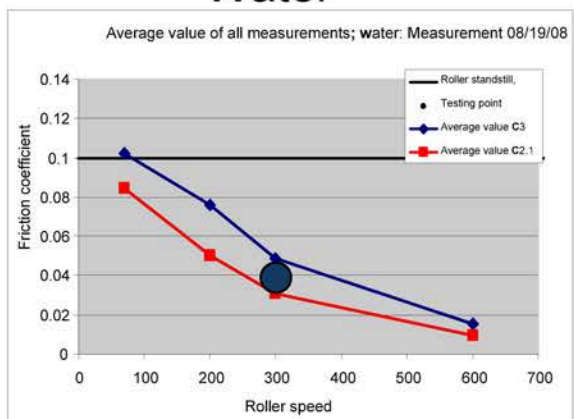
BDF 650



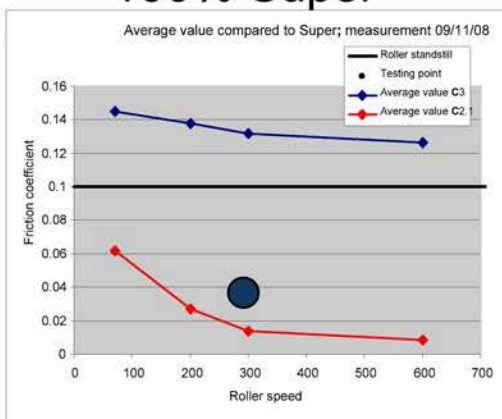
Kerosene



Water



100% Super



Assessment criterion:
friction coefficient

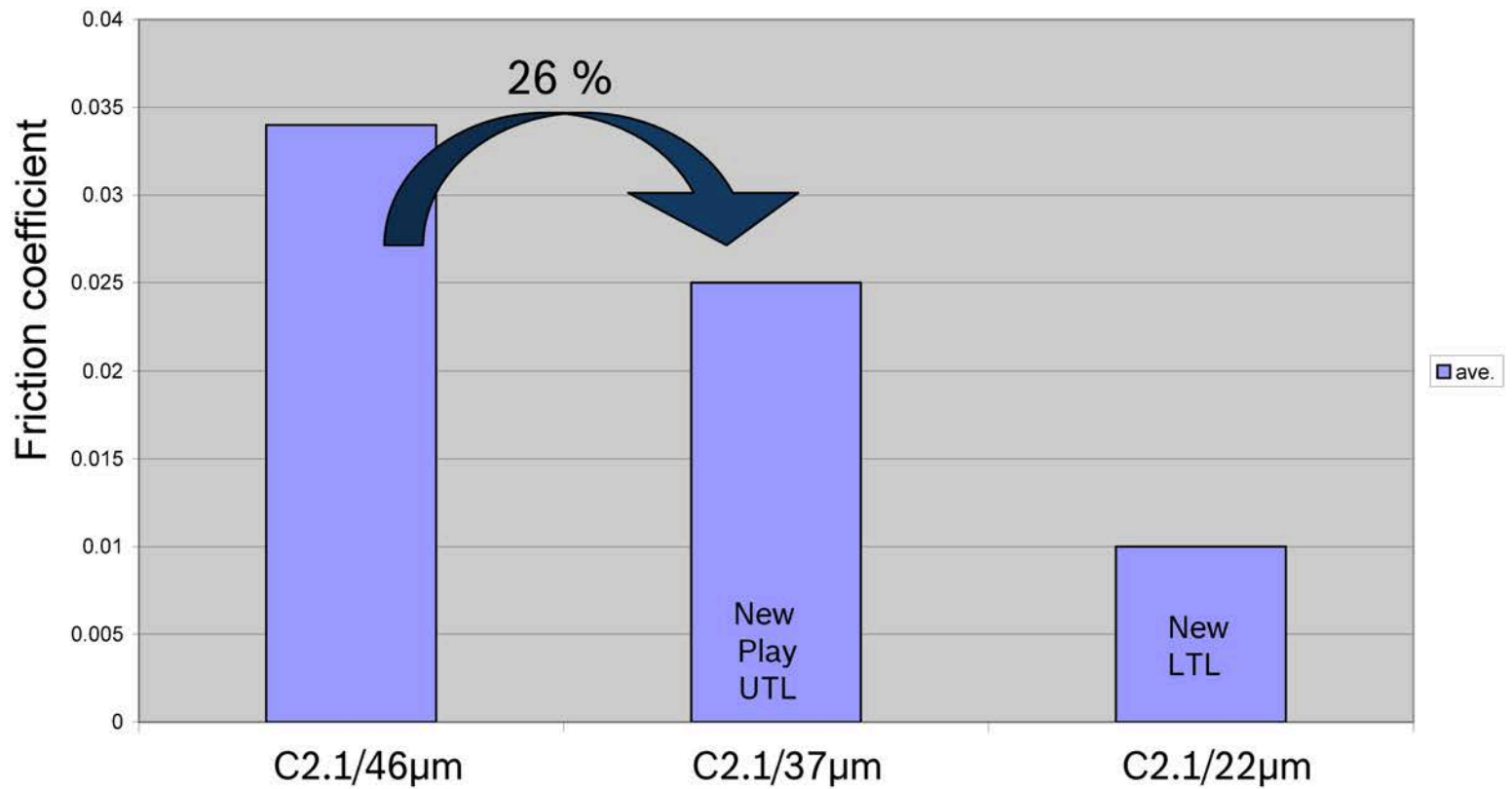
*average comparable play



Status Task Force CP4

Examination with viscosity 1.4mm²/s @40°C (Arctic Diesel)

Testing point 300rpm



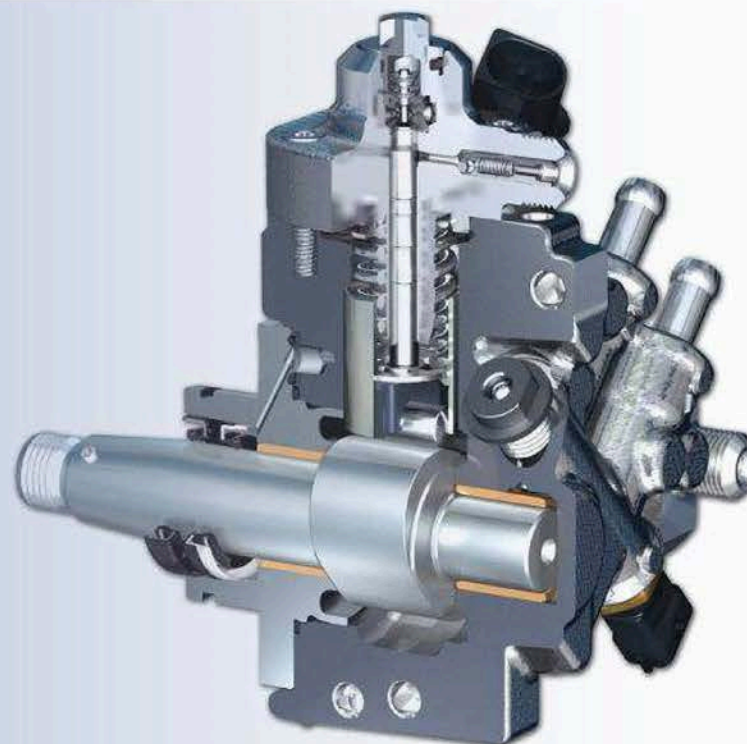
Diesel Systems



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9.2) Robustness increase based on endurance runs

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Diesel Systems



Status Task Force CP4

Test parts and test conditions**C3 RS (tappet good and bad),** Non-responsive content removed

- Tappet “good”: Roller support without texture, roughness/play medium (2010-CP4_0727)
- Tappet “bad”: Roller support without texture, roughness/play medium (2010-CP4_0728)

C2.1 RS (best parts), Non-responsive content removed

- Tappet “best”: Low play approx. 24 μm , Rmr 0.1, depth>90%, Rv<0.2 (2010-CP4_0029)
- Tappet “best”: Low play approx. 24 μm , Rmr 0.1, depth>90%, Rv<0.2 (2010-CP4_0030)

C2.1 RS (best parts), Non-responsive content removed

- Tappet “best”: Low play approx. 18 μm , Rmr 0.1, depth>90%, Rv<0.2 (2010-CP4_0053)
- Tappet “best”: Low play approx. 18 μm , Rmr 0.1, depth>90%, Rv<0.2 (2010-CP4_0054)

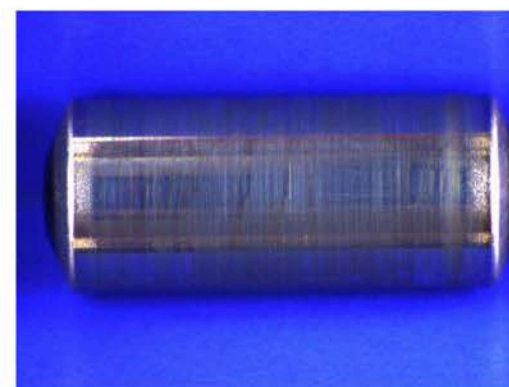
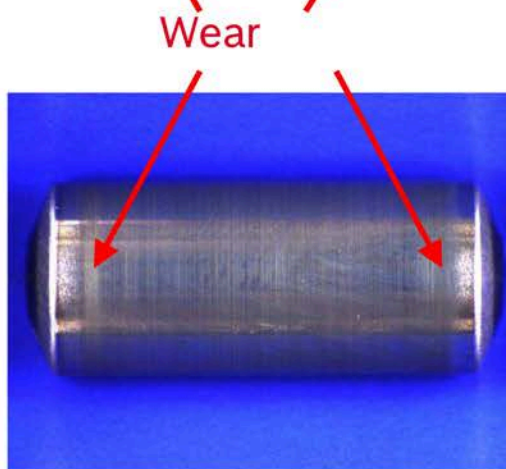
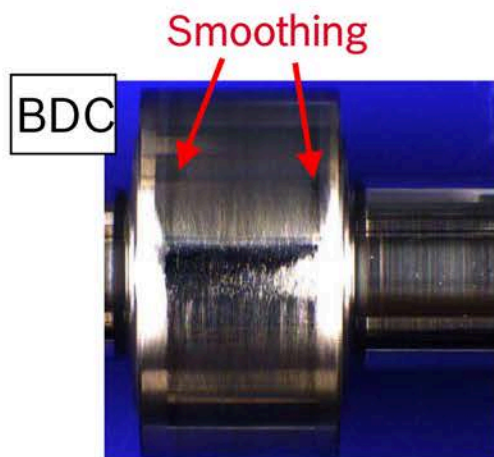
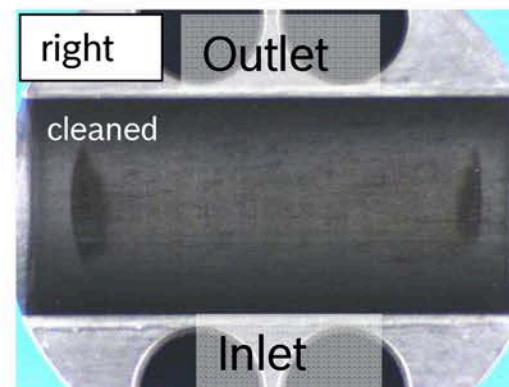
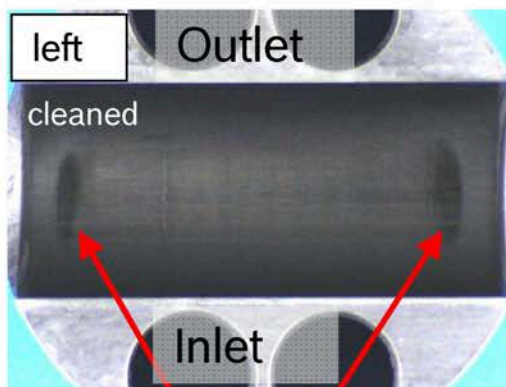
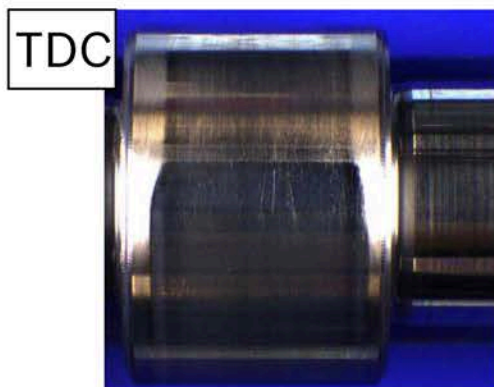
Overload test drivetrain CP4 Non-responsive content removed

- > Basic pump 0445010617
- > Variant 1: Mixed friction at low RPMs
 - Run-in program (15 h, 4,000 rpm, 2,000 bar, 40°C, Arctic Diesel Cl. 4.
 - Endurance run program (150 h, 600 rpm, 2,300 bar, 90°C, Arctic Diesel Cl. 4.



Status Task Force CP4

Pictures RS L C3 good 35 μm (2010-CP4_0727)

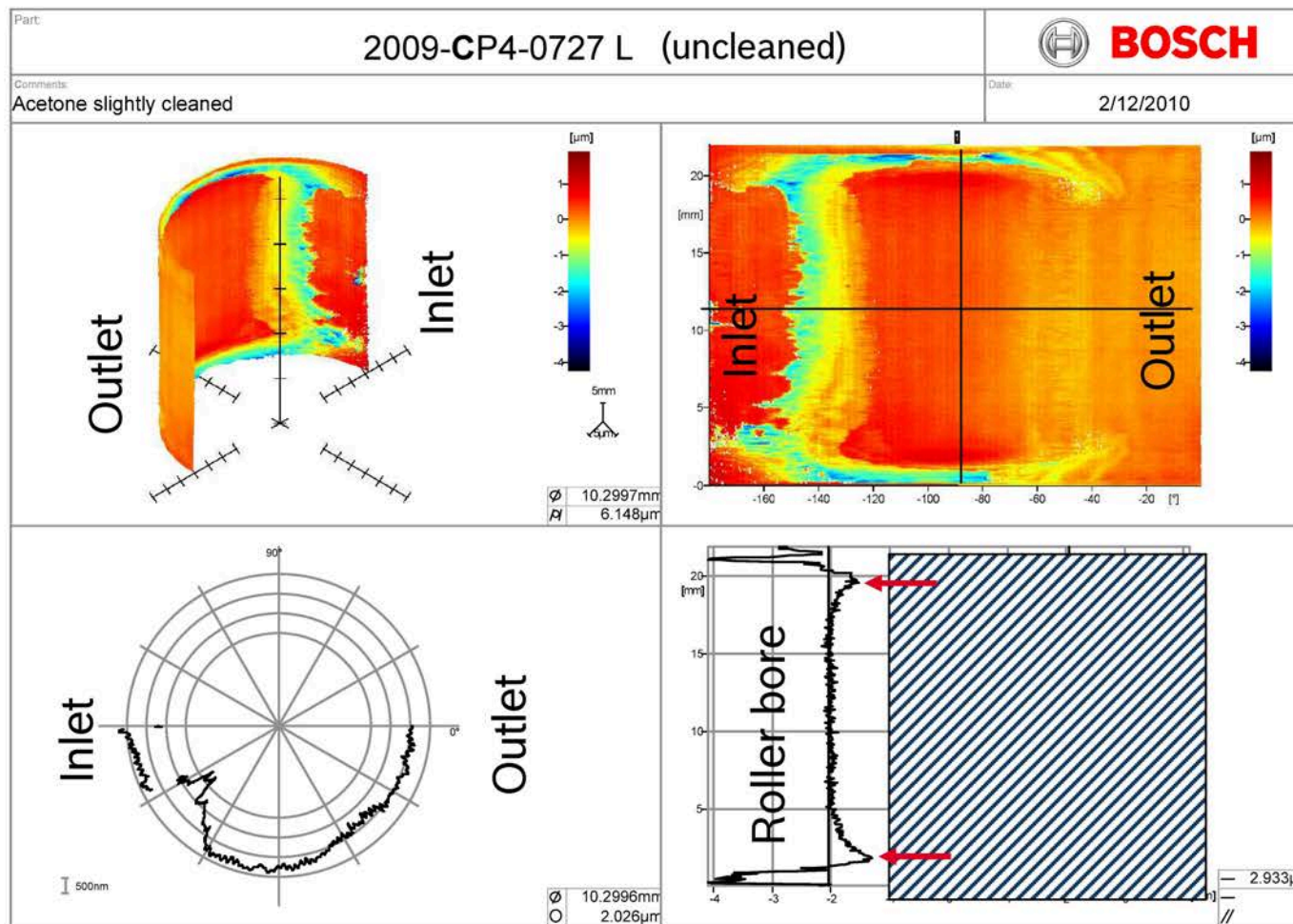


Diesel Systems



Status Task Force CP4

WP measurement RS L C3 good 35 μm (2009-CP4_0727)

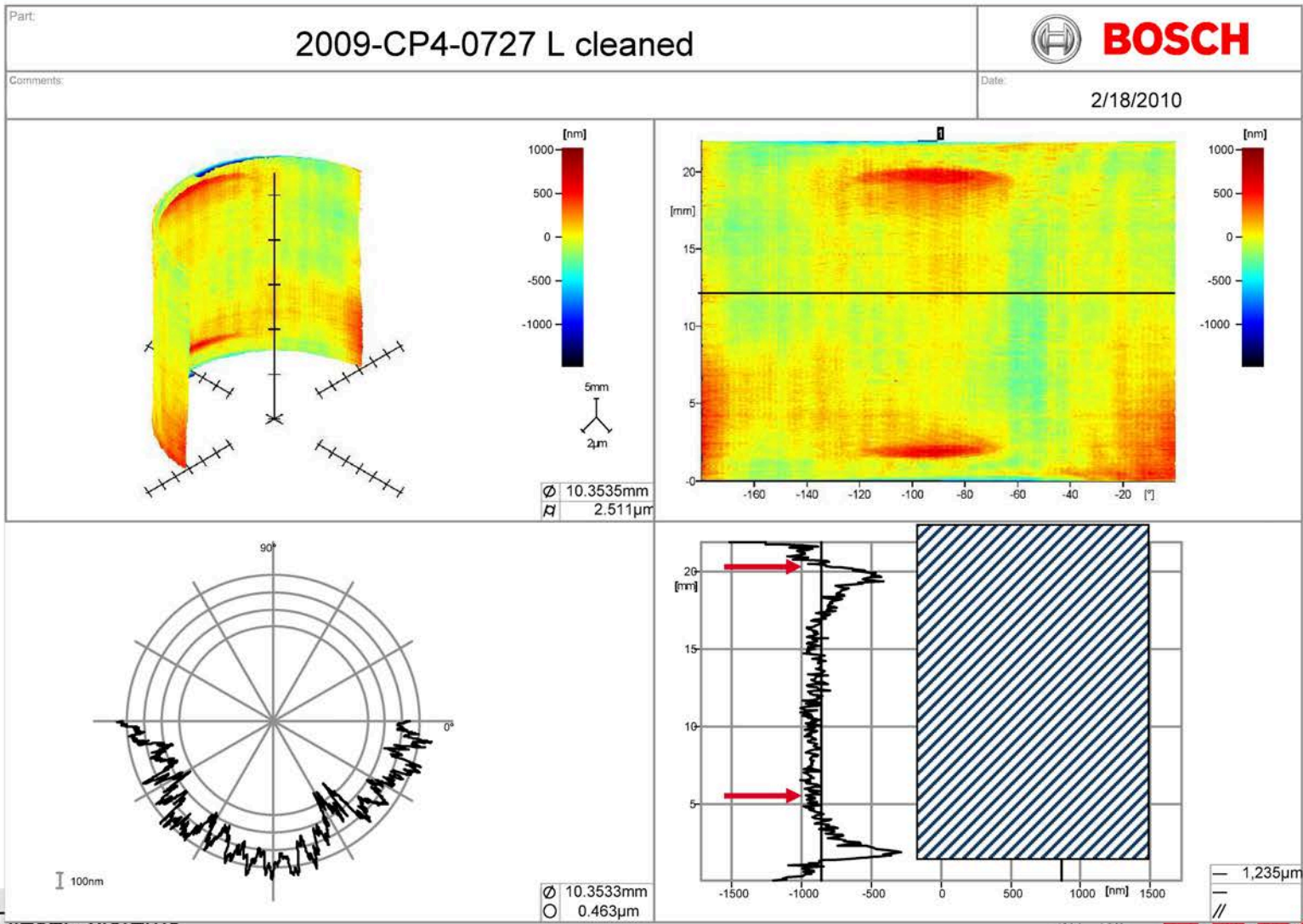


Diesel Systems



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Status Task Force CP4



Dieser systems

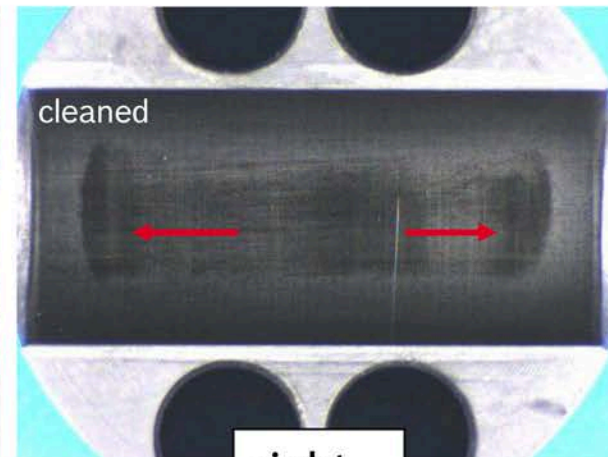
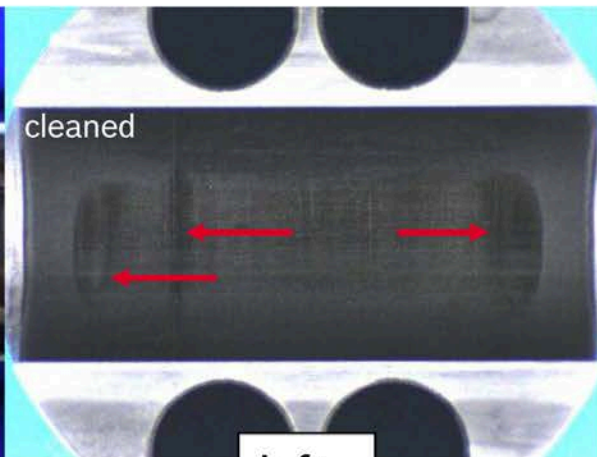
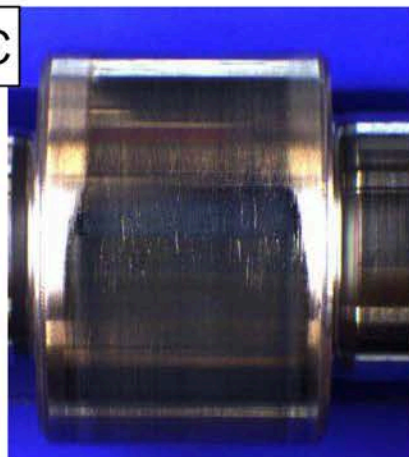


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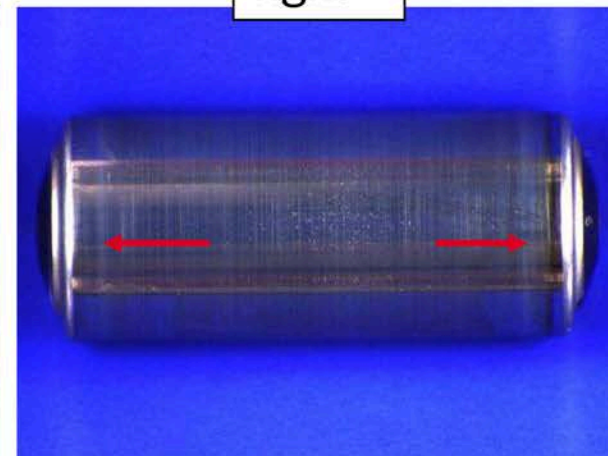
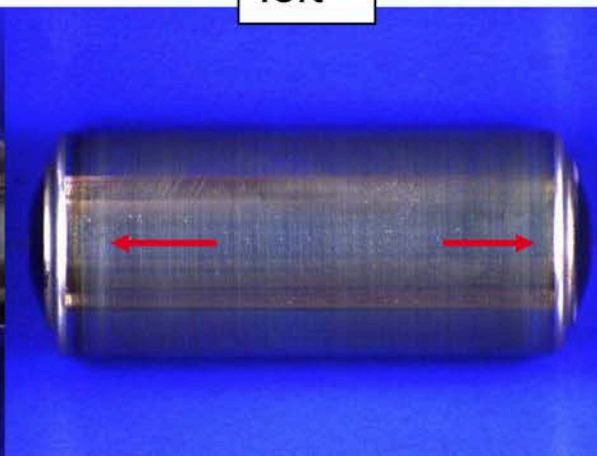
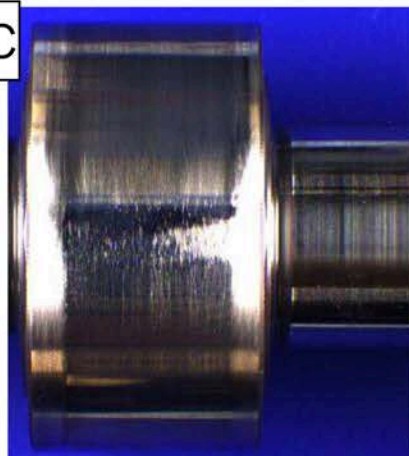
Status Task Force CP4

Pictures RS L C3 bad 35 µm (2010-CP4_0728)

TDC



BDC

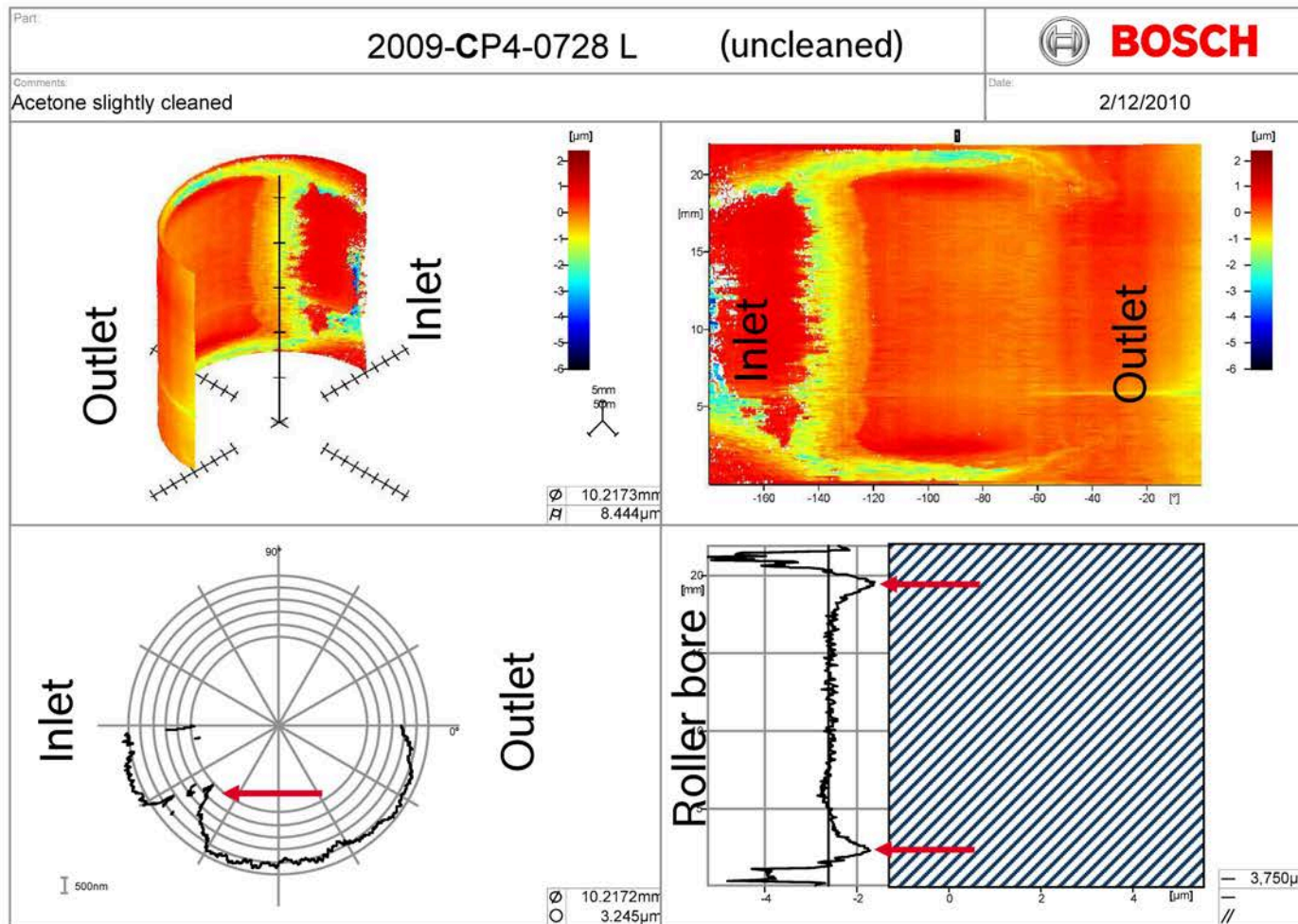


Diesel Systems



Status Task Force CP4

WP measurement RS L C3 bad 35 μm (2009-CP4_0728)



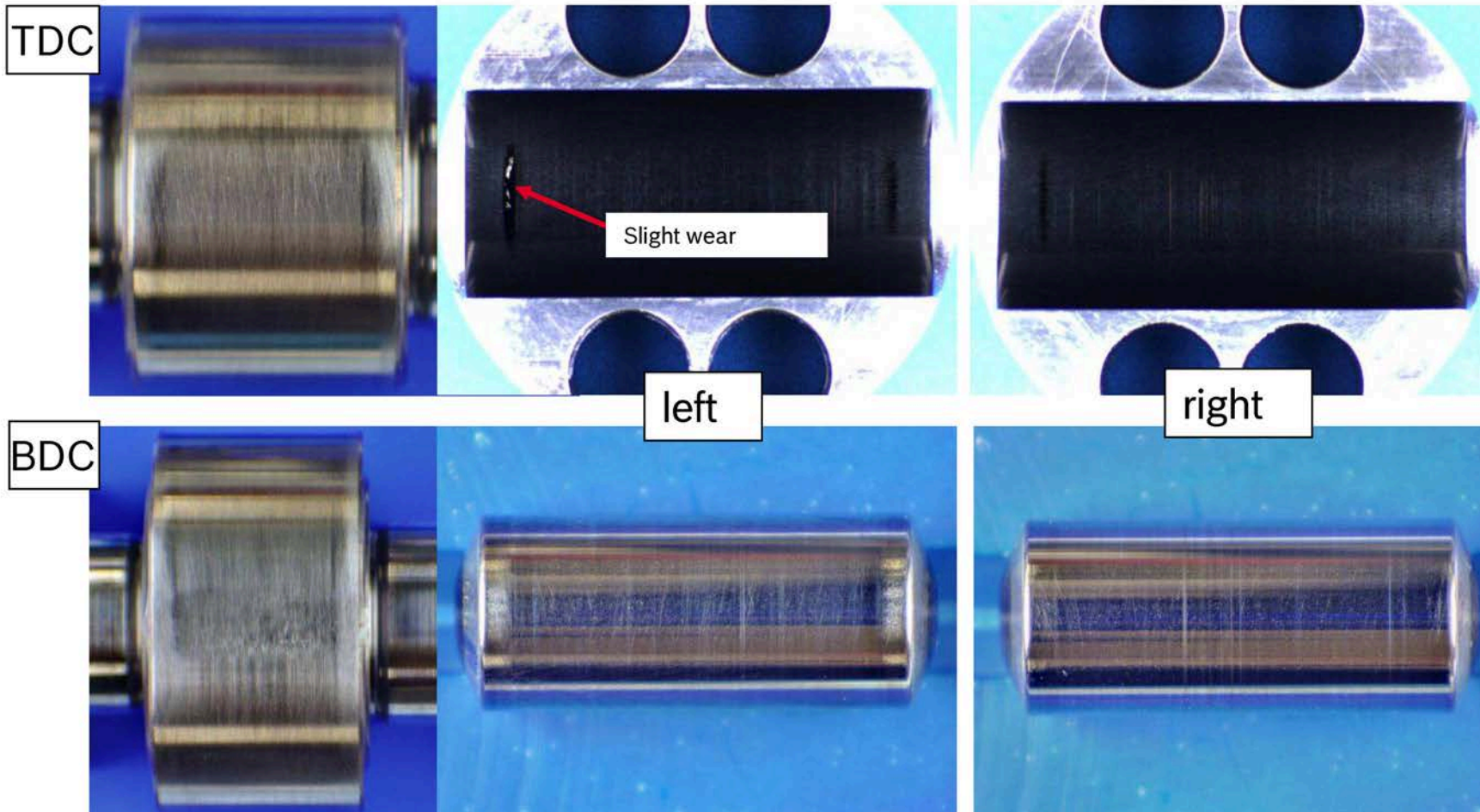
Diesel Systems



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Status Task Force CP4

Pictures C2.1 good 18 μm (2010-CP4_0053)



TDC

Slight wear

left

right

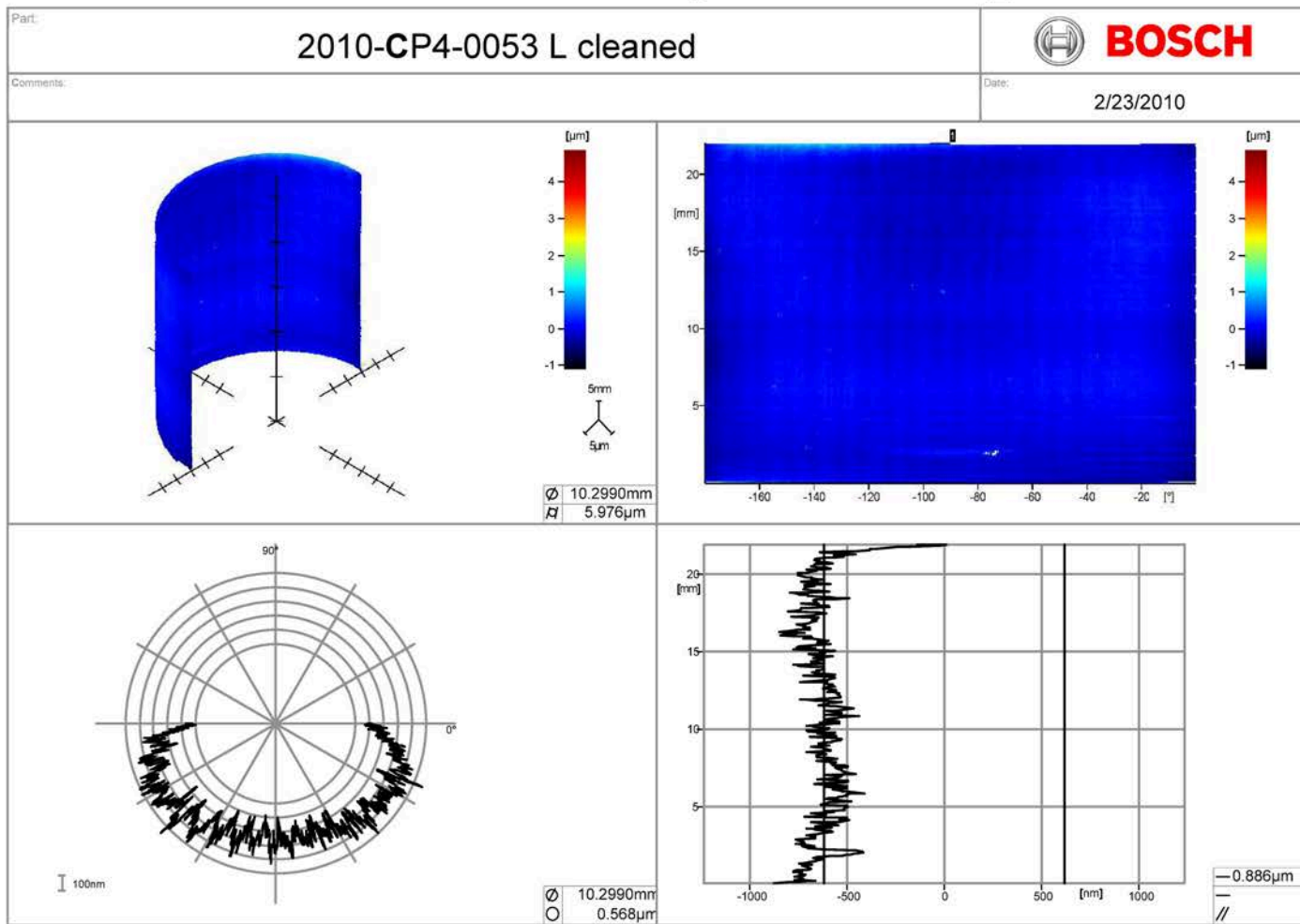
BDC

Diesel Systems



Status Task Force CP4

WP measurement RS L C2.1 best 18 μm (2010-CP4_0053)



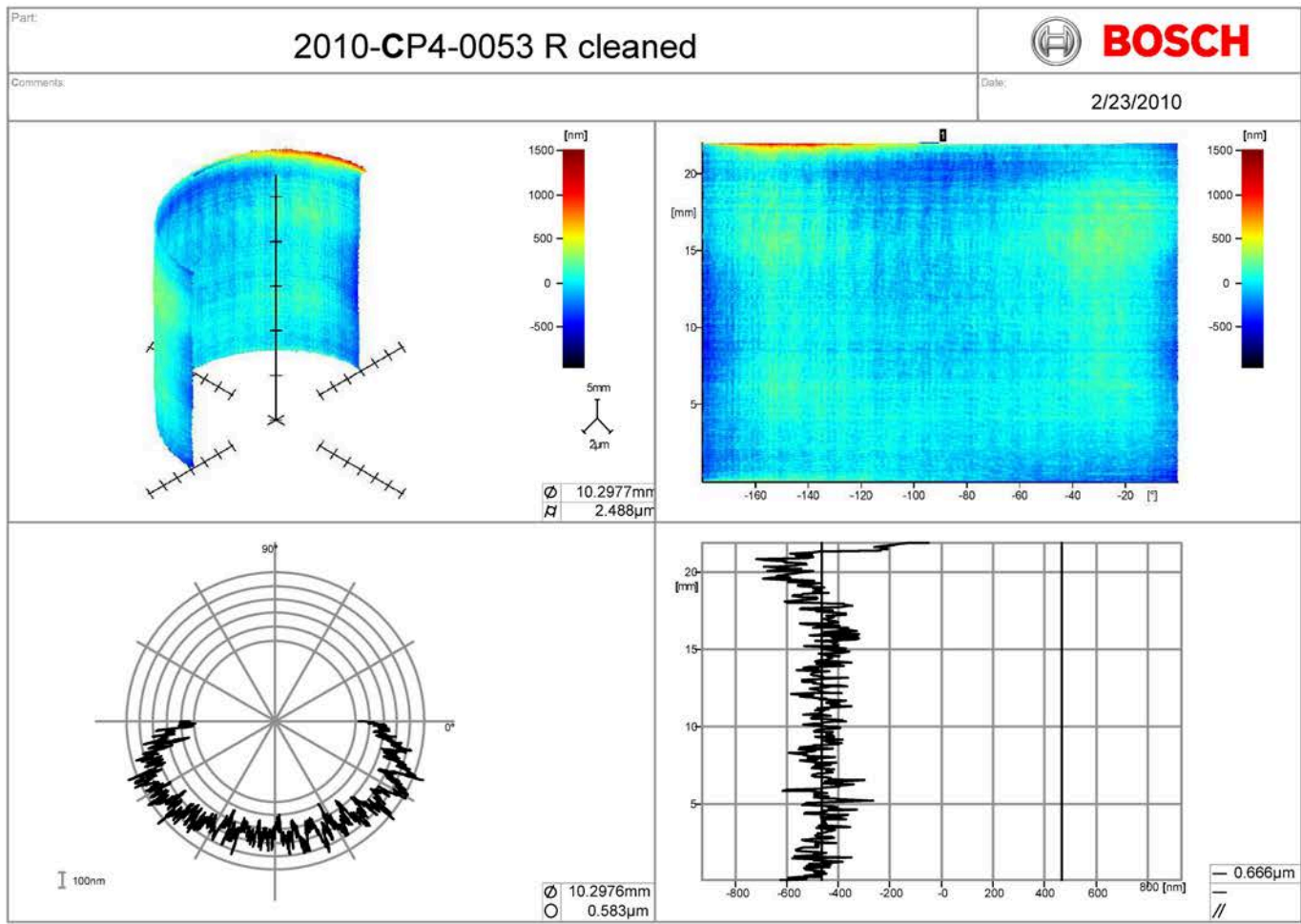
Diesel Systems



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Status Task Force CP4

WP measurement RS L C2.1 best 18 μm (2010-CP4_0053)



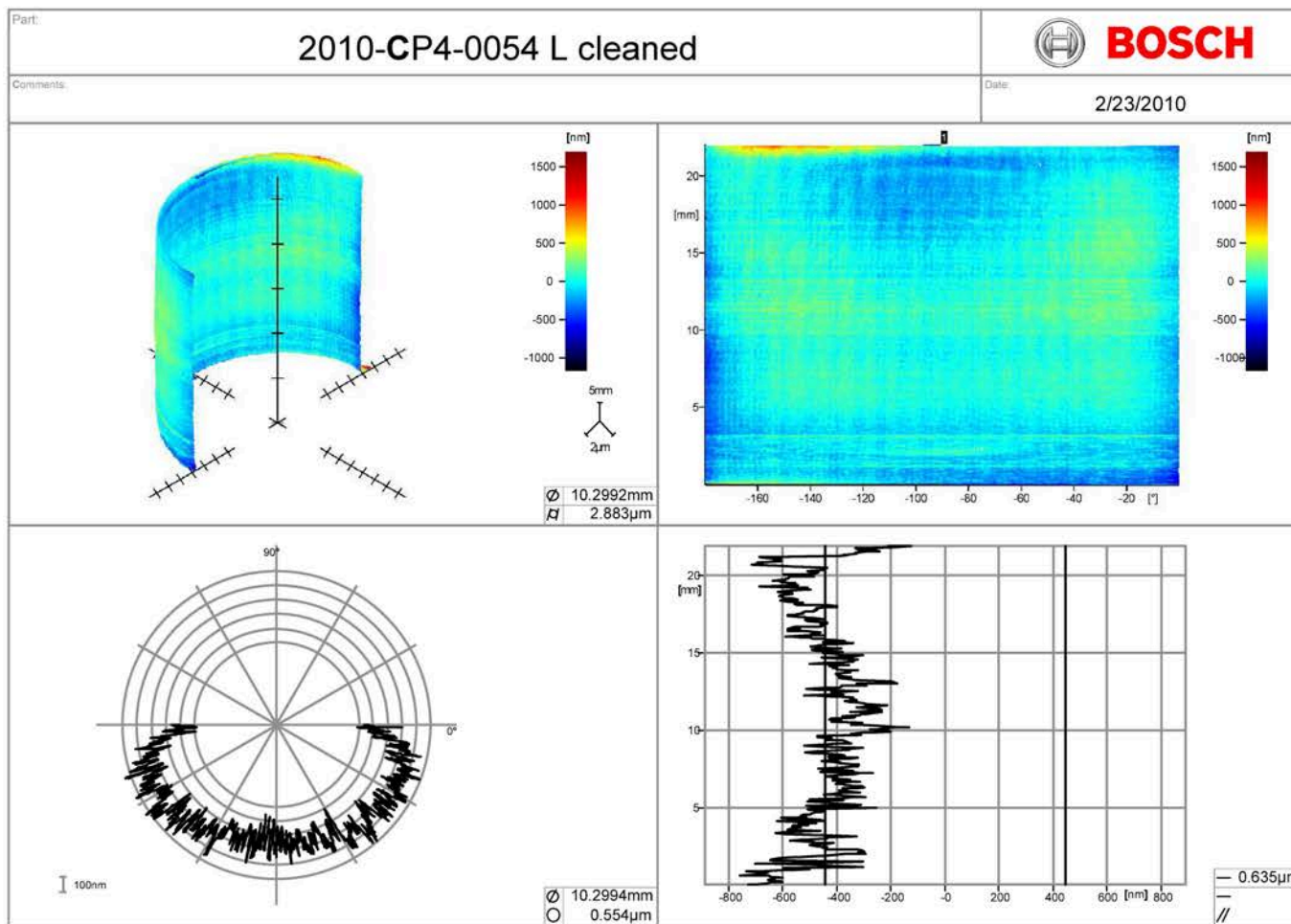
Diesel Systems



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Status Task Force CP4

WP measurement RS L C2.1 best 18 μm (2010-CP4_0054)



Diesel Systems



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Status Task Force CP4

Overload test conditions

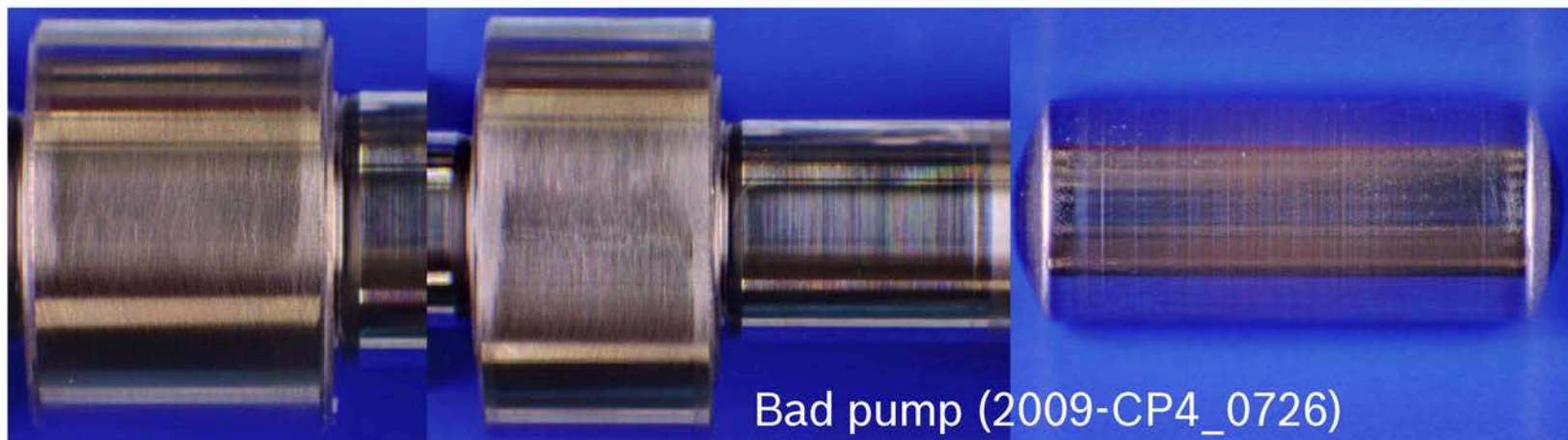
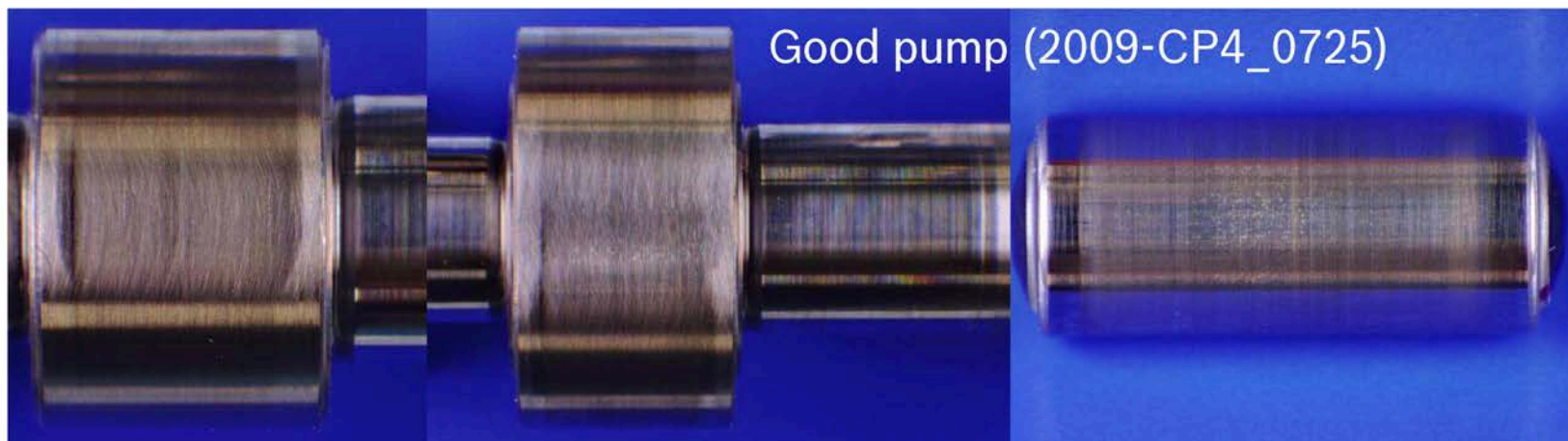
- > "Mixed friction" variant
- > 2x CP4.1, lift 5.25 mm (part no. ...508, VW R4 BIN5)
- > Arctic Diesel Class 4
- > 90° inlet temperature
- > 2,300 bar
- > 600 rpm
- > 150 h

- > One pump each with good and bad parts tappet assembly (C3 layer), that is, bad parts are scrap from visual inspection (series manufacturing)
 - VVT 2009-CP4_0725 (good), Non-responsive content removed
 - VVT 2009-CP4_0726 (bad), Non-responsive content removed



Status Task Force CP4

Diagnosis pictures camshaft, roller

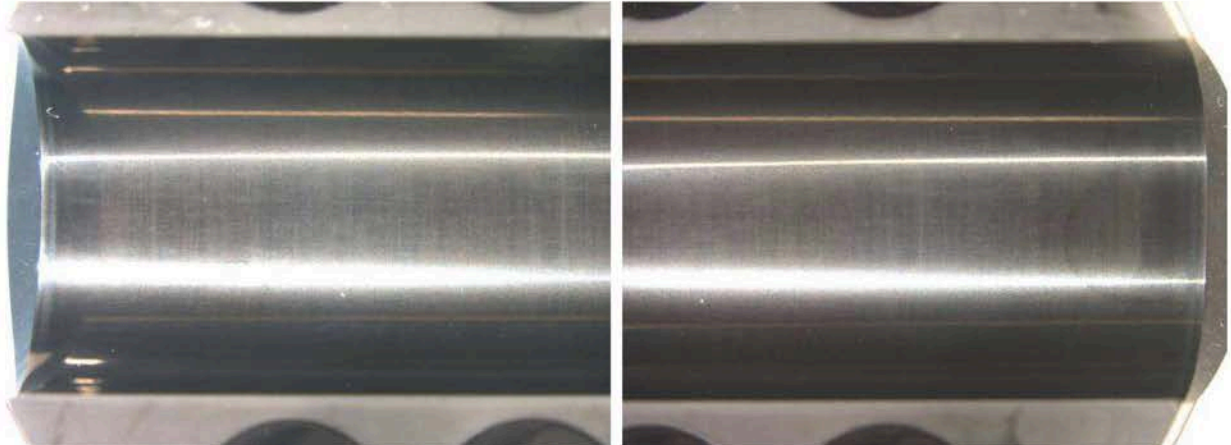


Diesel Systems

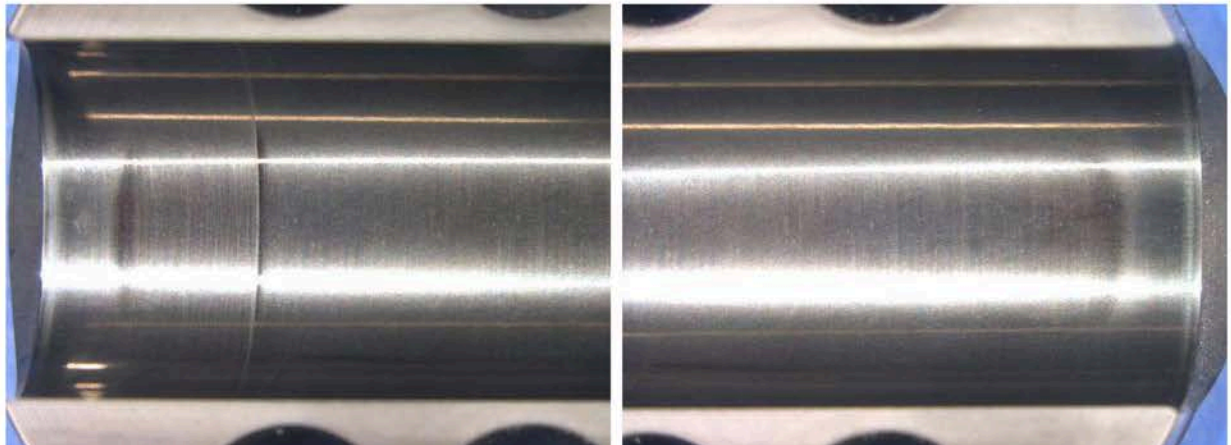


Status Task Force CP4

Diagnosis pictures roller support



Good pump
(2009-CP4_0725)



Significant
smoothing

Bad pump (2009-
CP4_0726)

Diesel Systems



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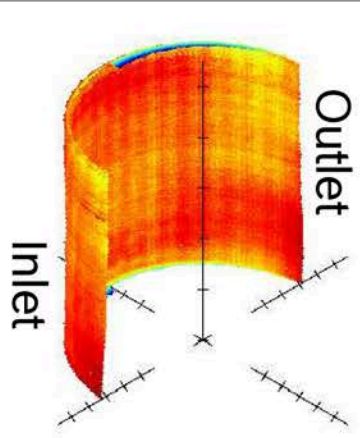
Status Task Force CP4

RS 6007-4984 Good pump
(2009-CP4_0725)



2.02.2010

Kommentar:



[nm]

500

0

-500

-1000

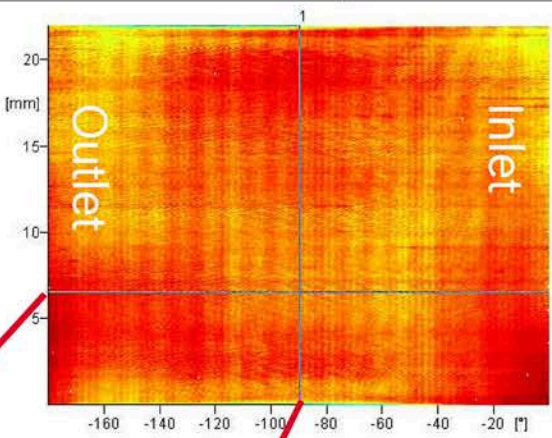
-1500

5mm

2µm

∅ 10.1604mm

R 2.213µm



[nm]

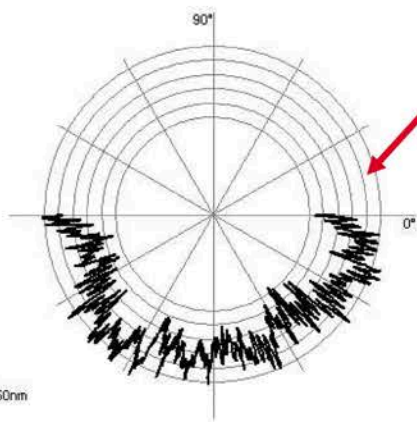
500

0

-500

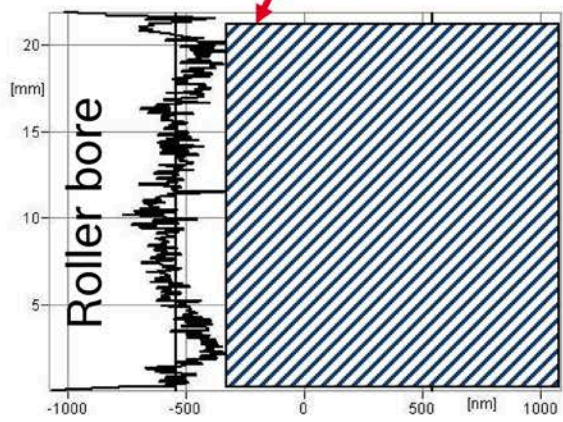
-1000

-1500



∅ 10.1607mm

○ 0.316µm



0.771µm

—

—

//

Diesel Systems



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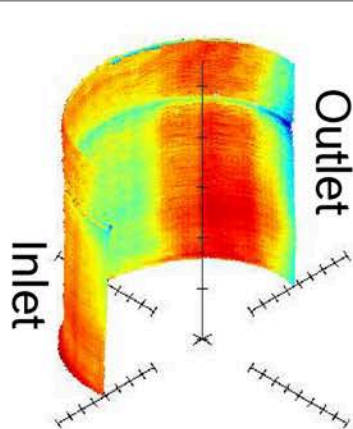
Status Task Force CP4

6007-0316 Bad pump
(2009-CP4_0726)



Kommentar:

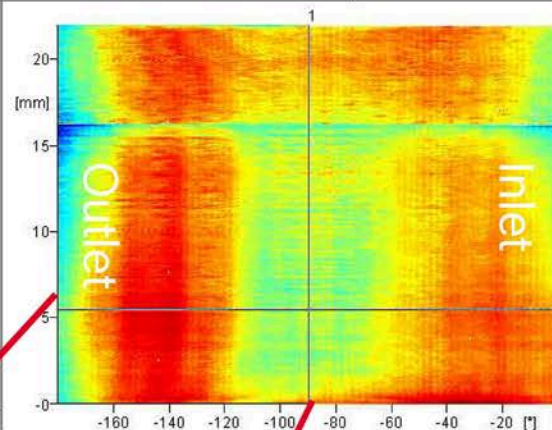
Datum: 2.02.2010



[nm]
1000
500
0
-500
-1000
-1500
-2000

5mm
2µm

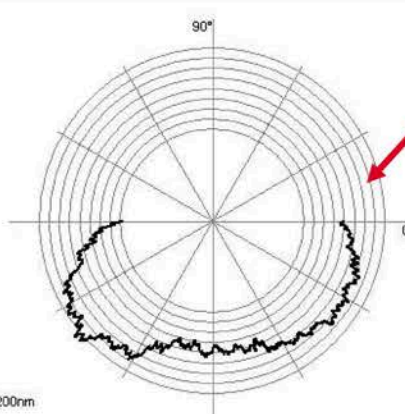
∅ 10.1698mm
// 3.213µm



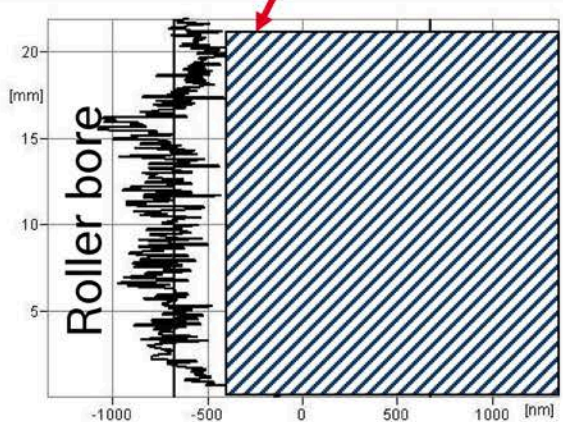
[nm]
1000
500
0
-500
-1000
-1500
-2000

20
15
10
5
0

-180 -140 -120 -100 -80 -60 -40 -20 [°]



∅ 10.1646mm
○ 1.771µm



0.962µm
//

Diesel Systems

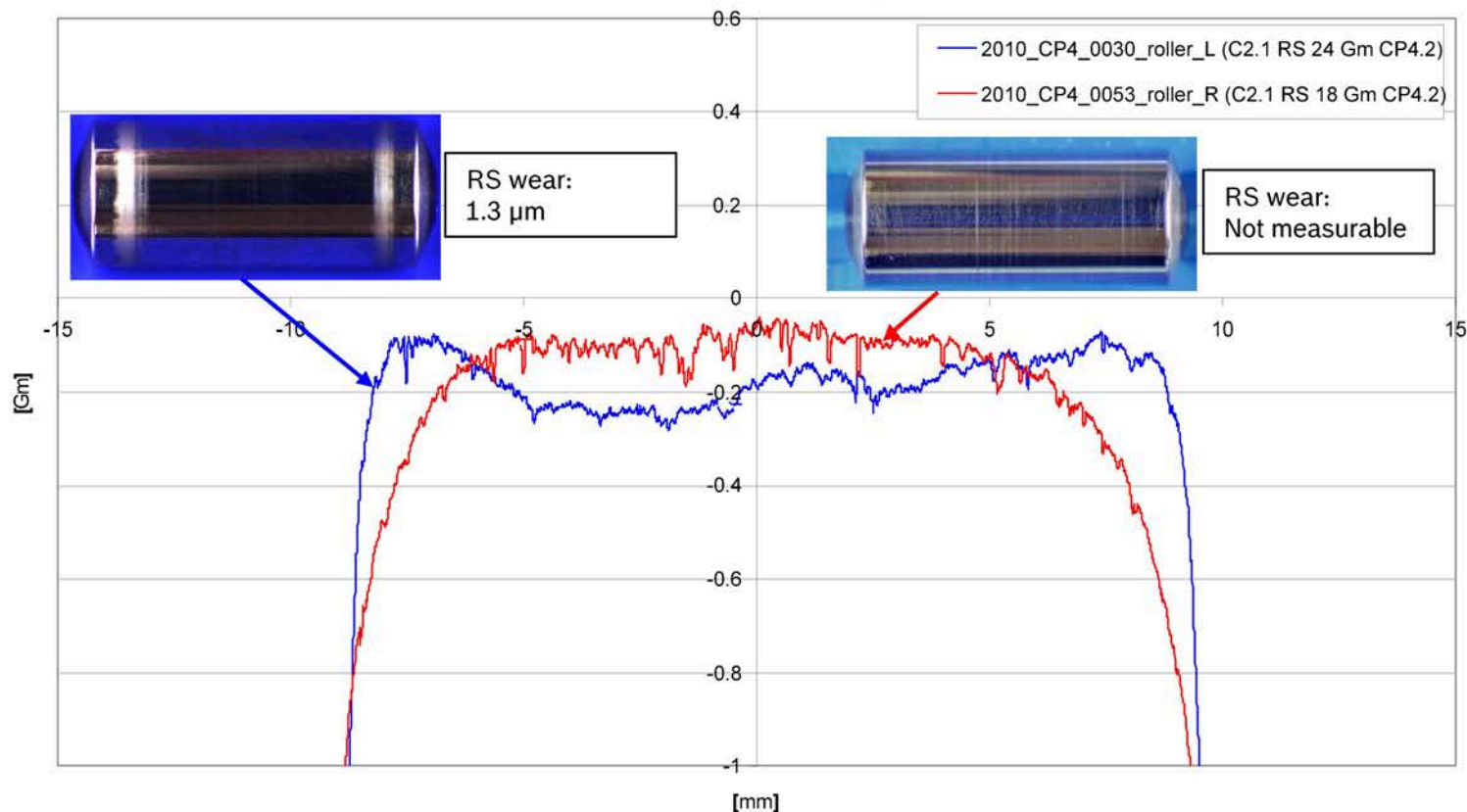


BOSCH

Status Task Force CP4

Roller contour plots

Contour plots of roller with (C2.1 RS 24/18 Gm CP4.2)



Diesel Systems

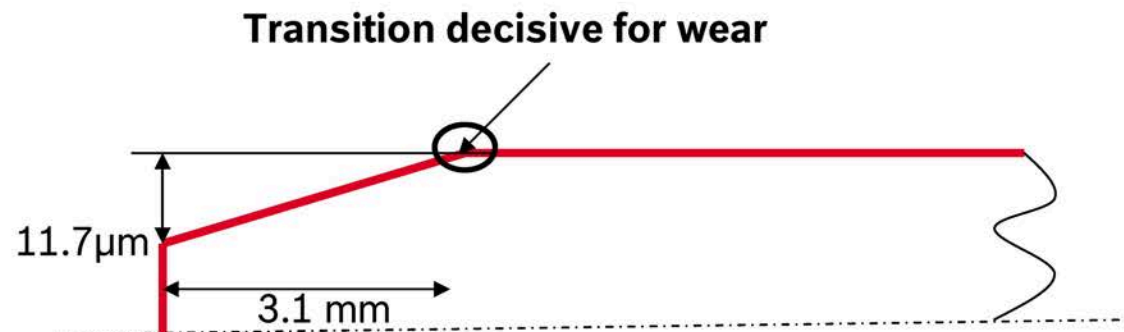


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Status Task Force CP4

Correlation smoothing at edge

- > Subsequent measurement of parts showed that smoothing at the edge of the roller support were created during operations under QALT conditions due to the shape of the slender taper on the roller
- > Flat transition of the slender taper results in maintenance of the lubrication gap at the edge of the roller even with extremely small lubrication gaps (reduced mixed friction).



Status Task Force CP4

Backup



Status Task Force CP4

Proof of robustness

End of Life QALT endurance runs @ 600rpm, 2,300bar, 90°C Arctic Diesel) with

- (A1)₁ (C1)₂ 1 x roller support C3 (max.)* and roller with “edge” (convex)
 (A1)₁ (C2)₂ 1 x roller support C3 (max.)* and roller without “edge” (convex)
 (S1)₃ (S2)₄ 1 x RP1 roller support (max.)* and roller without “edge” (convex) (=RP1.1)
 (B2)₃ (D2)₄ 1 x RP1 roller support (min.)* and roller without “edge” (concave) (=RP1.1)
 E) 2 x RP1 roller support (min.)* and roller without “edge” but concave **150h**) prio B

Kerosene

F) 2 x RP1 roller support (max.)* and roller without “edge” (=RP1.1) WK14

(min. / max.)*: Measurement of 100 series roller supports, table-based presentation of data,
 selection of borderline roller supports from this table



Status Task Force CP4

Test overview of anti-wear package 1 (basis: EHP_342 from 03/16/2010)

Description	TP no.	Fuel target	RT	Actual RT	Status	End date
Tappet "good" <small>(RS C3.0 & roller OK according to visual inspection characteristics)</small>	2009-CP4_0725	Arctic diesel	150	150		WK4
Tappet "bad" <small>(RS C3.0 & roller OK according to visual inspection characteristics)</small>	2009-CP4_0726	Arctic diesel	150	150		WK4
Tappet "good" <small>(RS C3.0 & roller OK according to visual inspection characteristics)</small>	2009-CP4_0727	Arctic diesel	150	150		WK6
Tappet "bad" <small>(RS 3.0 & roller OK according to visual inspection characteristics)</small>	2009-CP4_0728	Arctic diesel	150	150		WK6
Tappet with RP "best" of series <small>(with measured surface)</small>	2010-CP4_0029	Arctic diesel	150	150		WK7
Tappet with RP "best" of series <small>(with measured surface)</small>	2010-CP4_0030	Arctic diesel	150	150		WK8
Tappet with RP "worst" of series <small>(with measured surface)</small>	2010-CP4-0031	Arctic diesel	150	150		WK7
Tappet with RP "worst" of series <small>(with measured surface)</small>	2010-CP4-0032	Arctic diesel	150	150		WK8
Tappet with RP "worst" of series <small>(with measured surface)</small>	2010-CP4-0034	Kerosene	150	15 min		WK6
Tappet with RP "best" of series <small>(with measured surface)</small>	2010-CP4-0033	Kerosene	150	4		WK7
Reappear test <small>(metal spatters & fusing)</small>	2010-CP4-0065	Arctic diesel	150	13min		WK8
Reappear step test <small>(metal spatters & fusing)</small>	2010-CP4-0066	Arctic diesel	350	202		WK9
Tappet with RP "best" <small>(with measured surface)</small>	2010-CP4-0053	Arctic diesel	150	150		WK9
Tappet with RP "best" <small>(with measured surface)</small>	2009-CP4-0054	Arctic diesel	150	150		WK9
Tappet with RP "worst" <small>(with measured surface)</small>	2009-CP4-0073	Arctic diesel	150	150		WK10
Tappet with RP "worst" <small>(with measured surface)</small>	2009-CP4-0074	Arctic diesel	150	150		WK10

- Endurance run completed & diagnosed positively
- Endurance run ended with striking features
- Endurance run failed

Diesel Systems



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Status Task Force CP4

Test overview of anti-wear package 1.1 (basis: EHP_342 from 03/16/2010)

Description	TP no.	Fuel	target R	Actual	Status	End daten
Tappet witlmax. RP1.1 (roller convex, without edge)	2009-CP4-0188	Arctic diesel	EOL	150	15	WK14
Tappet witlmax. RP1.1 (roller convex, without edge)	2009-CP4-0189	Arctic diesel	EOL	150	15	WK14
Tappet witlmin. RP1.1 (roller convex, without edge)	2009-CP4-0073	Arctic diesel	EOL	150	15	WK14
Tappet witlmin. RP1.1 (roller convex, without edge)	2009-CP4-0074	Arctic diesel	EOL	150	15	WK14
Tappet witlmax. C3.0 (roller concave, with edge)	2010-CP4_0xx	Arctic diesel	EOL	150	0	WK14
Tappet witlmax. C3.0 (roller concave, with edge)	2010-CP4_0xx	Arctic diesel	EOL	150	0	WK14
Tappet witlmax. C3.0 (roller convex, without edge)	2010-CP4_0xx	Arctic diesel	EOL	150	0	WK14
Tappet witlmax. C3.0 (roller convex, without edge)	2010-CP4_0xx	Arctic diesel	EOL	150	0	WK14

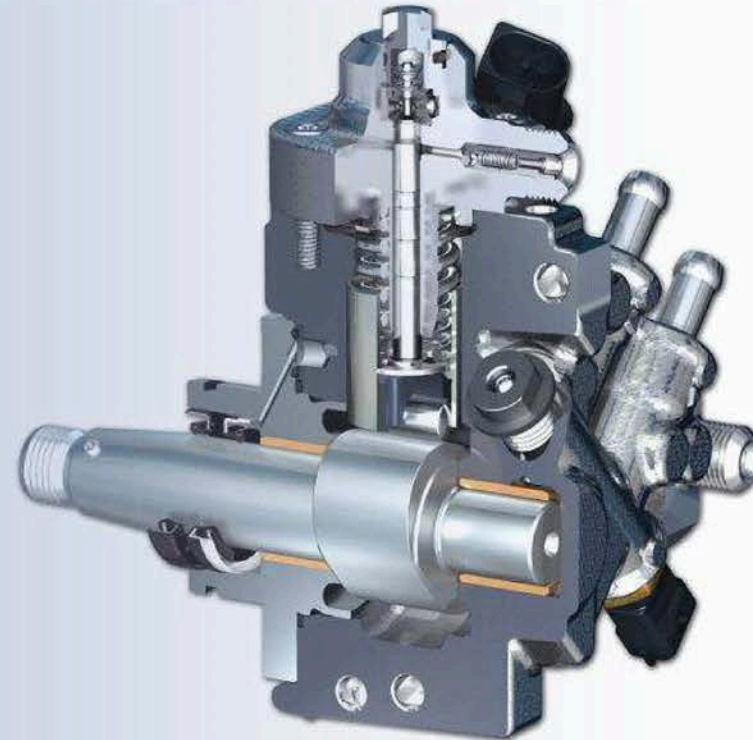
- Endurance run completed & diagnosed positively
- Endurance run ended with striking features
- Endurance run failed



Overview of CP4 robustness

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- 1) Anti-wear package 1 (RP1)
- 2) Anti-wear package 2 (RP2)
- 3) Failure statistics CP4 Non-responsive content removed



Diesel Systems

1

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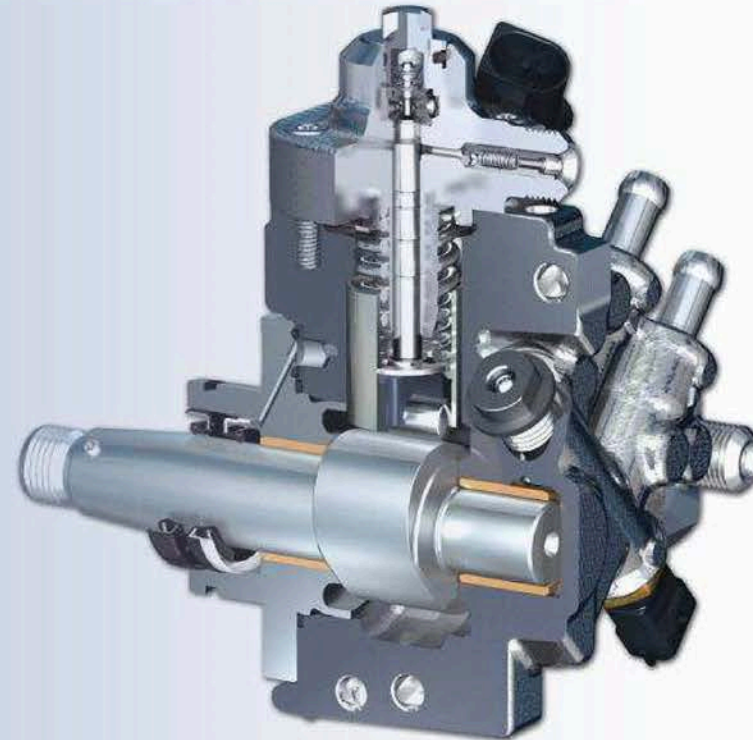
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1) Anti-wear package 1 (RP1)

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CP4 robustness

Anti-wear package 1

Assignment

Increase lubricating film between roller support and roller for fuels with lower viscosity (reduction of mixed friction fraction & temperatures)

Measures (derived from simulation results)

- Reduction in roughness in the roller support due to changeover to C2 coating
- Prevention of metal splashes (for process-related reasons there are no metal splashes with C2)
- Reduction of play between roller and roller support (smaller roller support bore)
- Reducing the roughness of the roller
- Optimization of edge taper on the roller (slender taper)

Execution

Testing RP1 vs. series in QHALT (600 rpm; 2,300bar; Arctic diesel; 90°C)

Result

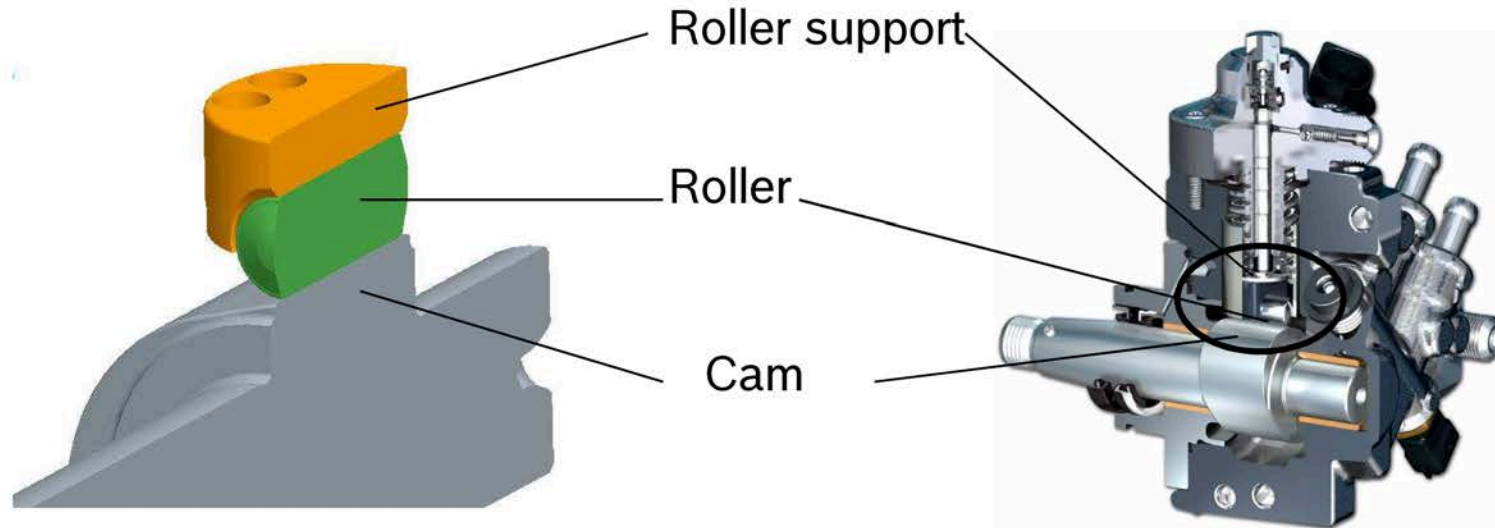
RP1 increases lubricating film by 2 x (derived from findings)

RP1 in series for all CP4.2 at Audi since WK12



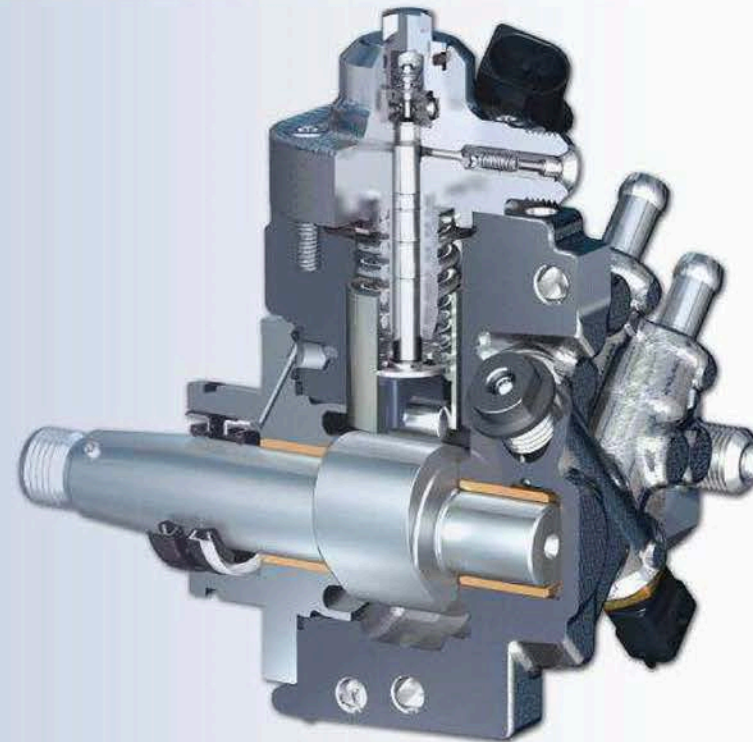
CP4 robustness

Anti-wear package 1



Anti-wear package 2 (RP2)

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CP4 robustness

Anti-wear package 2

Assignment

Reduction of local temperatures of the right (critical) roller tappet with target level CP4.1 for clockwise CP4.2 (Audi V6, not Audi V8)

Measures

- Optimized arrangement of supply & return position (result: Swapping of supply / return connections)

Execution

Temperature measurements on roller support	done
Testing RP2 in QHALT (600 rpm; 2,300bar; Arctic diesel; 90°C)	WK24

Result

Function measurements show by the optimized supply/return adjustment that temperatures as in CP4.1 can be achieved (temperature reduction of > 15°C in lubrication gap).

Further work

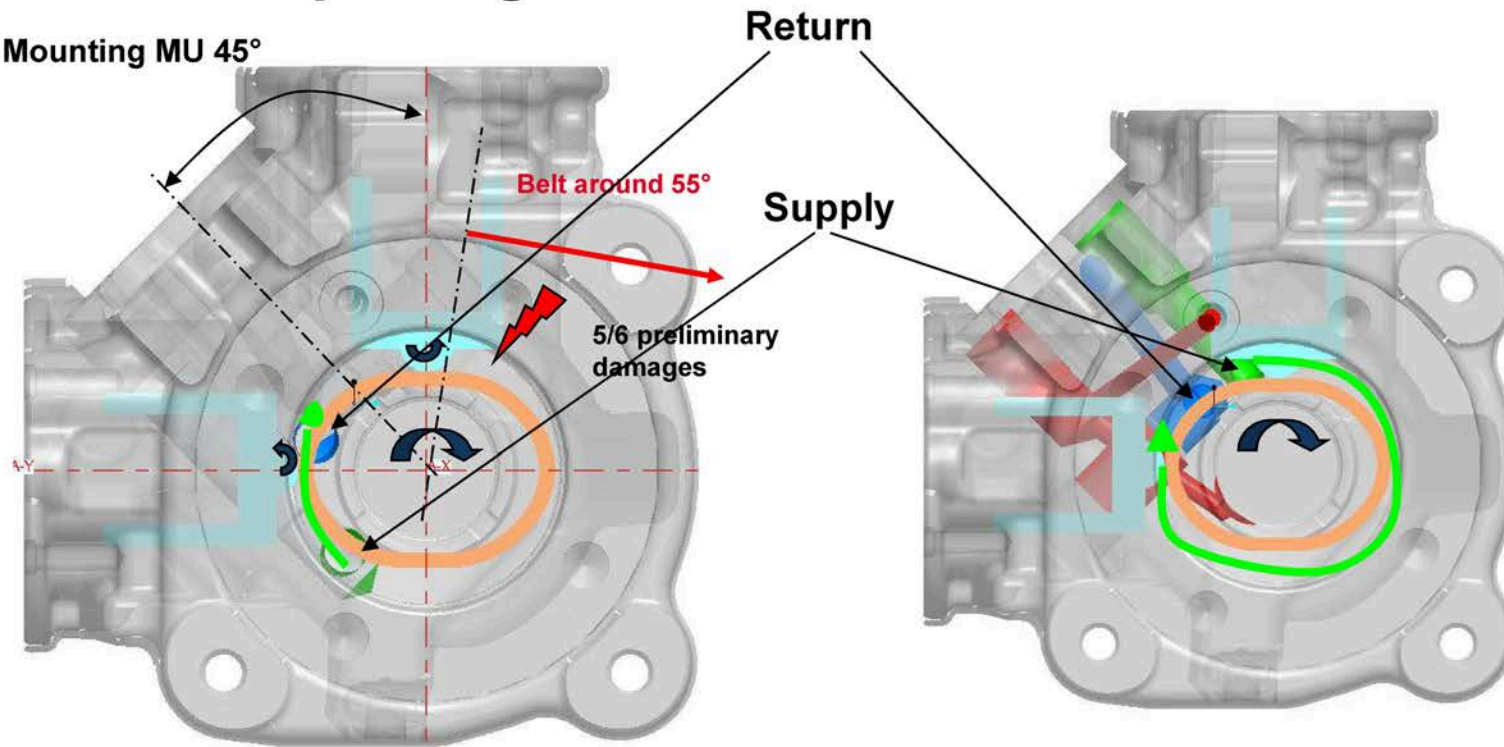
Confirm effectiveness in QHALT endurance run	WK24
Pumps for testing delivered to Audi. Introduction in series possible from WK 28.	



CP4 robustness

Anti-wear package 2

Mounting MU 45°



Fuel goes directly to outlet

CP4.2-EFP cw Audi W19

Fuel is recycled once

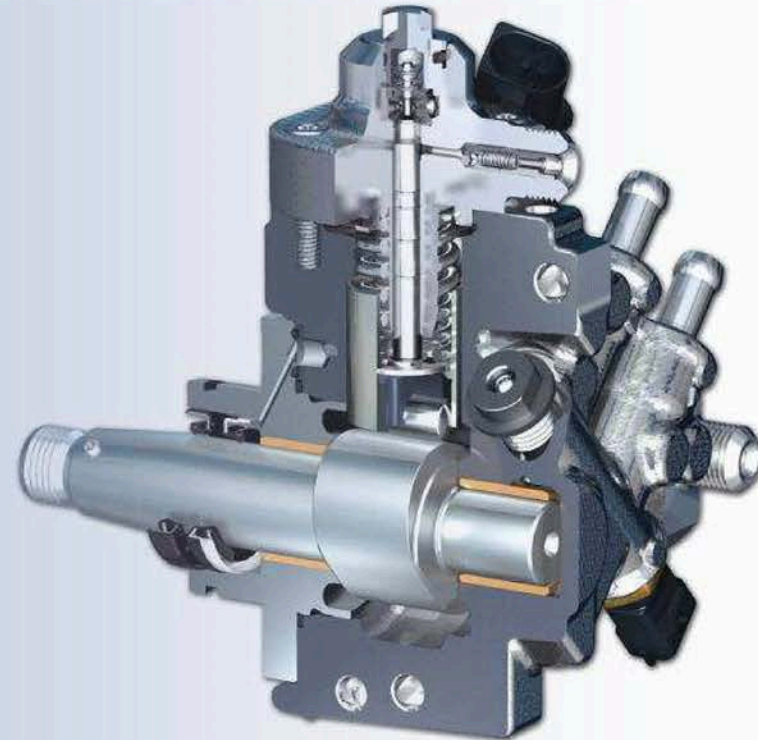
CP4.2 EFP cw **AWP2** for Audi W19

Diesel Systems



3) Failure statistics

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Diesel Systems

8

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CP4 robustness

Failure statistics Non-responsive content removed

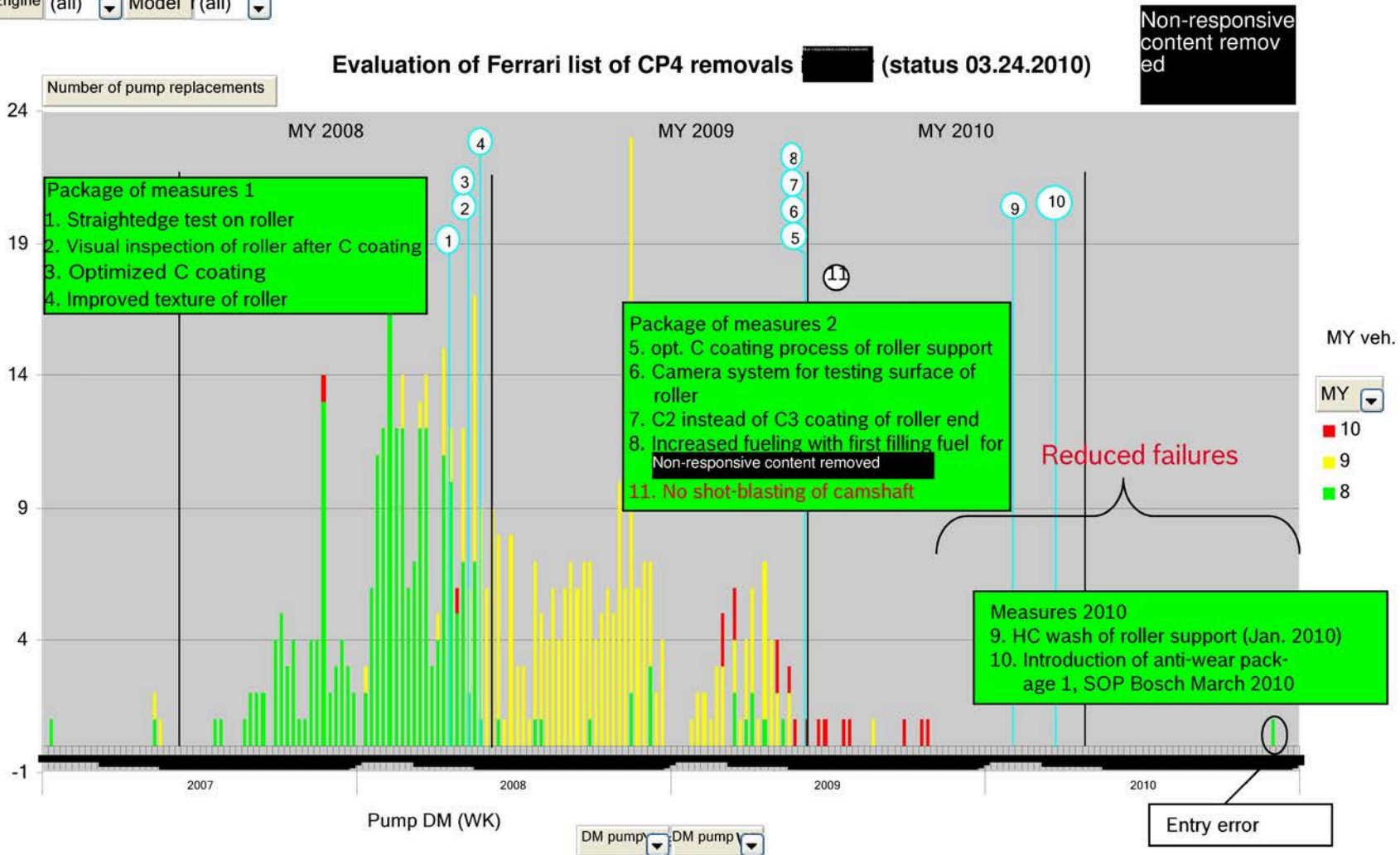
Italy (see page 10, 11, 12)

- Decline in complaints CP4.2 with pumps DM after Jun 2009 (page 10)
- Absolute increase in complaints CP4.2 & CP4.1 in Non-responsive content removed from 03/2010 (page 11, 12)
 - Presentation of relative values (CP4.2 / CP4.1 / total / vehicle model) agreed up on with Audi
 - Joint analysis “Influence of vehicle model as part of task force
 - CP4.1 complaints likely not 100% drivetrain damage, but rather
 - Non-starters due to shavings in intake valve
 - Pump exchange due to noise complaint



CP4 robustness

Engine (all) Model (all)



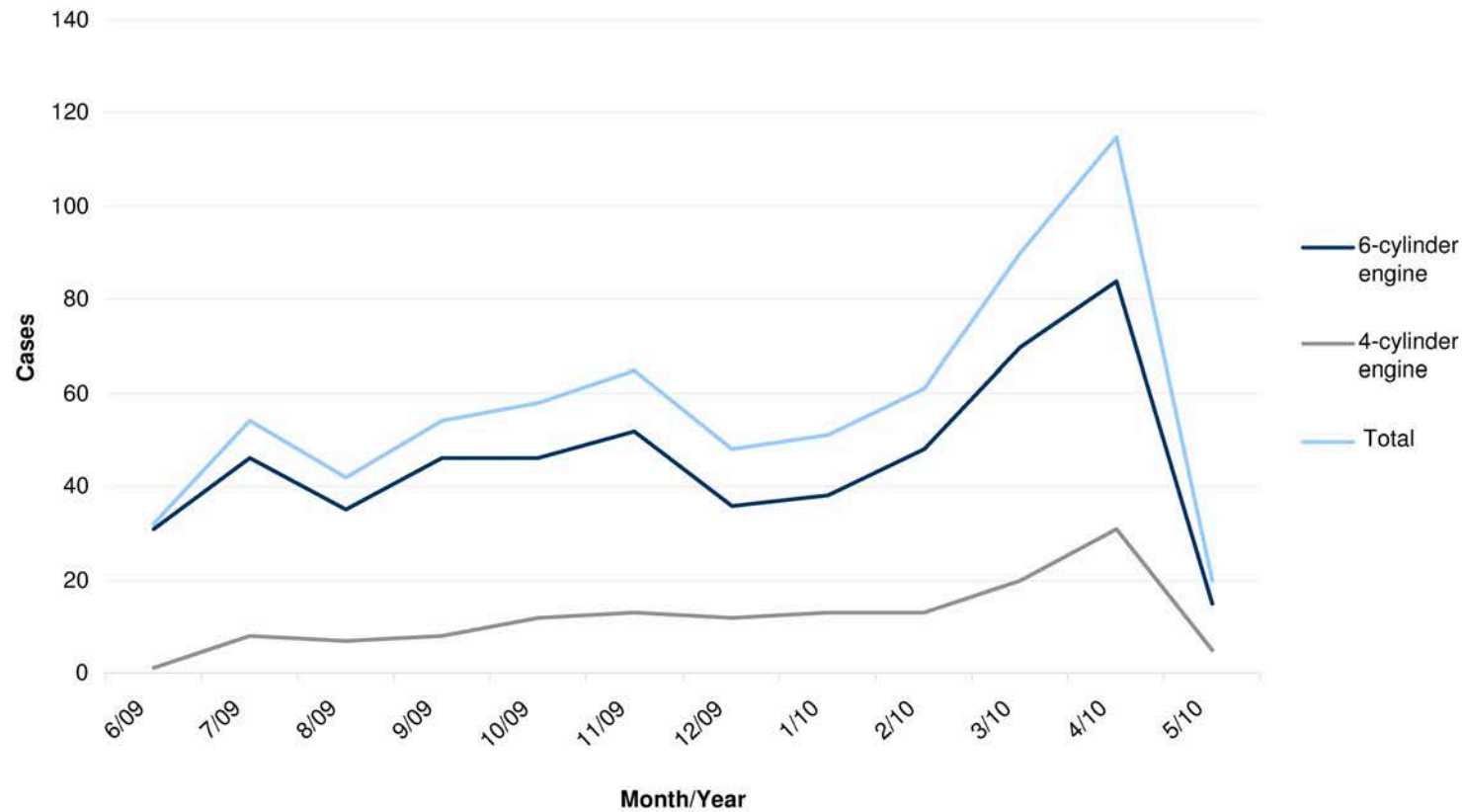
Diesel Systems



CP4 robustness

Failure statistics Non-responsive content removed (total of all vehicles)

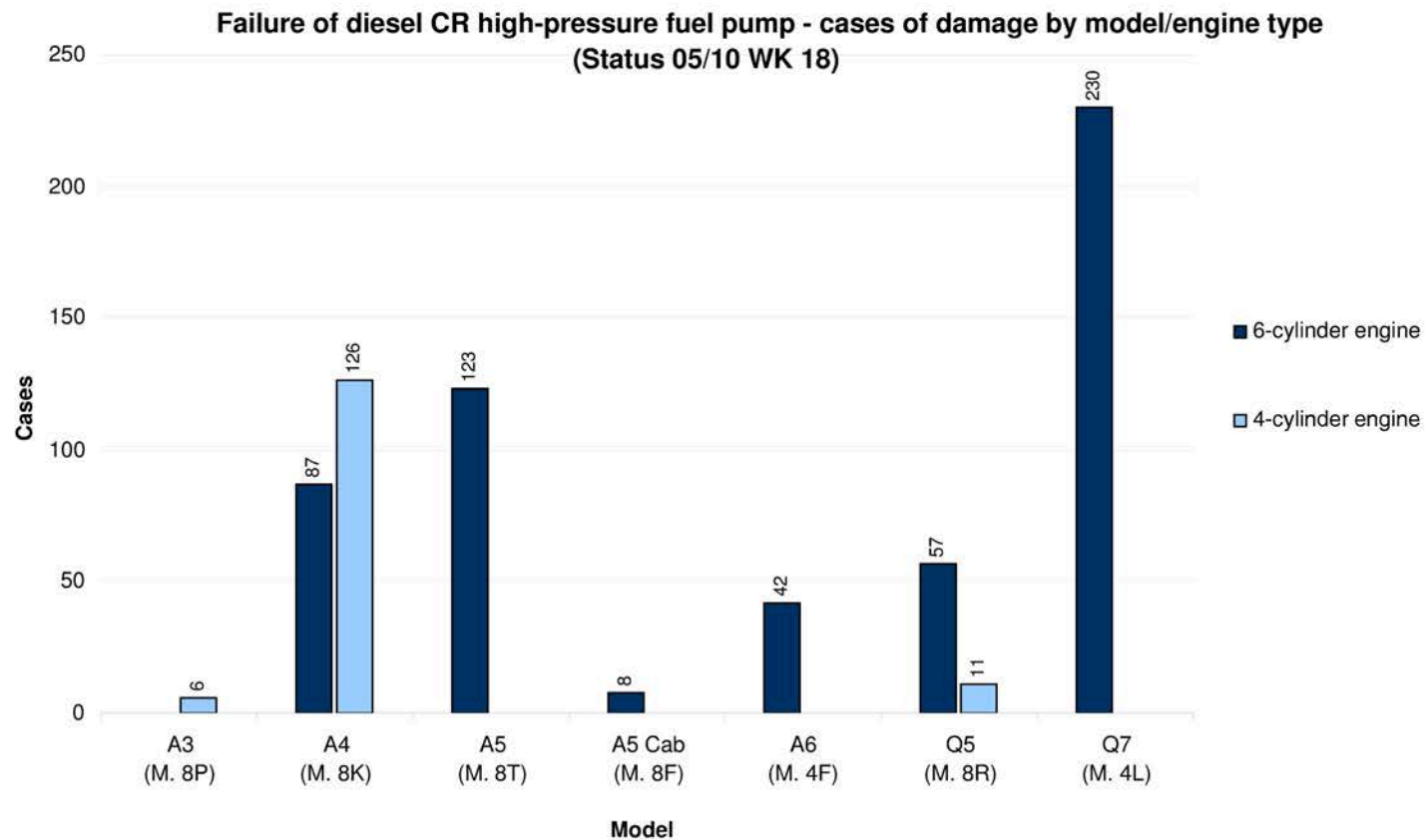
Failure of diesel CR high-pressure fuel pump - cases of damage by month (status: 05/11 WK 18)



CP4 robustness

Failure statistics (vehicles)

Non-responsive content removed



Diesel Systems



Previous results and further action

- Of the 4 vehicles inspected in [Non-responsive content removed] and 2 in [Non-responsive content removed] (Arctic Diesel), there were no violations of the specified return volume (80 l/h) under the examined measurement conditions.
- Additional vehicles will be measured to identify the further impact of fuel conditions on the injection system, including low-pressure circuit, in [Non-responsive content removed]
- We have agreed to examine the application of the BEM.
- Measurements of B8 vehicles and 4-cylinder (CP4.1) are planned, among others, for WK31. If possible, an A3 with transverse-mounted engine is also to be measured.

Further action #2

- A TEE with tank EFP was removed from one of the vehicles, to check whether the necessary output has changed compared to the new status.
- For further measurements, a transparent hose will be used to check whether air bubbles can be observed in the return of the CP4.
- Audi will provide Bosch with an affected vehicle for more comprehensive measurements, to assess the influencing factors (viscosity, temperature, battery voltage, tank level).

Evaluation of CP4 removals

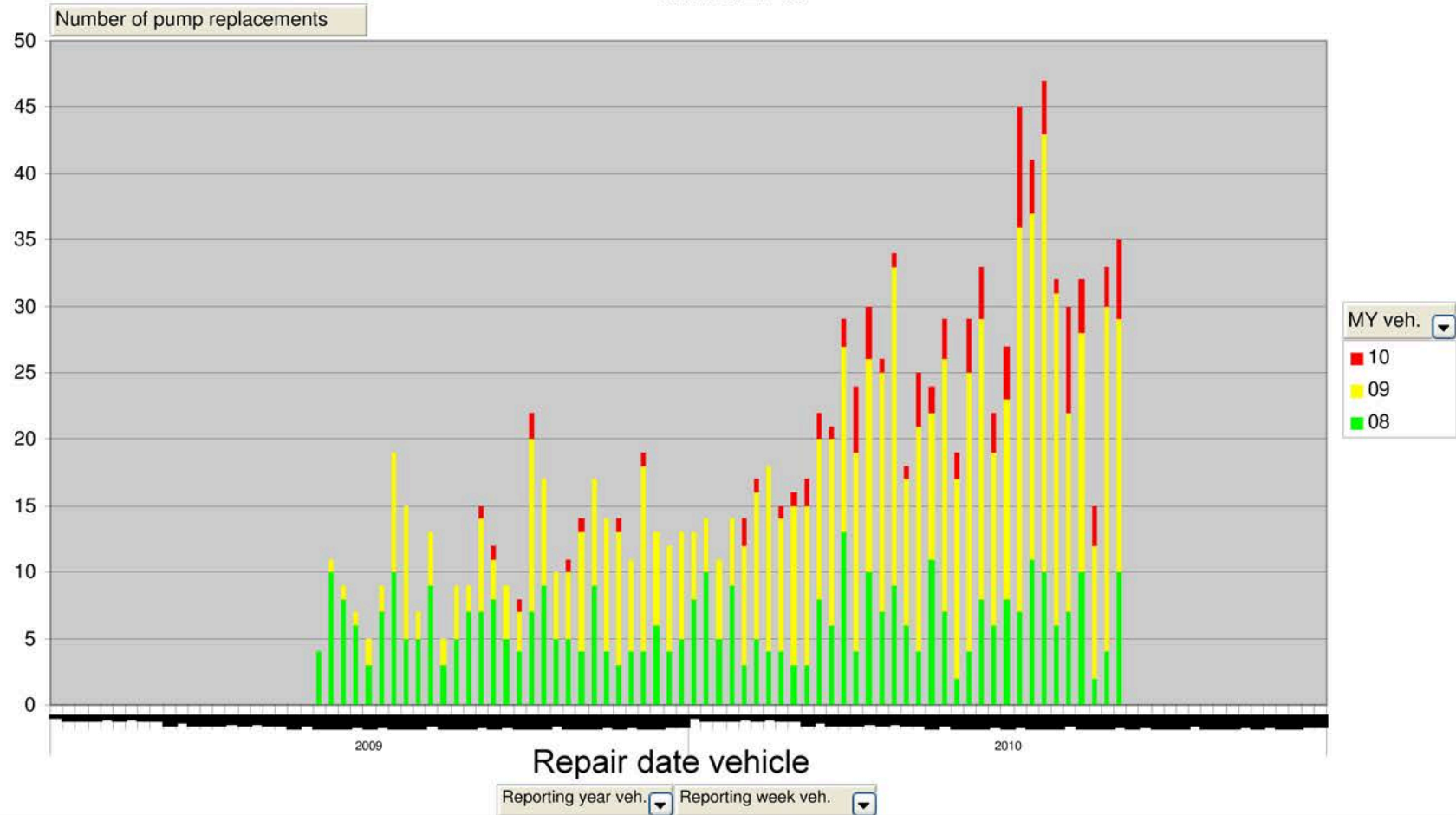
Non-responsive content removed

Status: WK35/2010

R4 and V6 engine

Engine (all) with/without chips (all)

WK35/2010

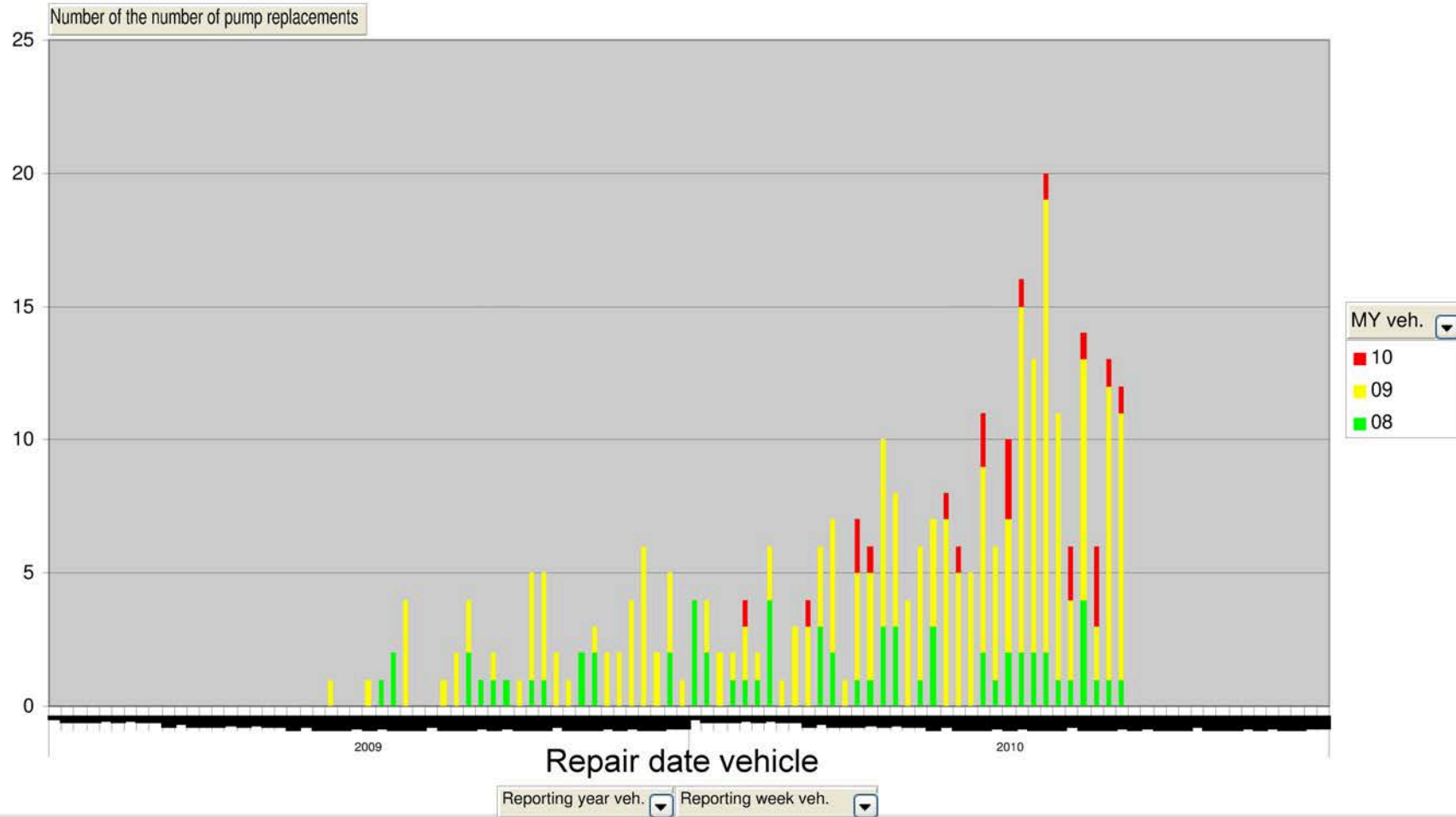


Evaluation of CP4 removals Non-responsive content removed

Status: WK35/2010 R4 engine

Engine R4 with/without chips (all)

WK35/2010

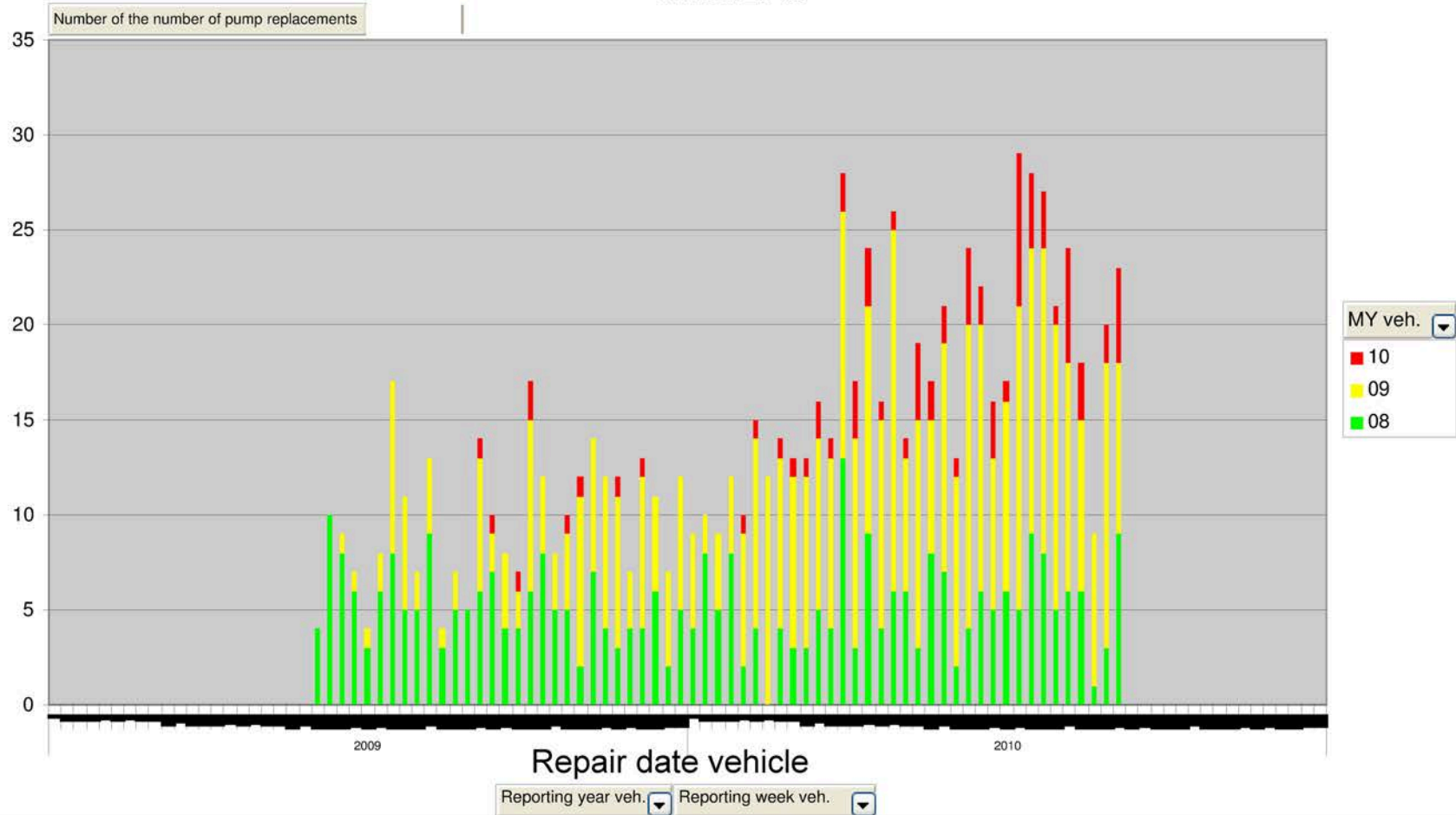


Evaluation of CP4 removals Non-responsive content removed

Status: WK35/2010 V6 engine

Engine V6 with/without chips (all)

WK35/2010

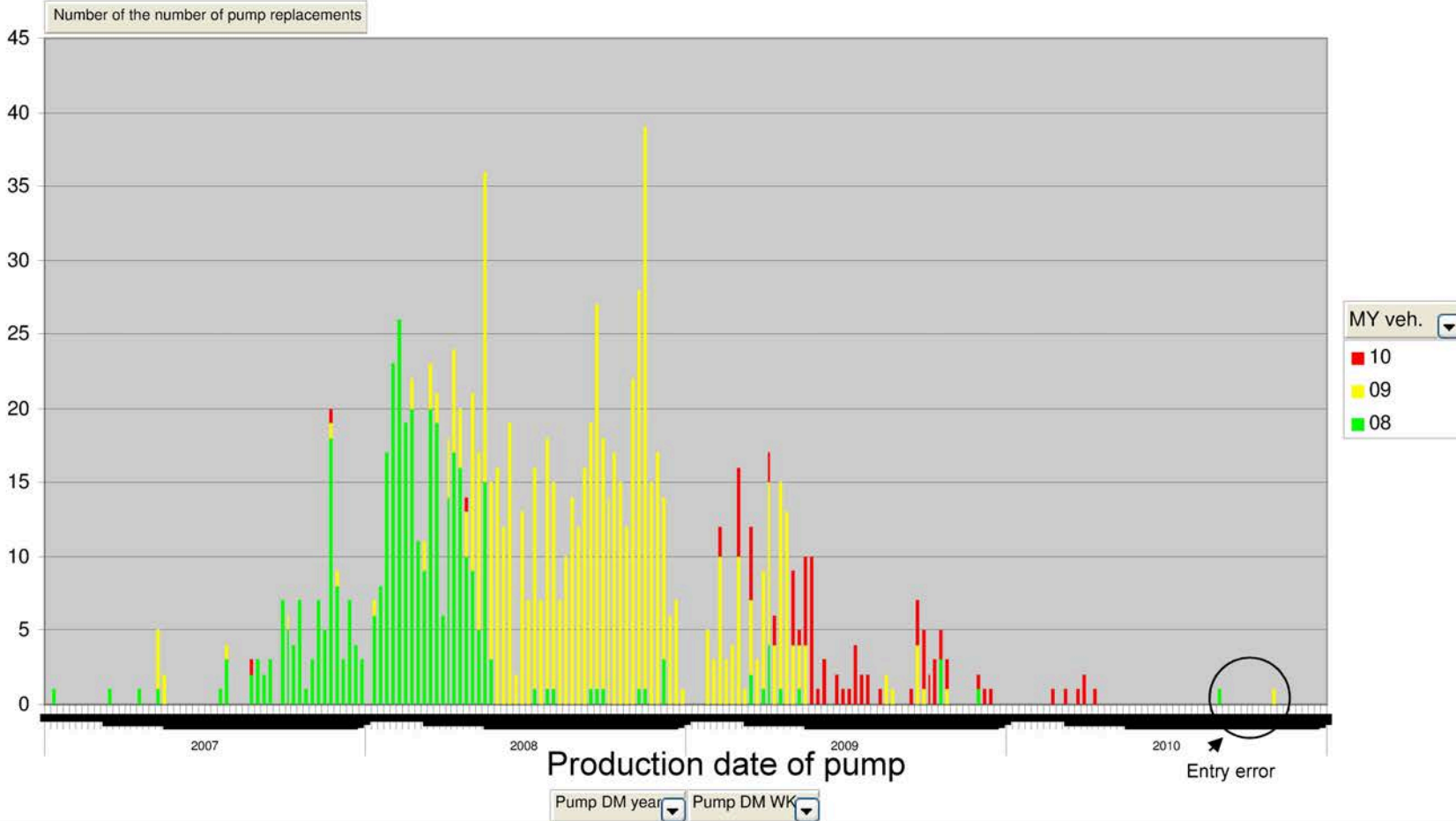


Evaluation of CP4 removals Non-responsive content removed

Status: WK35/2010 R4 and V6 engine

Engine (all) ▼

Status: WK35/2010

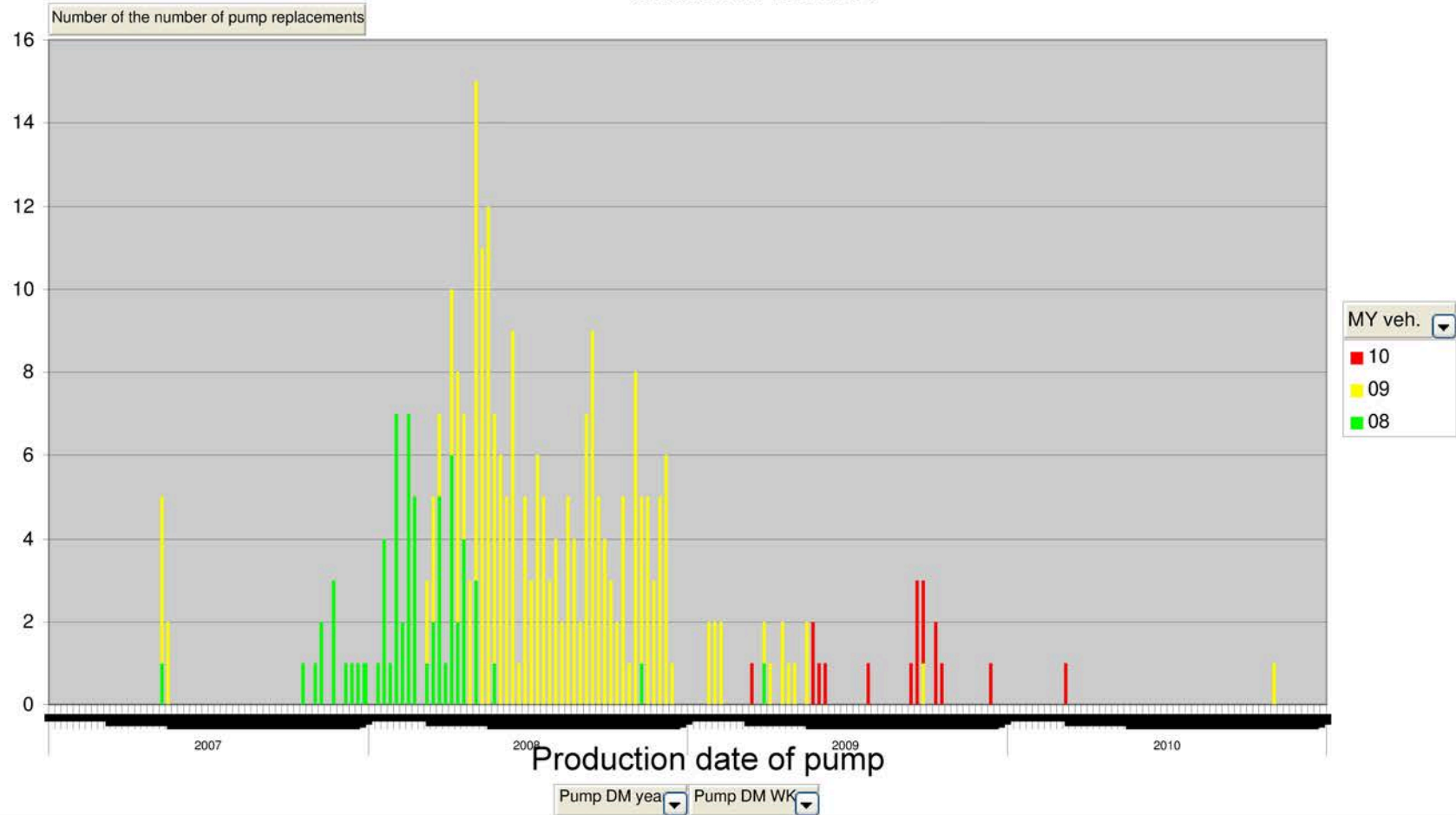


Evaluation of CP4 removals Non-responsive content removed

Status: WK35/2010 R4 engine

Engine R4

Status: WK35/2010



Evaluation of CP4 removals

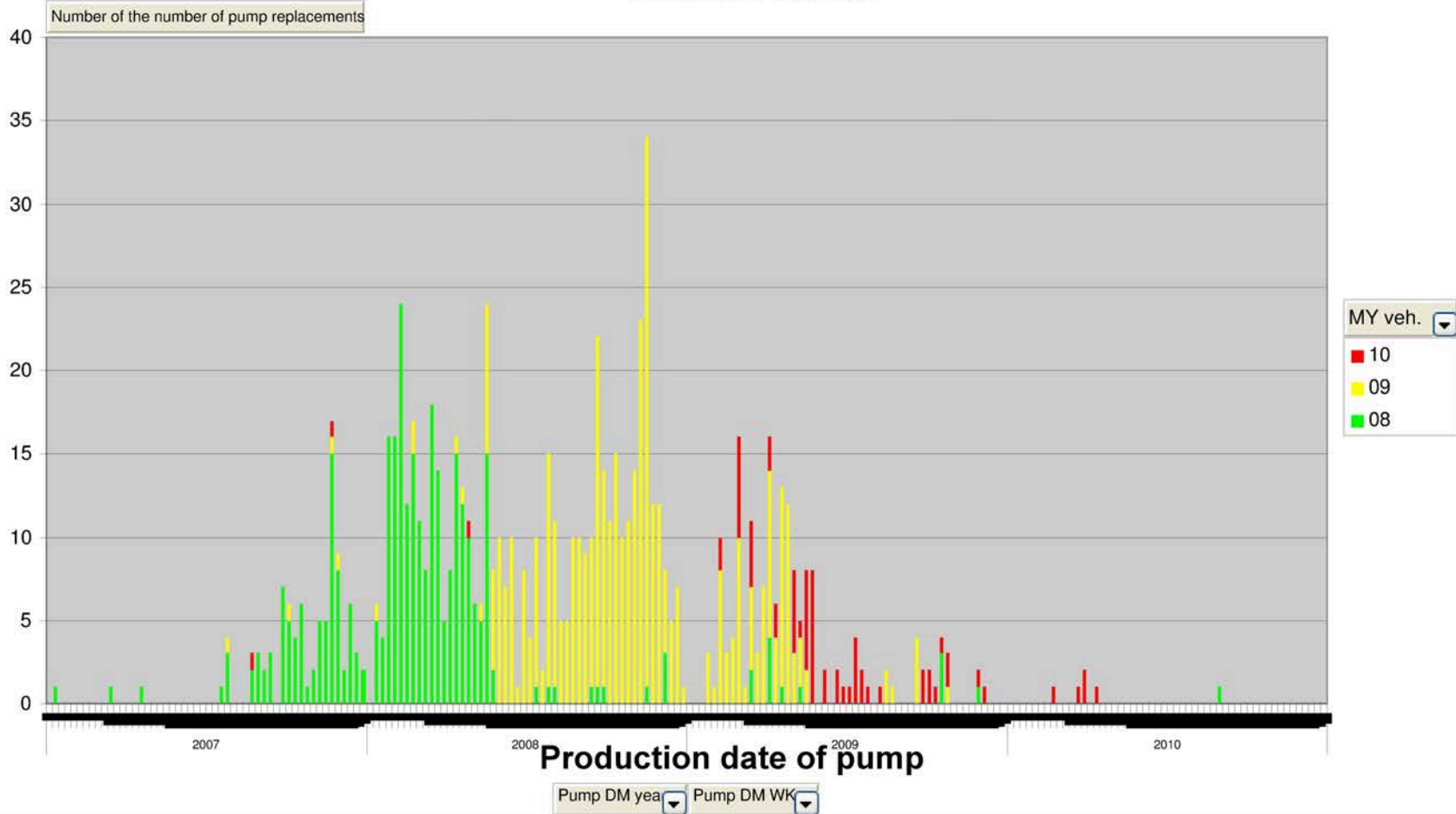
Non-responsive content removed

Status: WK35/2010

V6 engine

Engine V6

Status: WK35/2010



Evaluation of CP4 removals

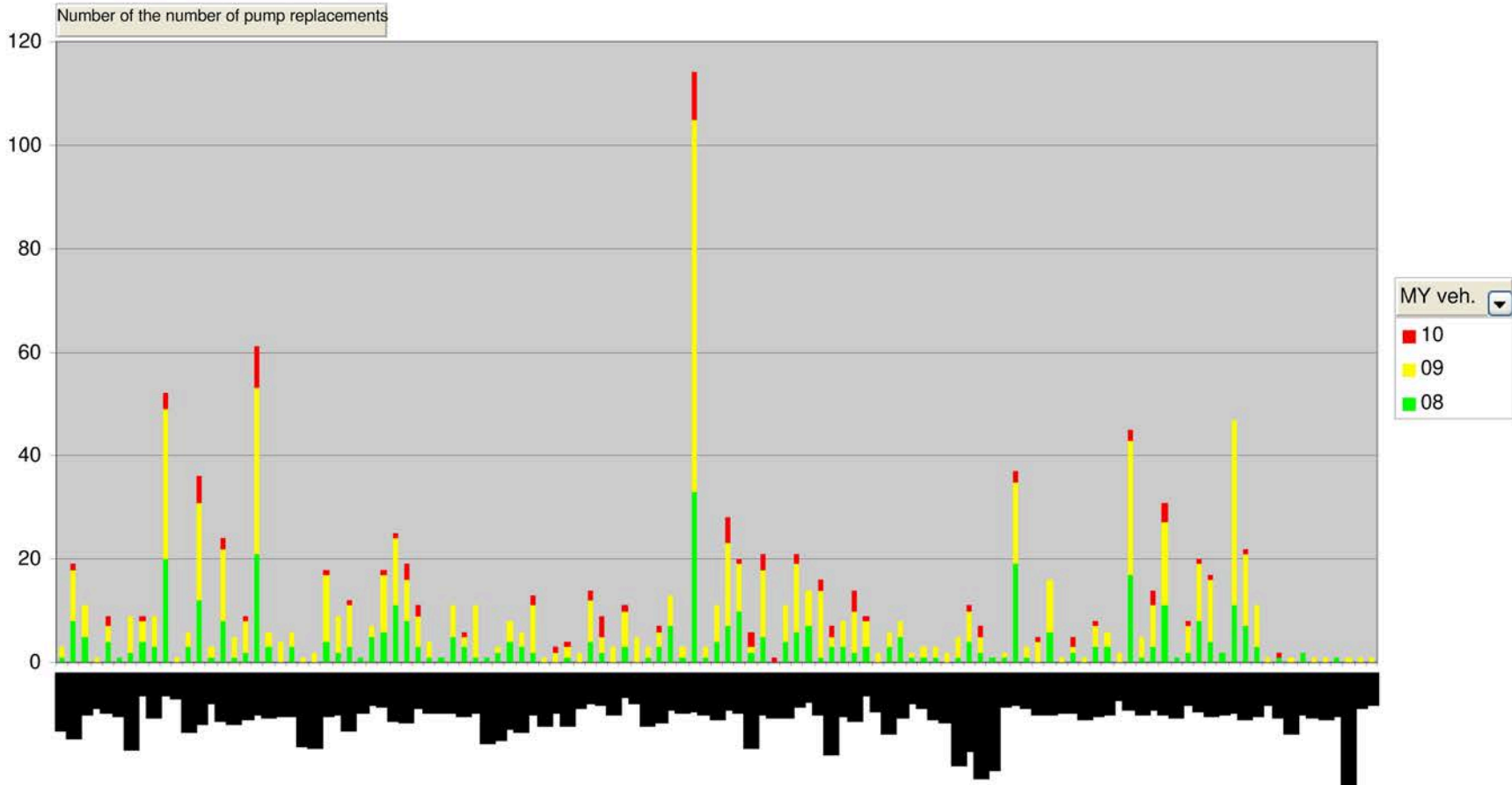
Non-responsive content removed

Status: WK35/2010

R4 and V6 engine

Engine (all) with/without chips (all)

Status: WK35/2010



Province



Evaluation of CP4 removals

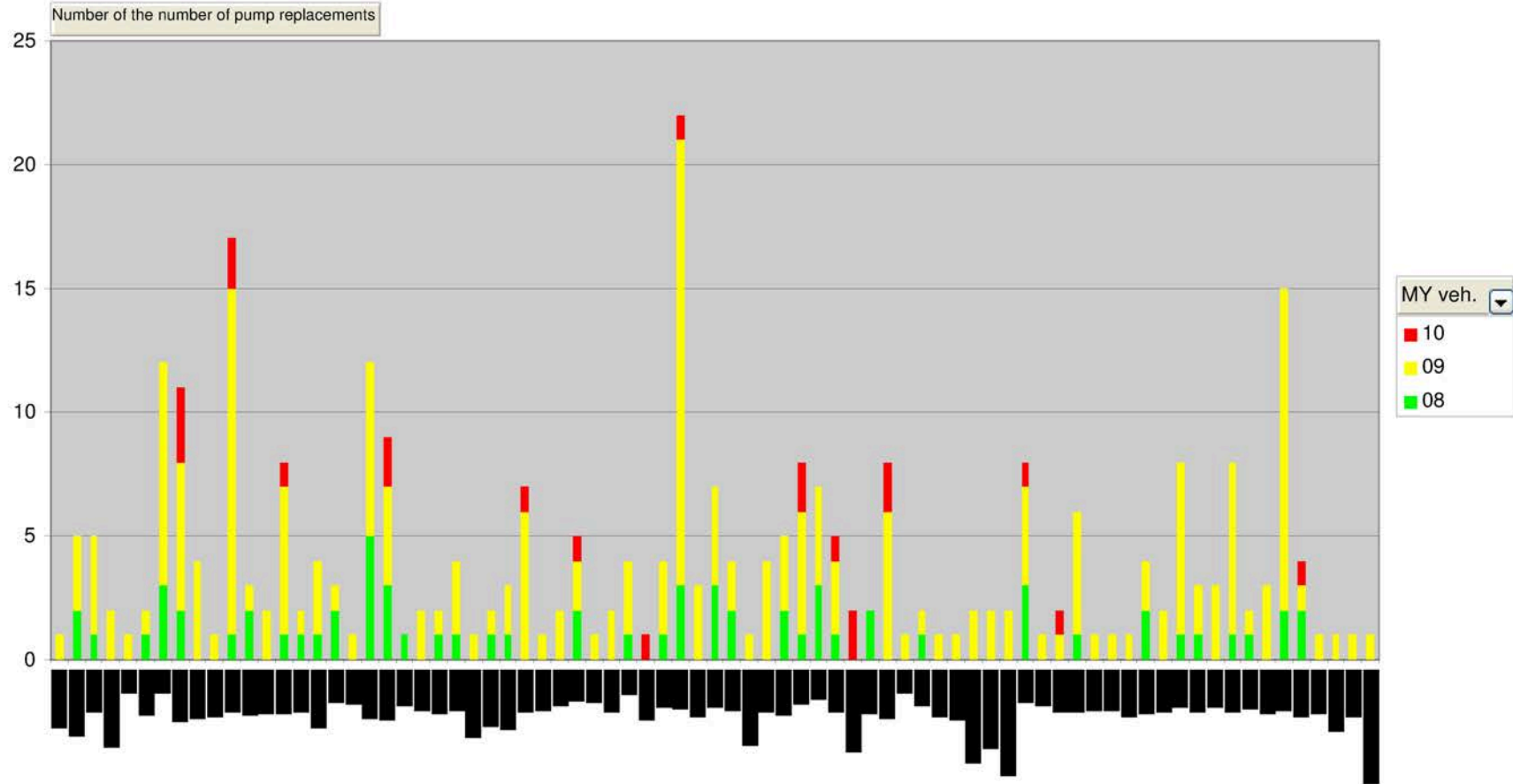
Non-responsive content removed

Status: WK35/2010

R4 engine

Engine R4 with/without chips (all)

Status: WK35/2010



Province



Evaluation of CP4 removals

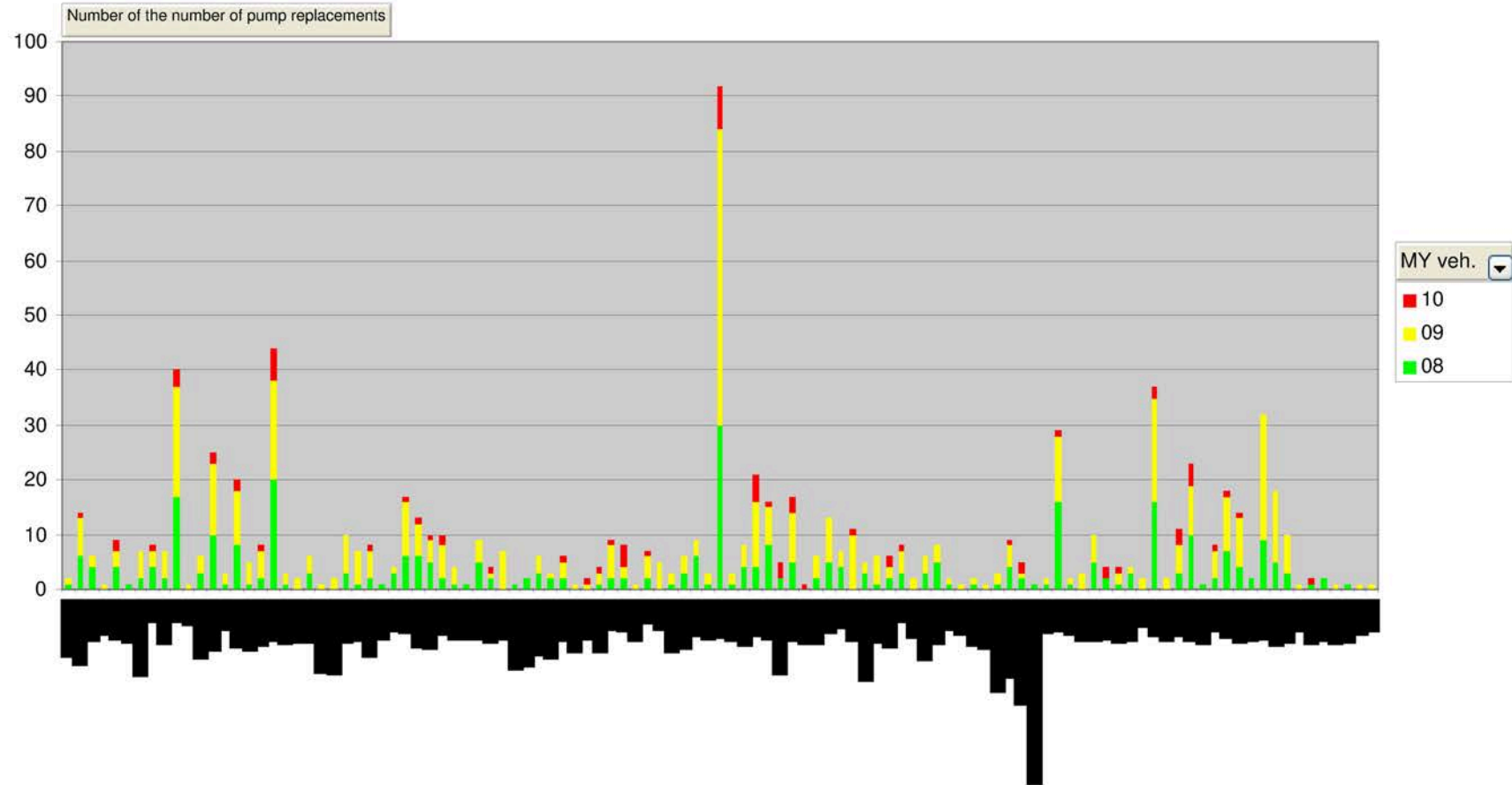
Non-responsive content removed

Status: WK35/2010

V6 engine

Engine V6 with/without chips (all)

Status: WK35/2010



Province



From: Non-responsive content removed
To:
CC:

Date: 03.18.2008 1:59:01 PM

Subject: Preliminary analysis result: Failed pump on-field VW US07

Attachments: [Alle Triebwerk gesamt Stand 080317.pdf](#)

Dear Non-responsive content removed

The drivetrain damage is confirmed by us.

The camshaft shows a deep groove in the middle.

It can be seen on the camshaft pendulum motions as well as the final 90° turn of the roller tappet. The roller shows several braking flats.

In the area of tappet hole of the housing, deposits to be analyzed later were found. The metering unit including O-ring is subjected to a detailed analysis in Waiblingen.

The roller support assembly is also subjected to a detailed analysis. The analysis results will be submitted to you - ASAP.

Please notify us the result of your fuel analysis.

The attached slide shows the status of the "drivetrain damage" issue based on the date of manufacture of the pumps.

<<Alle_Triebwerk_gesamt_Stand_080317.pdf>>

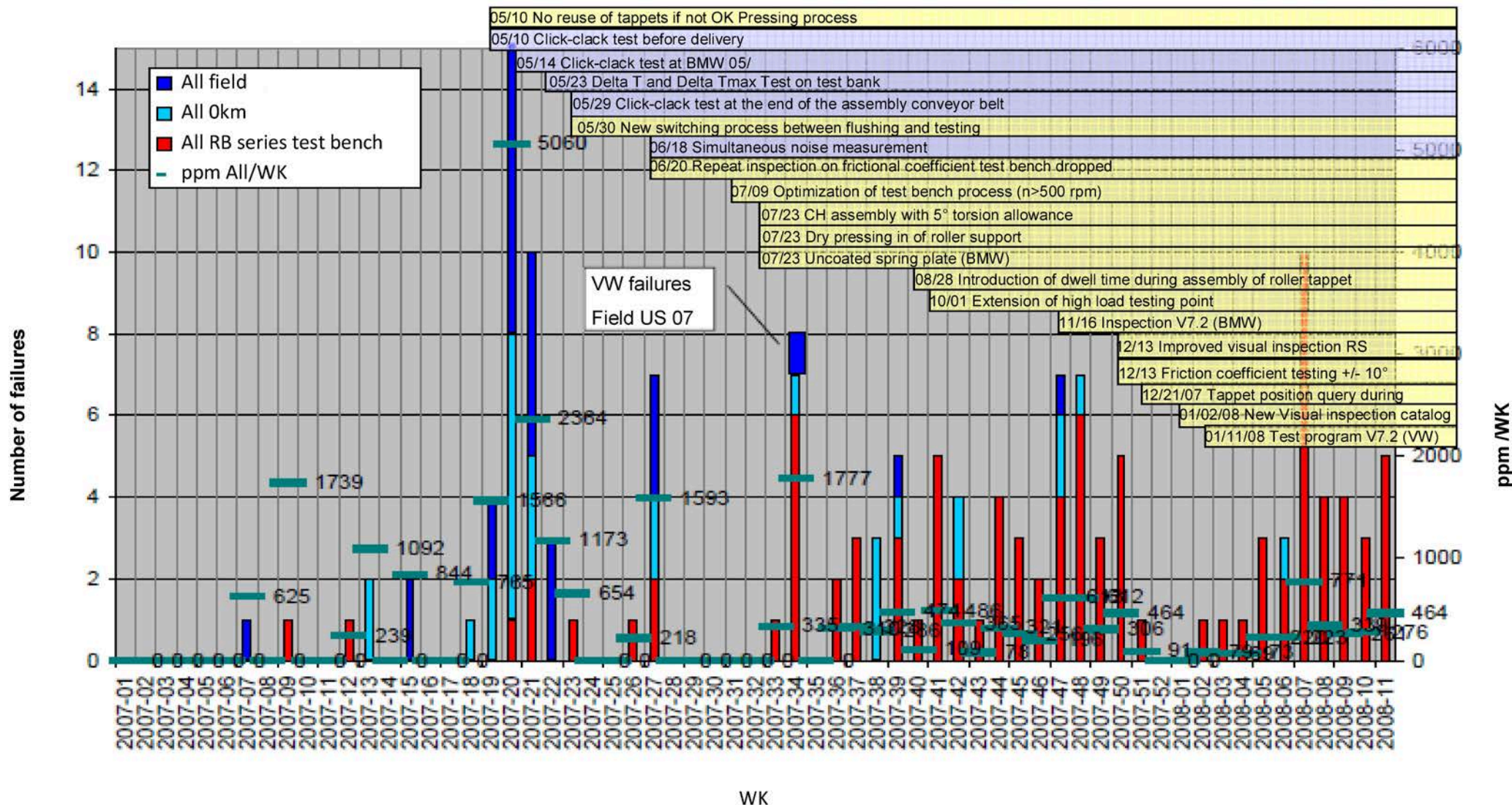
Mit freundlichen Grüßen / Best regards

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Robert Bosch GmbH

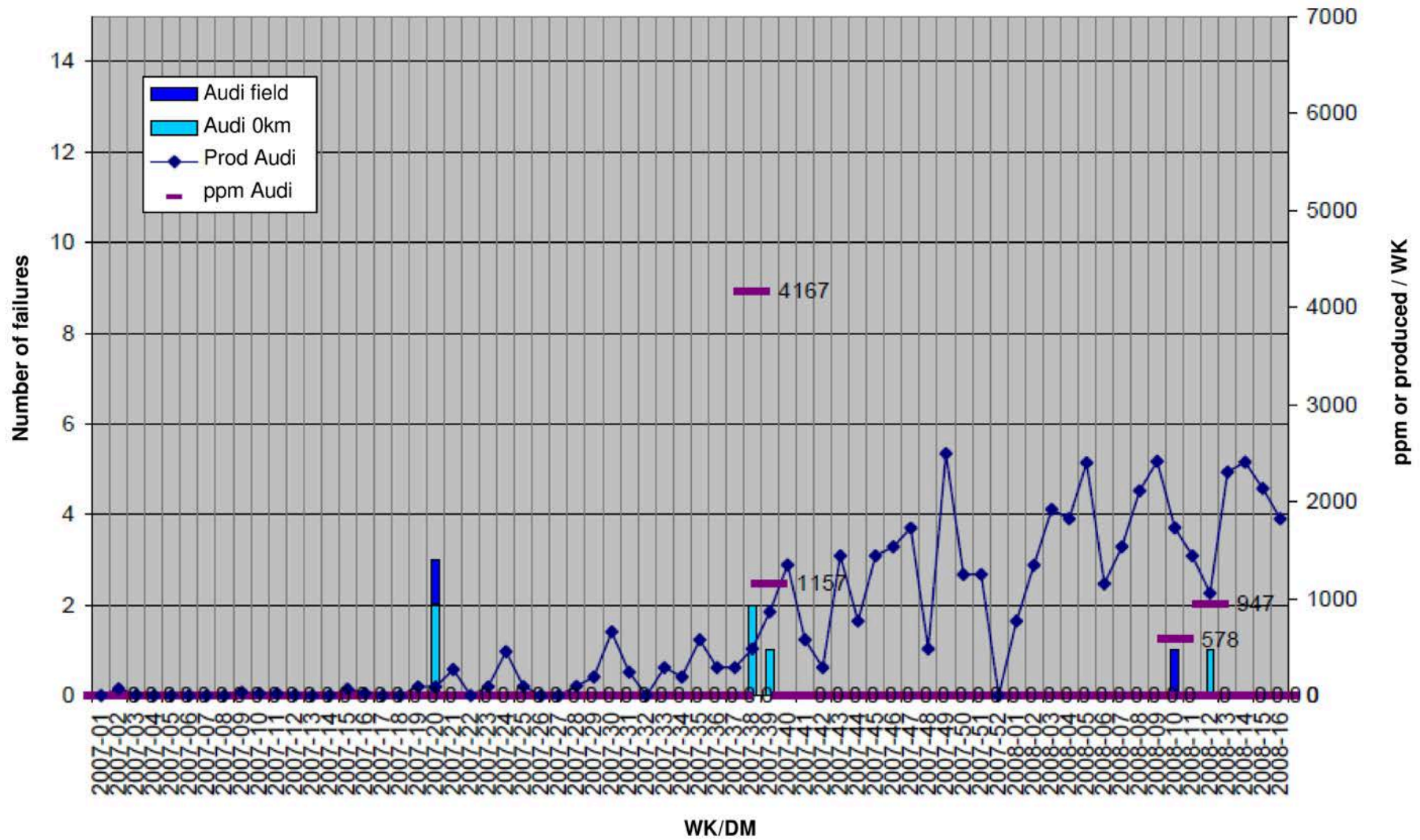
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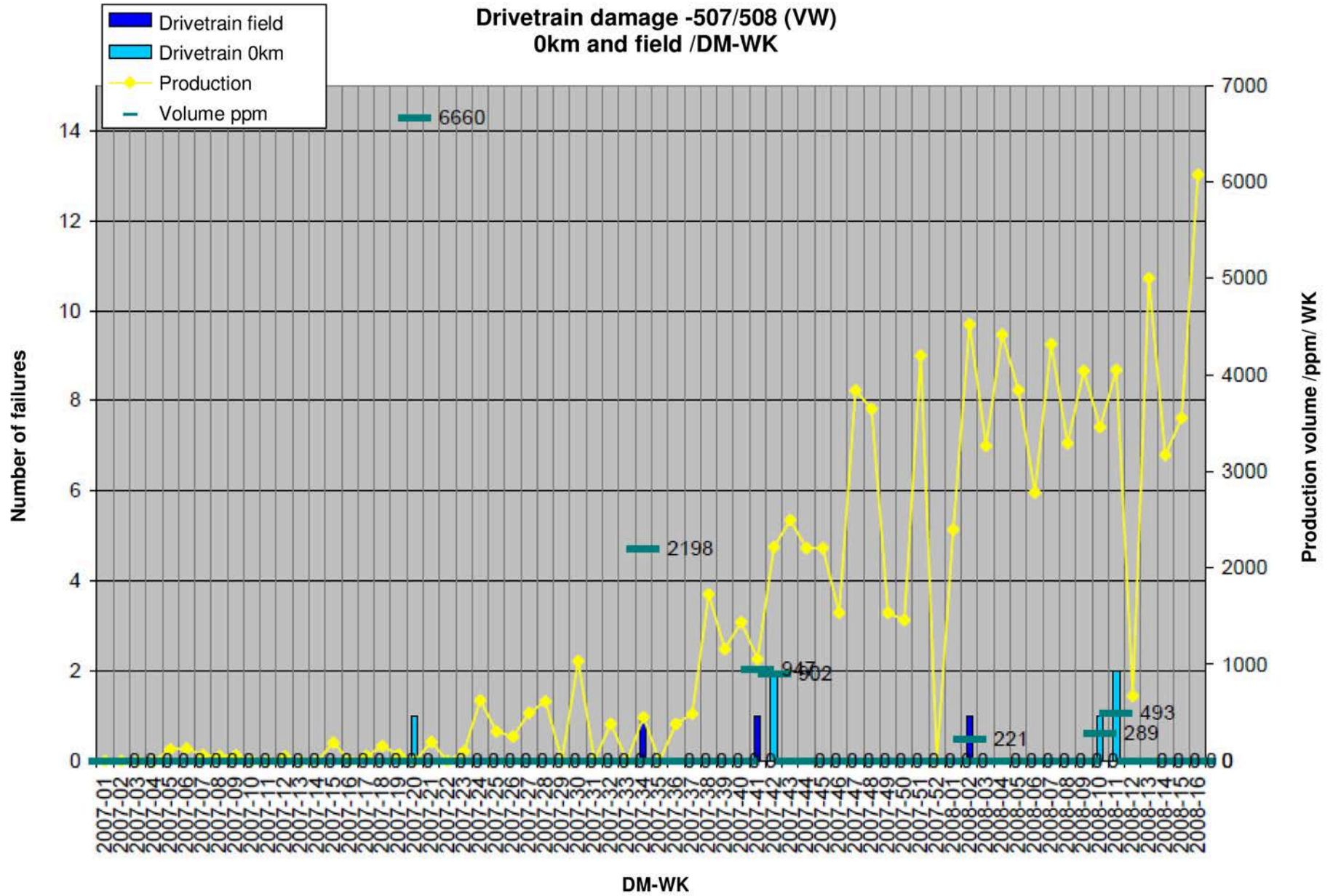
Failures due to drivetrain damages FD-WK



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Failures drivetrain damage -611/-613 (Audi) / DM-KW





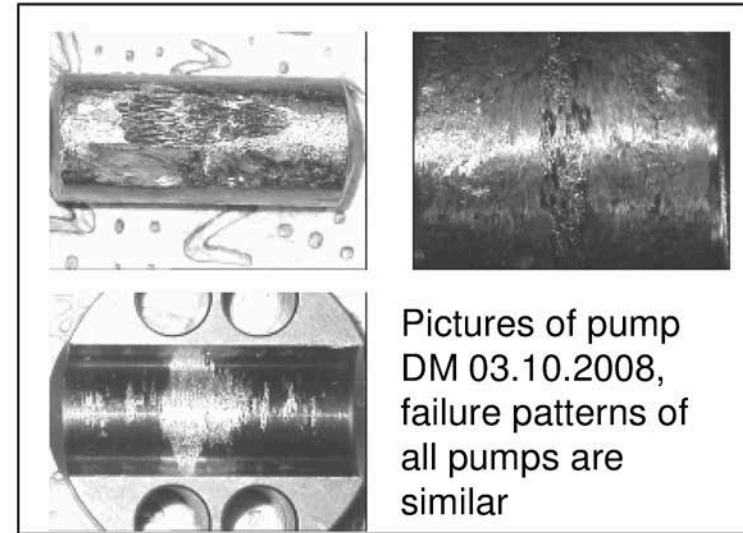
0km complaints

Scope of defect (current failures March / April)

0km 3x pump 0445010507 / 03L130755 (a)

1x pump 0445010611 / 059130755AB (b)

- Pumps DM a) 1x 03.05.2008 | b) 1x 03.19.2008
 1x 03.10.2008
 1x 03.11.2008
- Failure date: a) 03.14., 03.17., 03.18.2008
 b) 04.06.08
- GR Bosch: 03.25.08 (a), 04.14.08 (b)



Description of problem

- Failure on Audi final function test rig
(Cold test) with noise and rail pressure fluctuations or no fuel pressure

On-field complaints

Error scope (current failures April)

- Field: 1x pump 0445010507 / 03L130755
1x pump 0445010611 / 059130755AB
- DM and mileage
 - 1x 01.11.2008; 25 km ([redacted] A4 2,0l)
 - 1 x 03.03.2008; 6 km ([redacted], VOT-operating mode, A4 2,7l)
- Failure date: 03.26.2008, 04.08.08
- GR Bosch: 04.14.2008, 04.17.2008

Description of problem

- Engine does not start up
- Engine stopped while driving

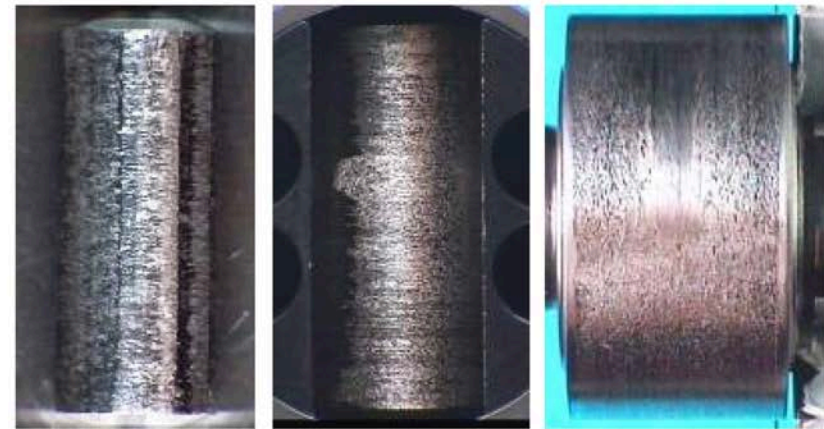
Cause analysis

- Excessive wear of the cam and the roller
- Possible damage profile: Increased friction between the roller and roller support leads to slip between the roller and cam. This causes damage to the cam, roller and roller support and turned tappet.



Error scope (previous failures)

- 0km: 5x Pump 0445010611/ 059130755AB
- DM 2x 05.14.2007
2x 09.20.2007
1x 09.28.2007
- WE 07.06.07/ 10.26.07/ 11.07.07/ 11.14.07



Description of problem

- Vehicle stop switch
- Injectors contaminated with particles

Cause analysis

- Excessive wear on the entire lateral surface of all rollers and camshafts
- Diameter of the rollers is greatly reduced, so that they cannot be held by the roller support any longer



Overall measures since SOP:

- Analysis of assembly and handling processes performed in Dresden on 07.12.2007. Result: Commissioning conditions not according to specification. Commissioning of the vehicles were changed immediately
- Optimization of Bosch test bench sequence by raising the starting speed from 200 rpm to 500 rpm.
D: 07.09.07 completed
- Cylinder head assembly with 5° torsion allowance
D: 07.23.07 completed
- Dry pressing in of roller support
D: 07.23.07 completed
- Introduction of dwell time in assembly of tappet assembly
D: 08.28.2007 completed
- Extension of high-load testing point
D: 10.12.2007 completed



Measures

- Improved visual check of roller support for new visual check catalog
D: 12.13.2007 completed
- Friction coefficient test +/- 10° for better testing of the main load area of the roller support
D: 12.13.2008 completed
- Introduction of tappet position query using laser for secure alignment of the tappet during assembly
12.21.2008 completed
- Introduction of a new test program for CP4.1 VW with tighter testing conditions, namely
 - Starting with a steeper speed ramp to cause drivetrain damage internally and not at the customer
 - Critical load points (1,800 bar) are placed from the end of the test sequence to the start of the test sequence, so that drivetrain damage can be detected better.
 - Elimination of the flushing nozzle, thus detection of not OK rail pressures even during flushing of the pump and omission of the critical switching procedure from flushing to measurement.
 - Flushing operation has been made more intense from a state of 300 bar and 2,500 rpm to 1,800 bar and 3,375 rpmD: 01.11.2008 completed



Measures

- Introduction of visual check of roller support with techno scope instead of magnifier for better detection of metal spatter
D: 02.04.2008 completed
- Introduction of a new test program for Audi CP4.2 with stricter testing conditions similar to VW CP4.1, D: 02.05.2008 completed
- 100% straightedge testing of roller to detect elevations of the roller; since the introduction of the test, parts are found. Parts are used for large-scale test.
D: since 04.01.2008 in parts production, from 04.07.2008 in pump
- Measures currently in testing C coating:
Roller support (RS):
 1. Reduction in the valances impact, trial with 480 RS batch; first result positive;
Result: FIB cut did not show any metal spatter, then step 2.

Measures

Measures currently in testing C coating:

Roller support (RS)

- 2. Reduction in the valances impact, trial with 2880 RS batch;
If the result is positive, Audi agrees to the switchover of the C coating process;
Result: The result of the whole batch with 2880 pieces showed only a metal spatter, so clear improvement over the trial batch, hence the C coating series process for the RS is changed;
Launch date of roller support tentatively on: 04.23.2008;
Launch date product CP4.1 / CP4.2: after 04.30.2008

Measures currently in testing C-coating:

Roller:

- Optimized holder model for roller to prevent fusing
- D: Time schedule 04.23.2008

Audi - CP4 drive train damage

US Test with CP4.2 for V6 BIN5

- 3 failures in quality assurance (2 x Q7, 1x Touareg)
- **Analysis:** Probably stiff roller; cause is no longer detectable
- Preventive replacement measure (in Germany): 1 of 6 pumps show abnormality at roller
Action: Tests for damage reproduction WK32; RB



Audi - CP4 drive train damage

Testing, quality assurance, on-field CP4.1 & CP4.2 (██████ list, pages 5 and 6)

55 Audi & VW worldwide failures (50 field, 4 quality assurance, 1 testing, delivery quantity Audi 125,520)

- 22 complaints in ████████ (VW & Audi)
 - 15 CP4.2 (12xAudi, 3xVW) Delivery quantity Audi 2,154 / VW unknown
 - 1 CP4.1 Audi Delivery quantity Audi 430 / VW unknown
 - 6 CP4.x Audi Delivery quantity 1724
- 3 ████████ pumps submitted: 3 x drivetrain damage, detailed analysis WK32; RB
- 9 complaints in ████████ (VW & Audi) Delivery quantity 478 (only Audi)
 - 9 CP4.2 (5 x Audi, 4 x VW) Delivery quantity 478 / VW unknown
 - 0 CP4.1
- 2 ████████ pumps submitted: 1 x suspected cam fatigue (overload); detailed analysis WK32, RB

Action: Organize VW delivery quantities WK32; RB



Audi - CP4 drive train damage

Hypotheses & Activities

1) Water in fuel

Analysis: No corrosion observed on pump components

Action: Basic test with splash water

analysis of fuel filters & fuels for moisture content

WK 32, RB

Audi/ RB

2) Non-responsive content removed -> **Fuel characteristics (steroyl glucosides)**

Unlikely, because Non-responsive content removed does not use biodiesel

Fuel analysis (SGS Survey) from winter 2006/2007 and 2007

Non-responsive content removed and Non-responsive content removed do not show any indication of similarities / abnormalities with regard to the fuel properties in these countries

Procurement (steroyl glucosides) for basic tests

a.s.a.p.; RB

3) **Air in the fuel (false air in the system)**

Basic test with a high proportion of air

WK32; RB

4) **CT analysis of vehicle system** (4 vs. 6 cylinder, application, load pattern), WK 32; RB (comparison of CP4.2 with CP4.1 operating conditions, fitting, drive)

5) **Analysis of fuels in and around** Non-responsive content removed

a.s.a.p.; RB

Diesel Systems

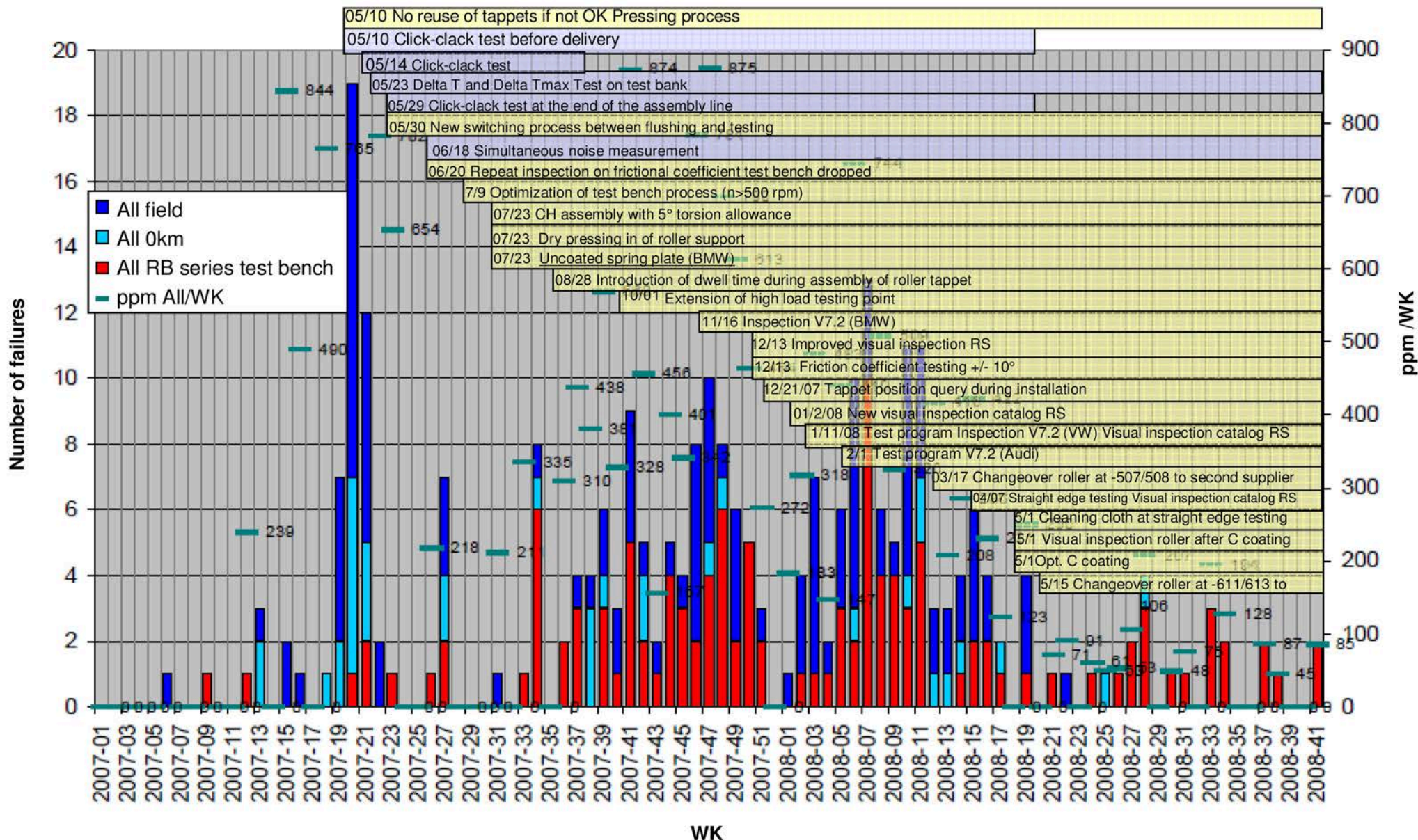
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Non-responsive content removed 08.01.2008 | Non-responsive content removed | © Robert Bosch GmbH 2007. All rights reserved, also regarding any disposal, exploitation, reproduction, processing, distribution, as well as for the registration of special industrial property rights.

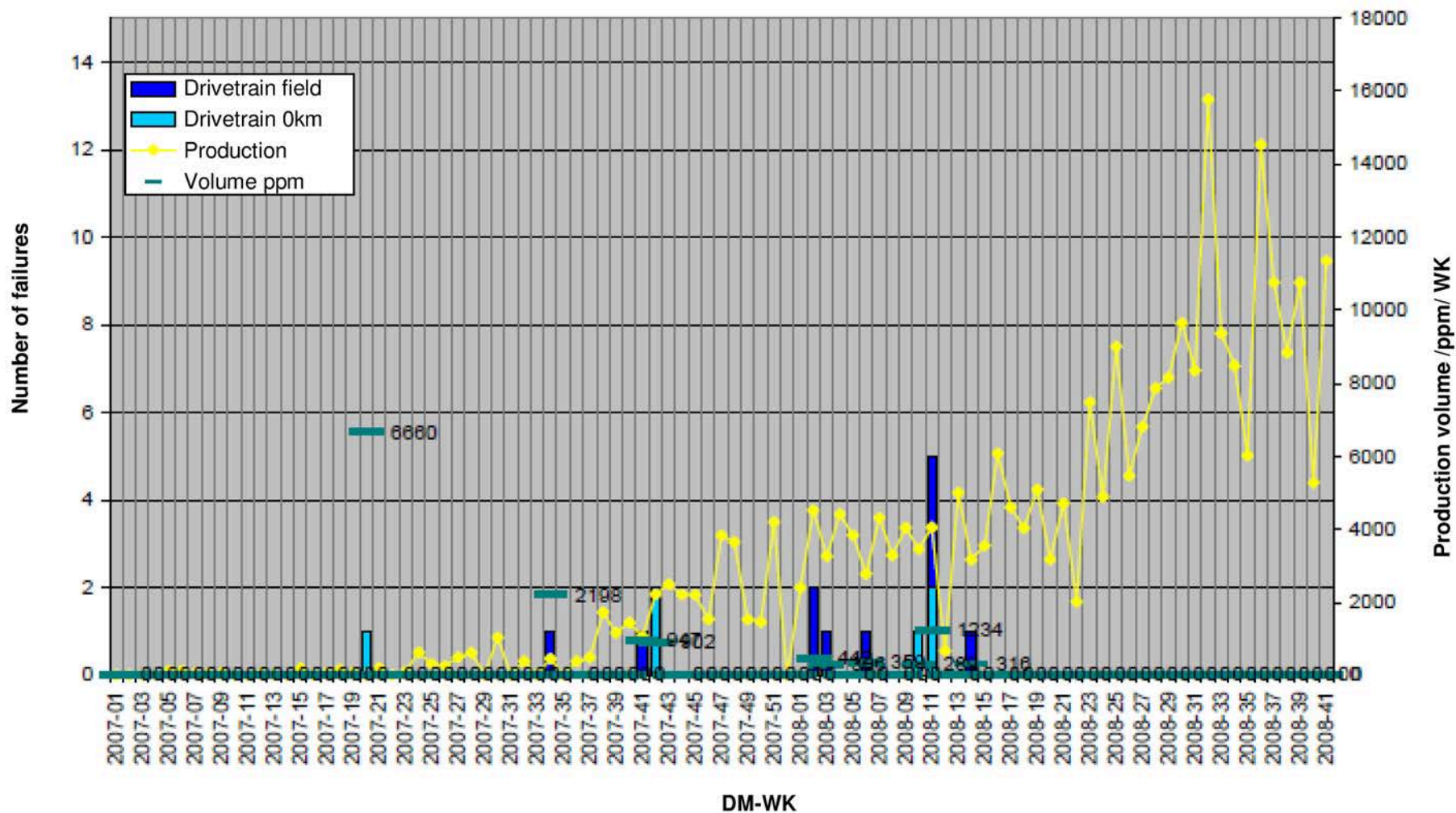


BOSCH

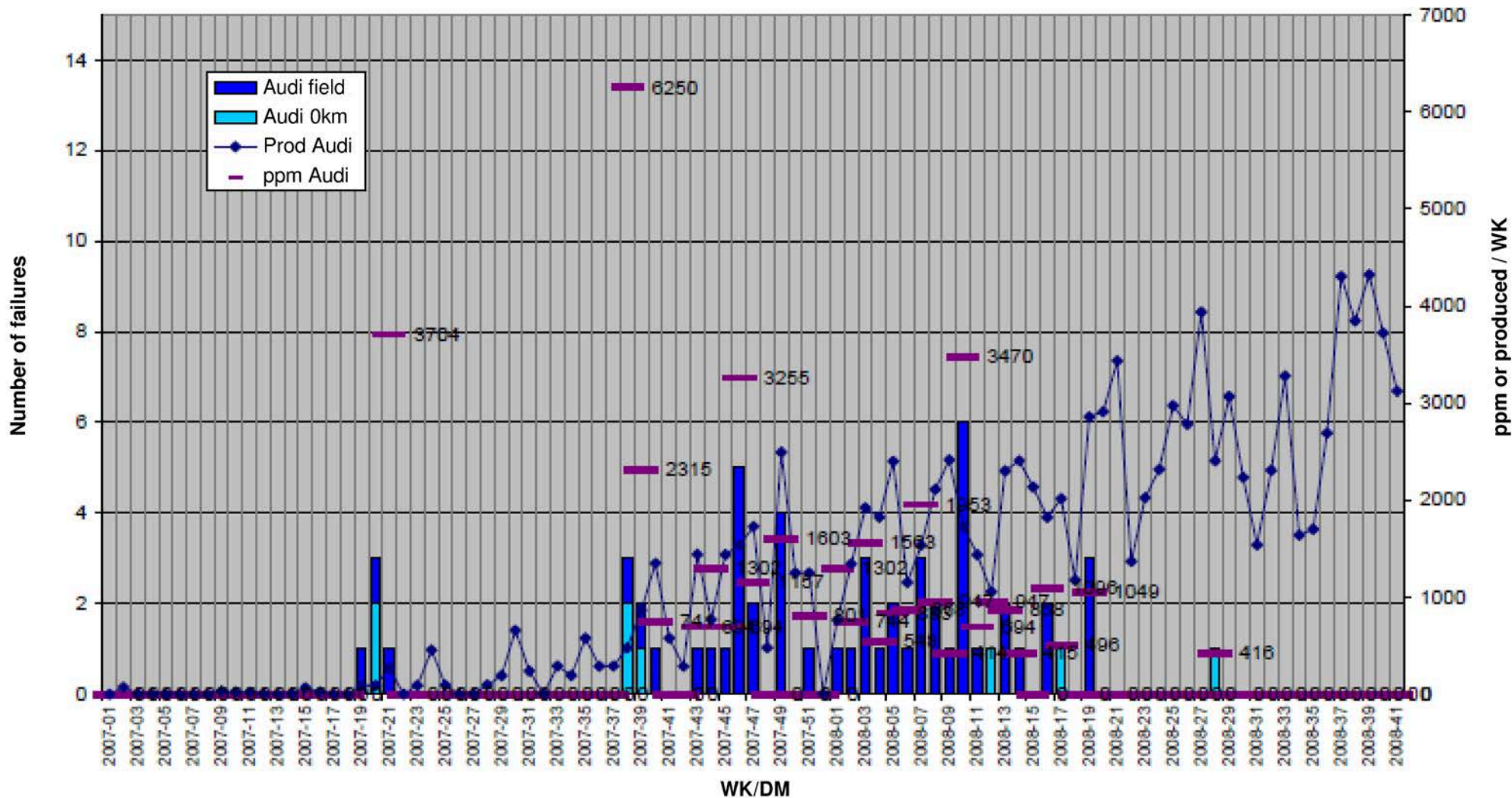
Failures due to drivetrain damage DM WK



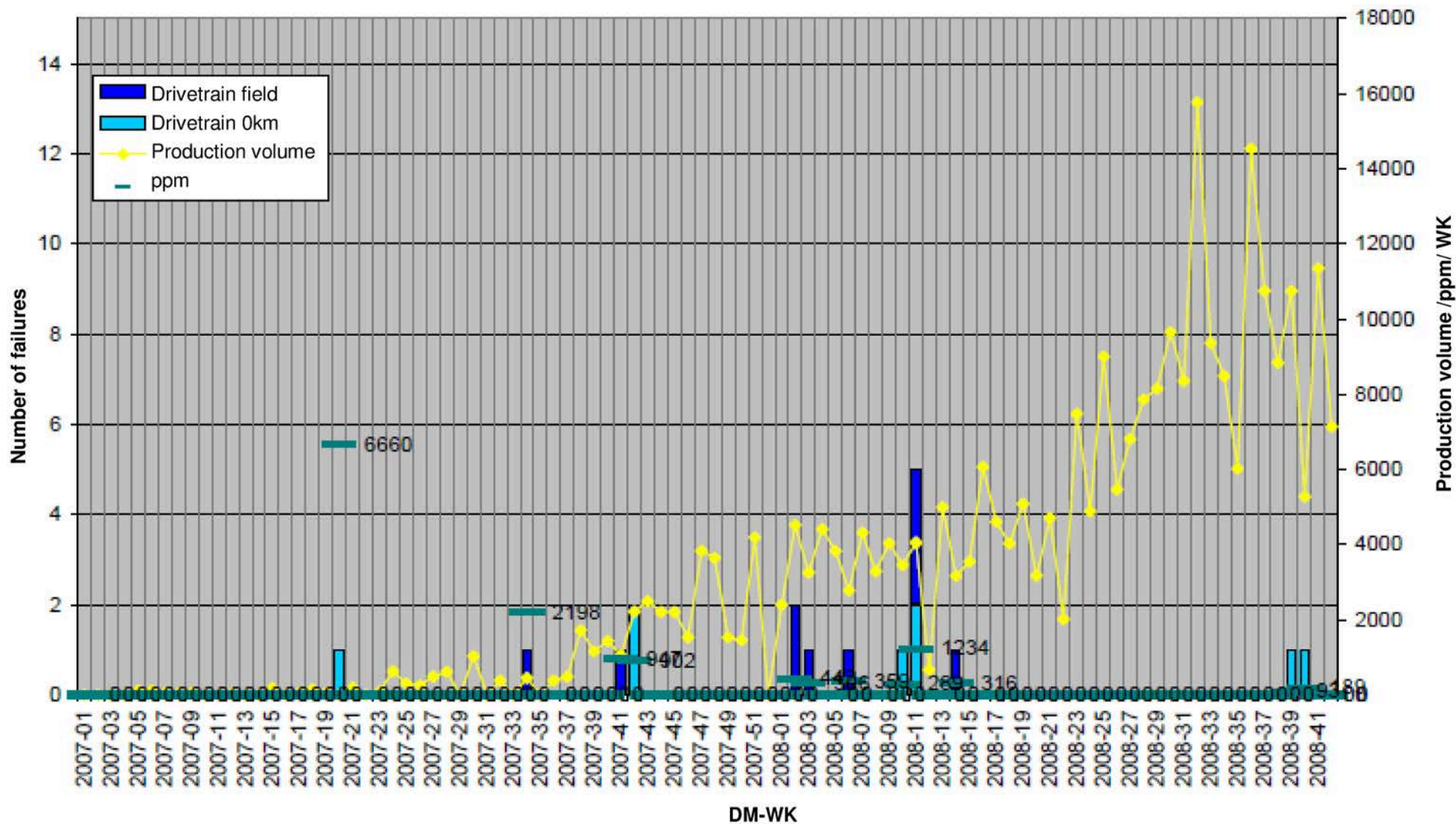
Drivetrain damage VW/Audi CP4.1(-507/508) 0km and field /DM-WK



Drivetrain damage VW/Audi CP4.2 (-611/613) 0km and field /DM-WK

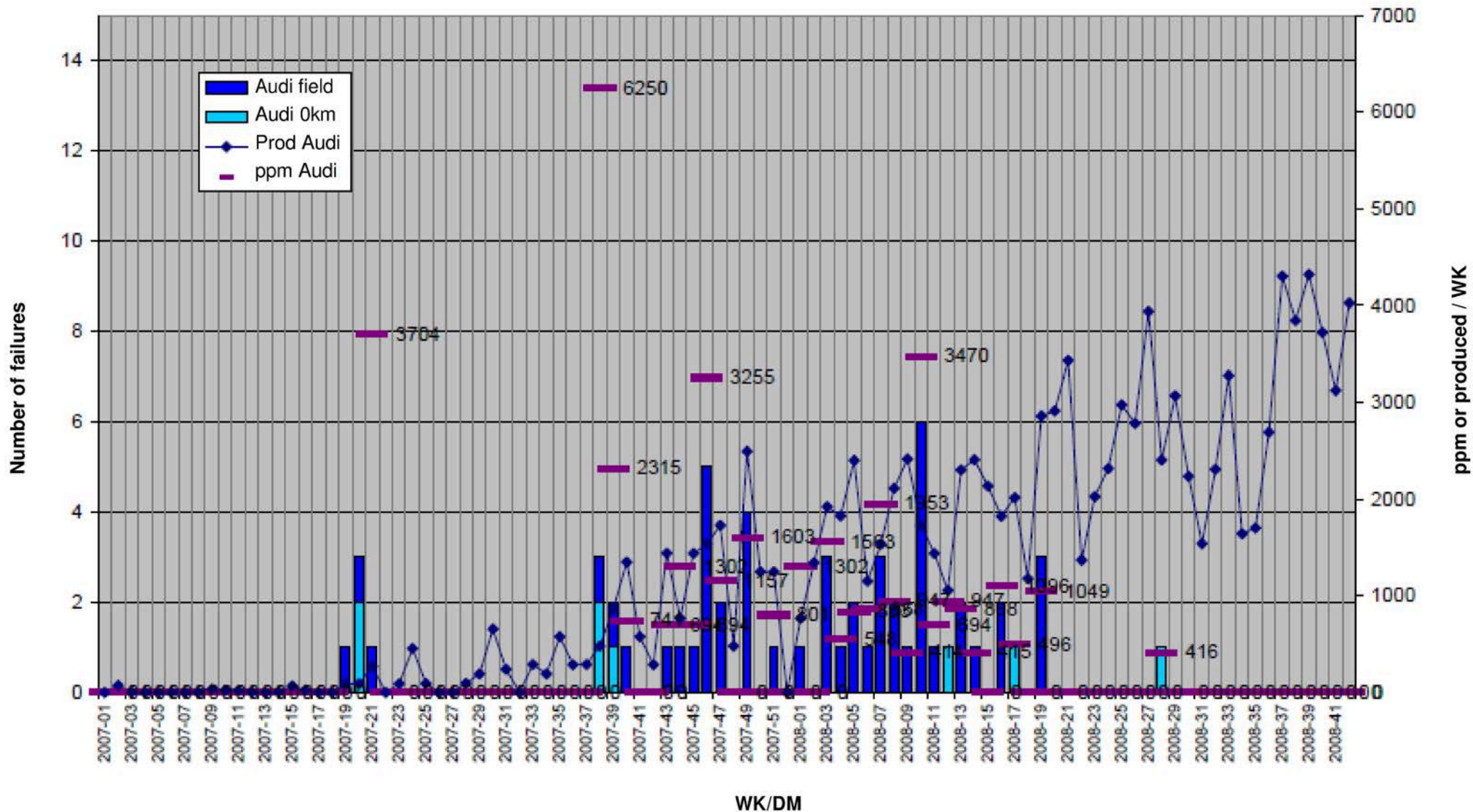


Drivetrain damage VW/Audi CP4.1(-507/508) 0km and field /DM-WK

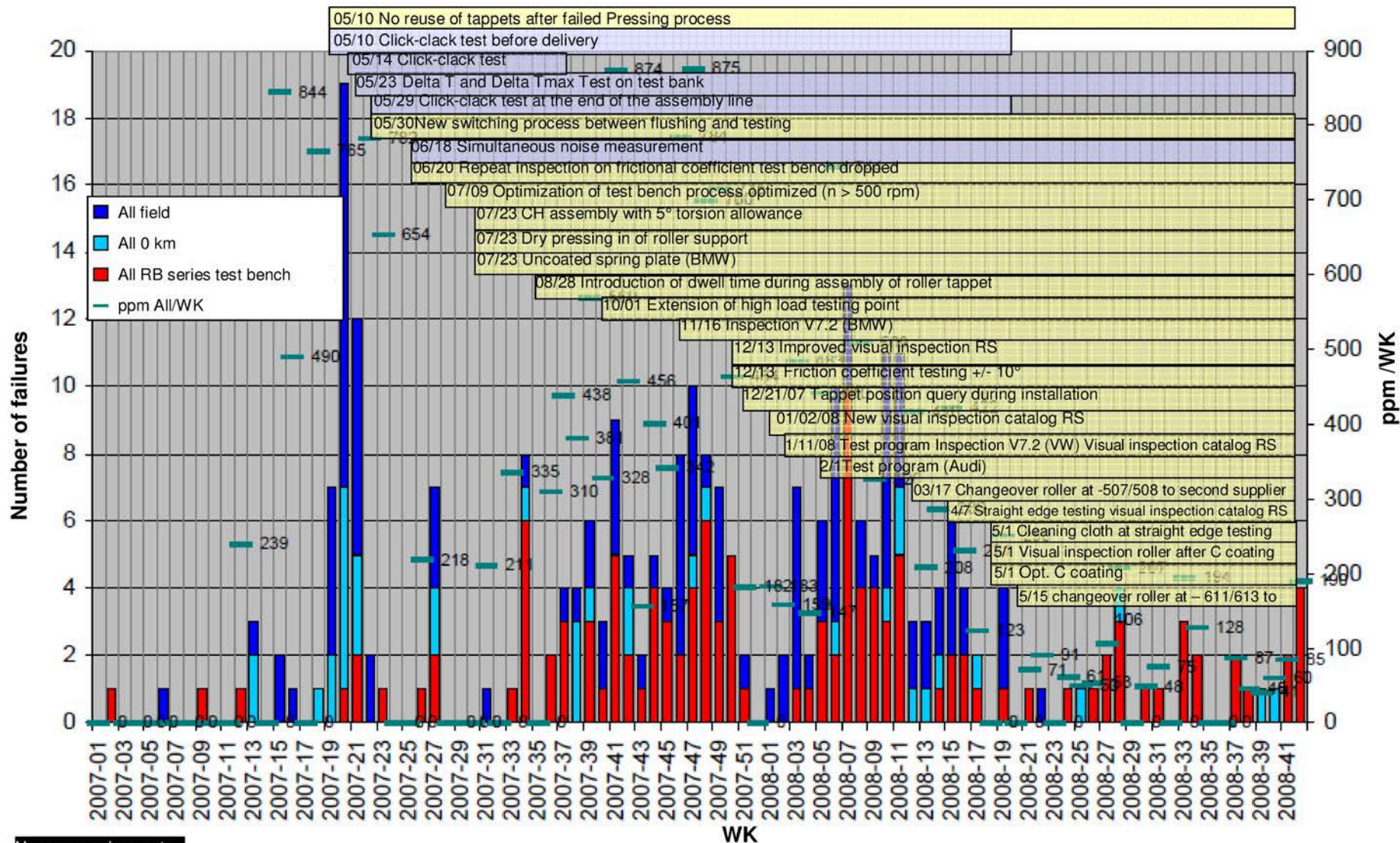


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Drivetrain damage VW/Audi CP4.2 (-611/613) 0km and field /DM-WK

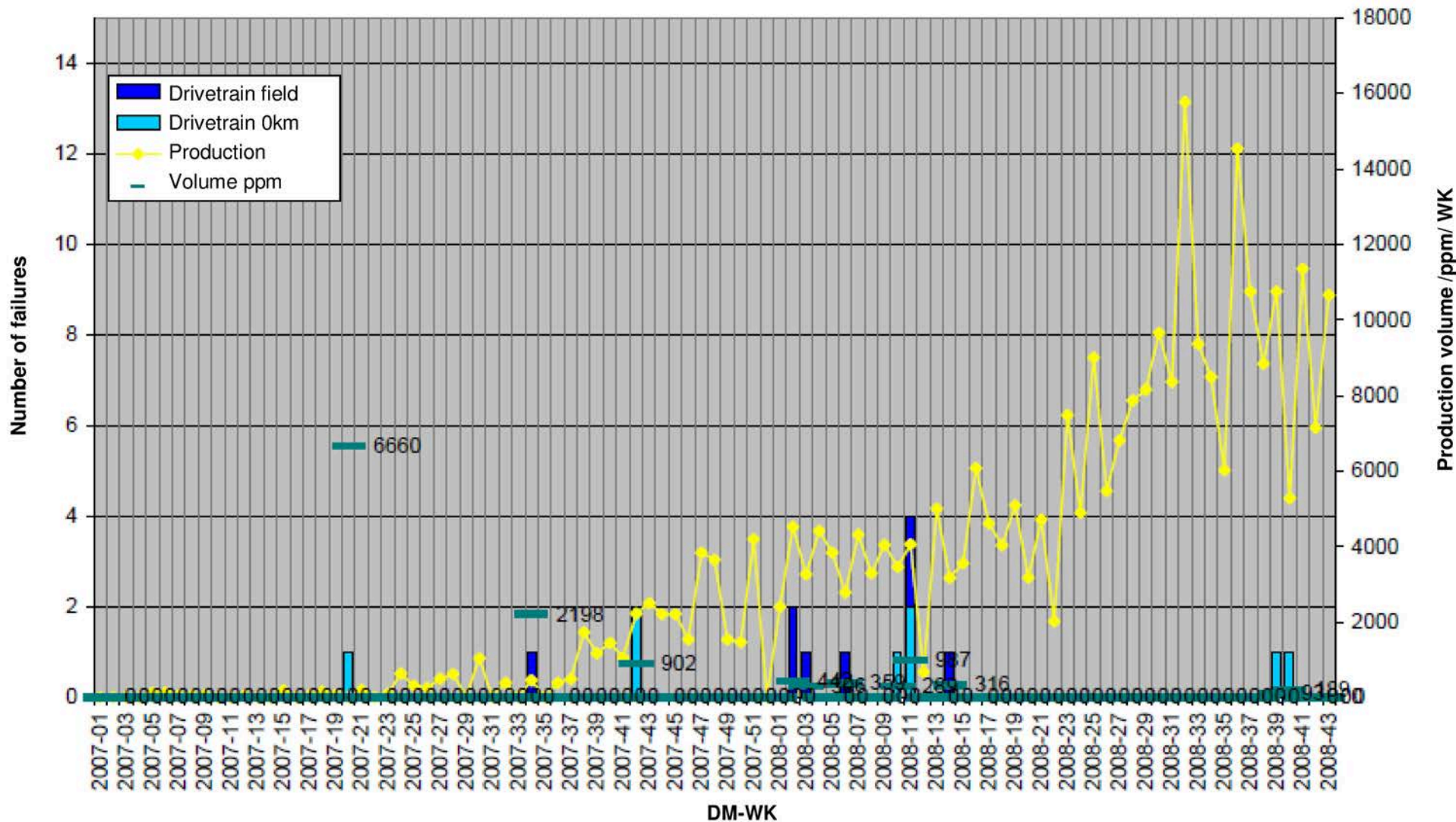


Failures due to drivetrain damage DM-WK

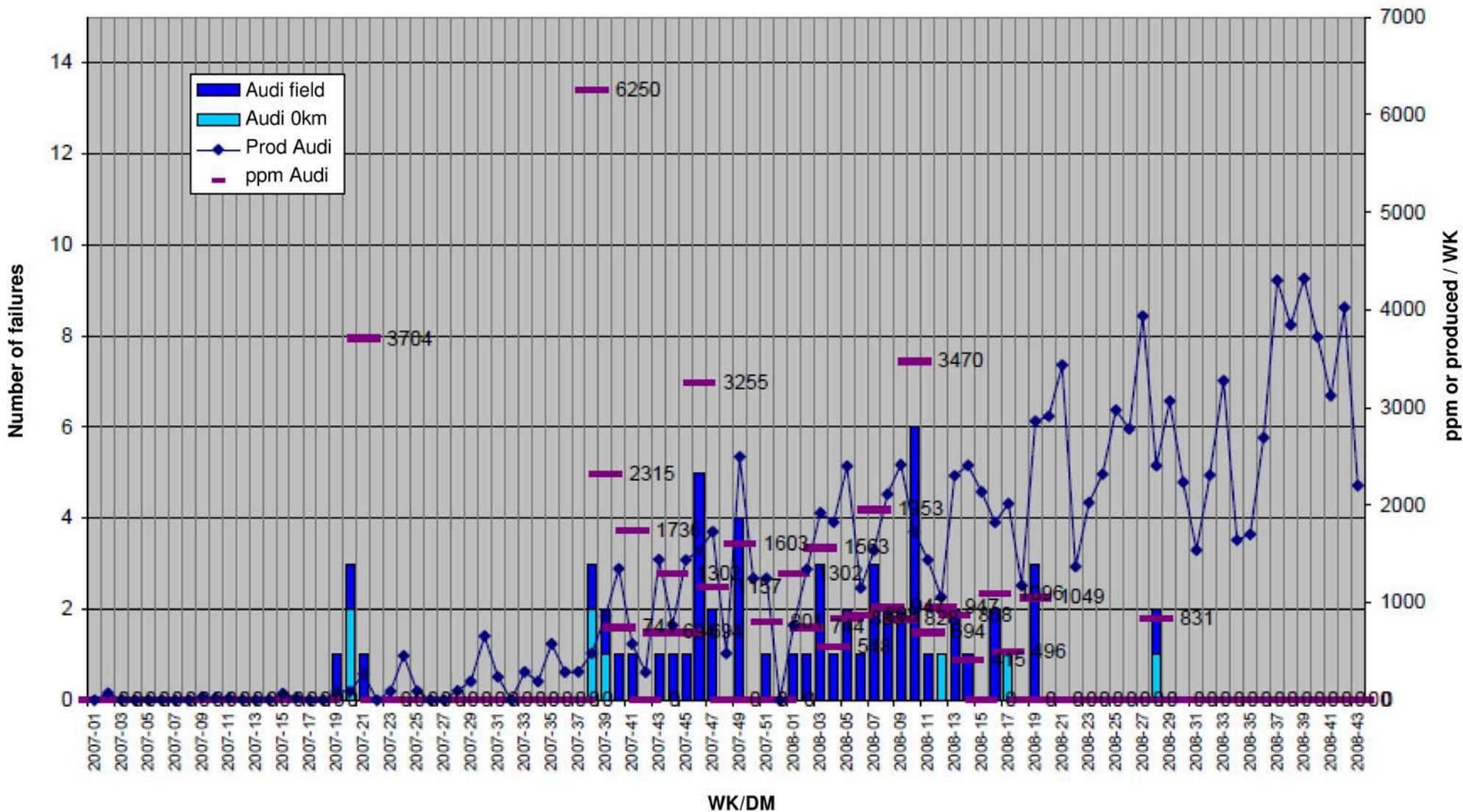


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Drivetrain damage VW/Audi CP4.1 (-507/-508 or 03L 130 755 / 03L 130 755 A) 0km and field /DM-WK

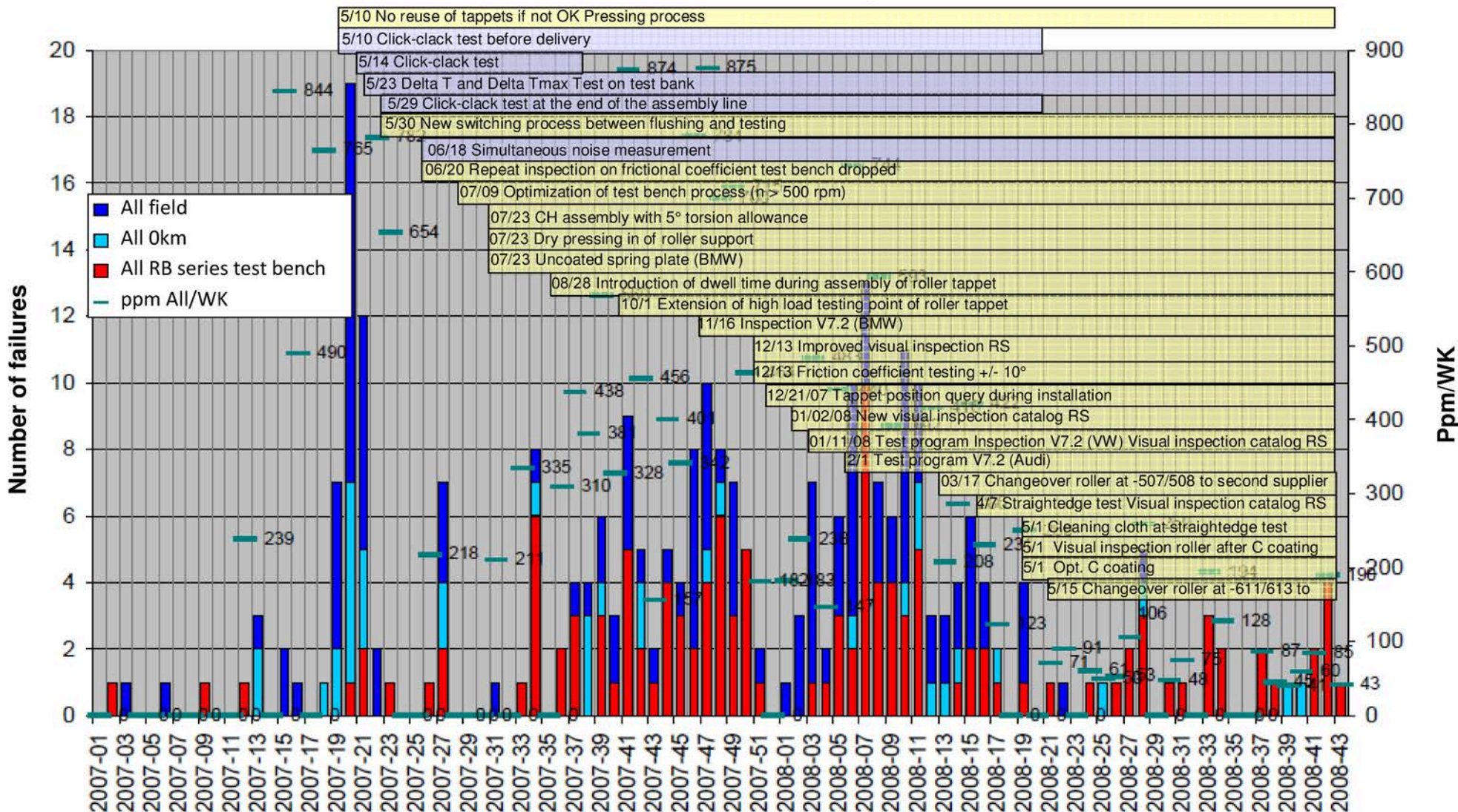


Drivetrain damage VW/Audi CP4.2 (-611/613 or 03L 130 755 AB / AG) 0km and field /DM-WK



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Failures due to drivetrain damage DM-WK



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WK

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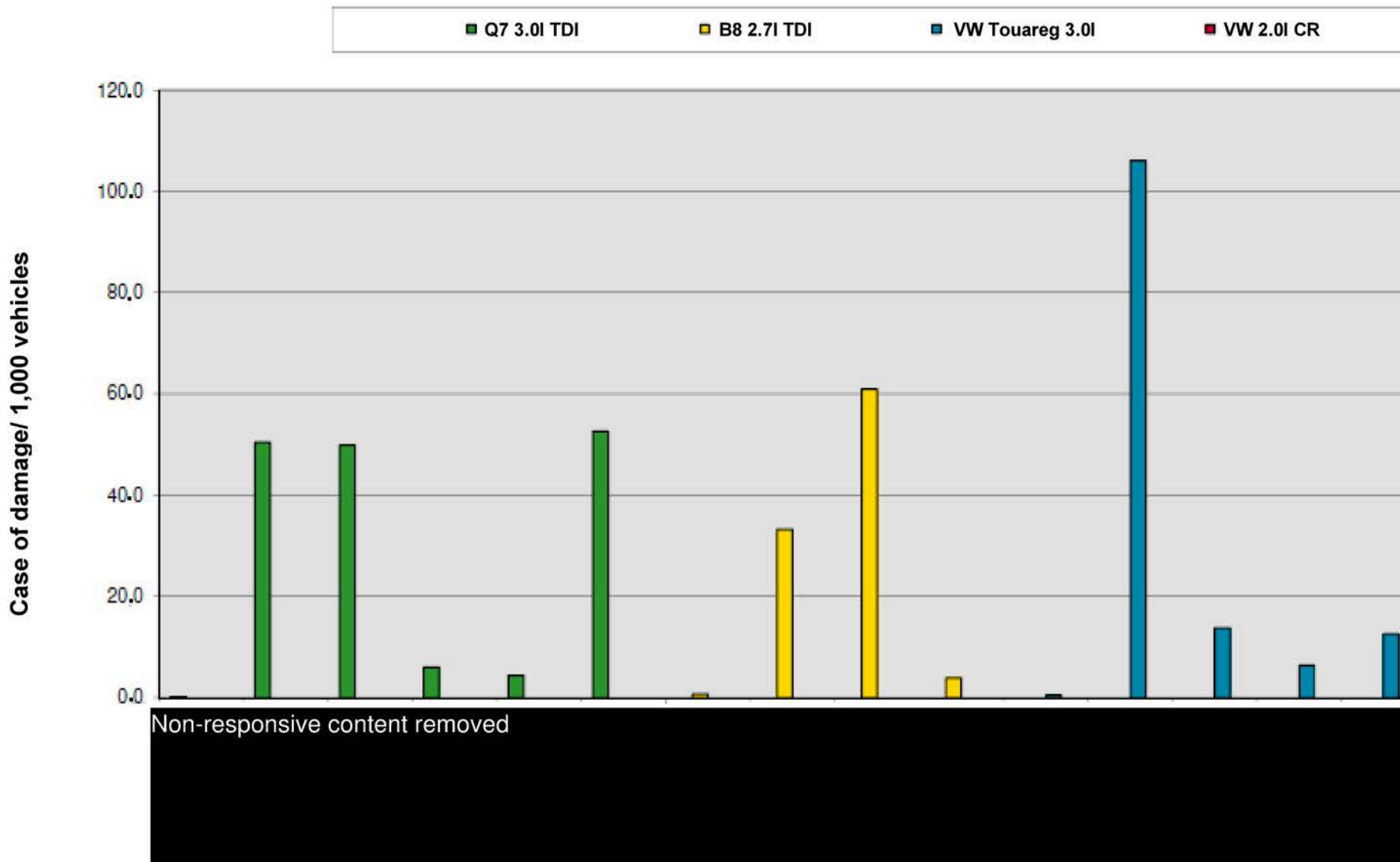
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Only vehicle failures in the field

Model	Engine	Market	Failures	Total	Delivery amount of vehicles SGP - June 08	Delivery amount of vehicles July - Sept. 08	Delivery amount of vehicles SGP - Sept. 08	First vehicle delivery in the market	Failure rate in parts per thousand until June 08	Failure rate in parts per thousand until September 08	Factor above average in worldwide comparison	Non responsive content removed		
Audi Q7 3.0l	3.0l	Non-responsive content removed	1	57	19,344	4,537	23,881	Dec 07	2.9	2.4	---			
			13		0,655	1,169	1,824	Dec 07	0.3	0.1				
			18		187	71	258	Dec 07	69.4	60.4	21	347		
			19		217	4	221	Dec 07	66.5	49.8	21	243		
			3		474	24	501	Dec 07	6.3	4.9	3	41		
			11		1,954	583	2,537	Dec 07	5.6	4.3	2	30		
			4		76	229	78	Jan 08	52.6	45.4	22	252		
			2		2,812	625	3,437	Dec 07	0.9	0.6				
			1											
			1											
			Audi A3/A4/A5 2.0l	2.0l		14	87,860	82,870	140,530	Oct 07	0.2	0.1		
1				24,813	18,540	43,358	Oct 07	0.2	0.2					
1				10,324	3,884	14,208	Nov 07	0.1	0.1					
2				2,225	494	1,730	Dec 07	1.0	1.2					
1				2,723	3,851	16,129	Dec 07	0.1	0.1					
2				1,724	1,070	2,784	Dec 07	1.3	0.7	7	4			
1				1,225	34	1,858	Nov 07	0.8	0.5	6	3			
Audi A6/A8 2.7l	2.7l		43	18,516	6,040	24,556	Sept 07	2.3	1.8					
1				8,509	2,389	8,208	Sept 07	1.3	1.1					
13				243	148	391	Dec 07	63.9	33.2	18	48			
10				161	3	164	Nov 07	62.1	61.9	25	84			
10				1,995	822	2,817	Sept 07	6.0	3.8	2	5			
2				1,777	318	2,095	Sept 07	1.1	1.0					
1														
Audi A6/A8 3.0l	3.0l		2	2,329	850	3,179	Sept 07	0.4	0.3					
1				48	2,238	2,278	Sept 08	69.0	6.9					
0				0	810	1,103	Sept 08	0.0	0.0					
0				0	334	334	Sept 08	0.0	0.0					
1														
VW Phaeton 3.0l	3.0l		4	3,347	43	29	Sept 08	38.5						
1				2,824	378	3,000	Oct 08	0.4	0.3					
1														
VW Touareg 3.0l	3.0l		75	10,829	2,688	13,517	March 07	6.9	6.6					
1				4,525	1,837	6,362	March 07	0.1	0.1					
14				120	12	132	Nov 07	116.7	106.1	19	221			
17				10,008	227	10,235	Nov 07	16.8	13.6	2	29			
5				759	in QUASIS-F1	759	in QUASIS-F1	6.3	6.3	1	13			
33				1,962	378	1,840	Apr 08	14.7	12.5	2	28			
4				431	72	500	Nov 07	9.2	7.9	1	18			
5														
1														
1														
VW Passat 2.0l	2.0l		12	42,039	25,039	67,078	July 07	0.3	0.2					
4				16,505	12,621	31,126	Jul 07	0.3	0.1					
7				6,250	3,969	10,219	Feb 08	0.3	0.3					
1				407	47	454	Feb 08	2.3	2.2					
2				3,111	1,836	4,947	Feb 08	0.4	0.3					
2				4,813	2,221	7,034	Feb 08	0.4	0.3					
1				44,862	16,271	61,133	Feb 07	0.4	0.3					
5				11,028	7,002	18,030	Feb 07	0.3	0.2					
2				4,163	1,479	5,642	Oct 07	0.5	0.4					
1				2,073	866	2,939	Sept 07							
2														
1														
1 x Golf														
1				8,299	2,186	8,485	Sept 07	0.3	0.3					
5				459	344	873	Sept 07	5.3	4.4	11	17			
Jetta USA 2.0l	2.0l	Jetta USA 2.0l	8	1,379	4,779	6,158	Oct 07	5.8	1.3	4	6			
Blacka Superb 2	2.0l 125 kW		1											
Total field			234											

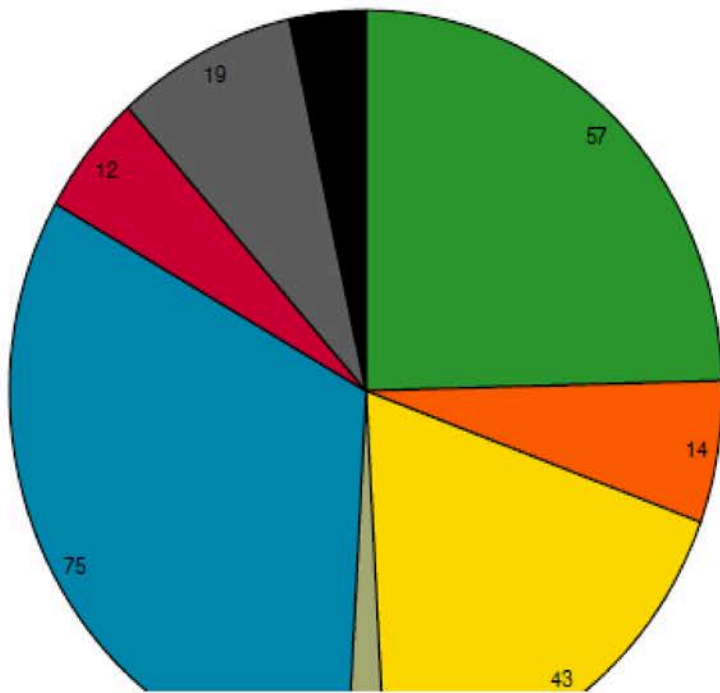
Names, departments displaced by ABCO	Qty	Deliveries	Failure (parts per thousand)
Non-responsive content removed	48	4474	11.3
	21	2992	11.0
	29	2294	11.4
	28	2294	11.3
	21	4179	6.6

Failure rate of critical markets CP4
(SOP - June 2008)



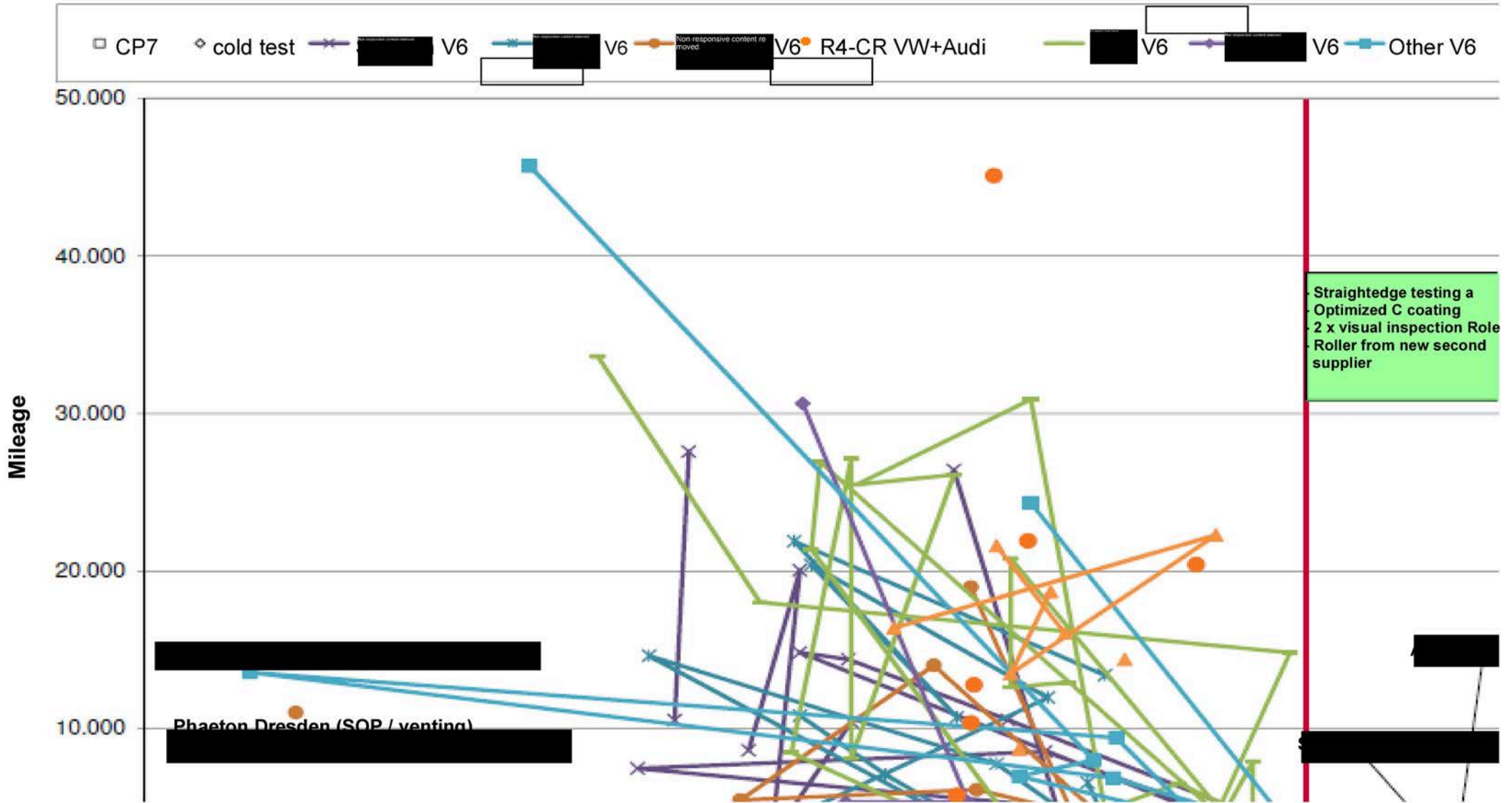
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Number per model / engine
(without individual cases)



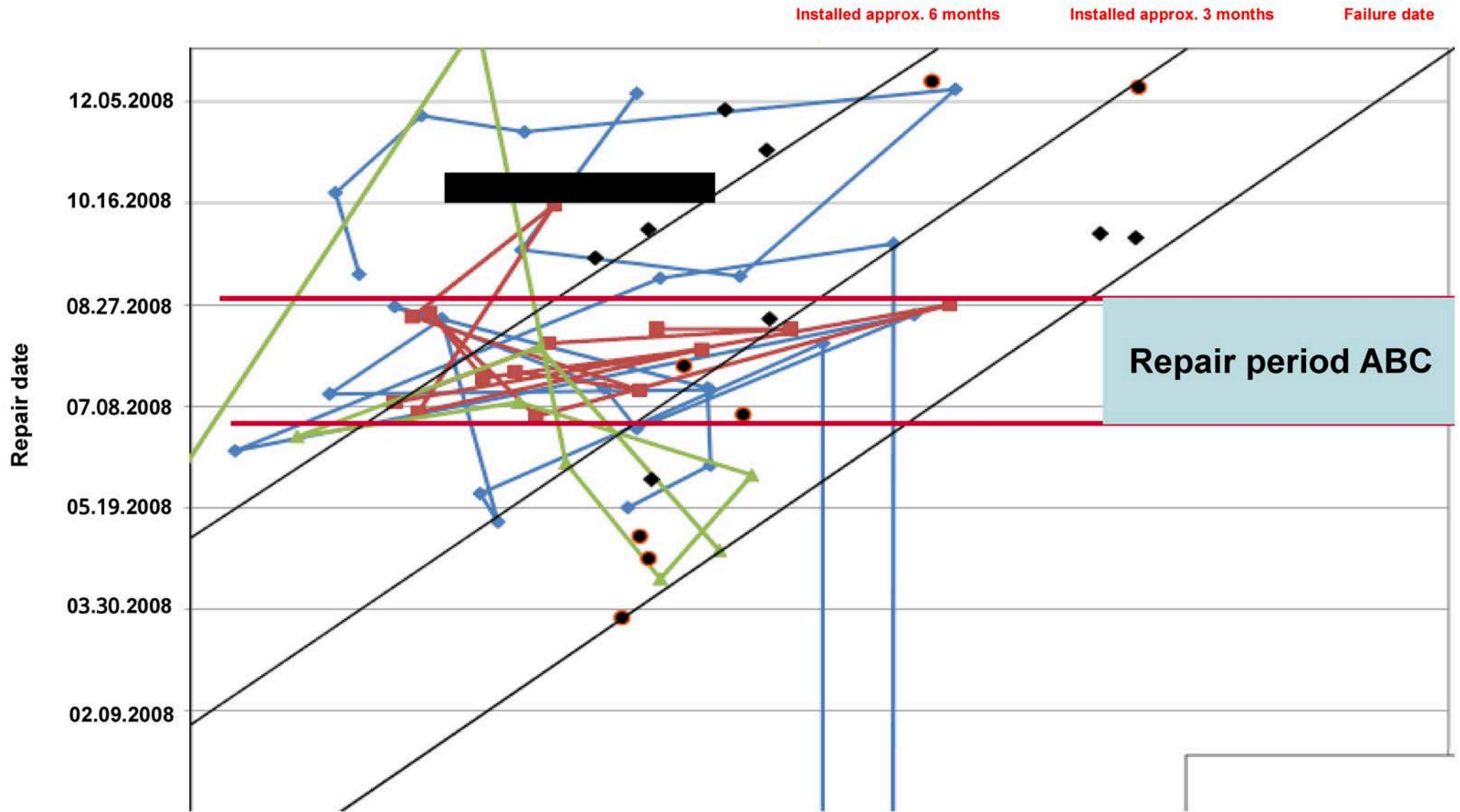
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Effectiveness of actions

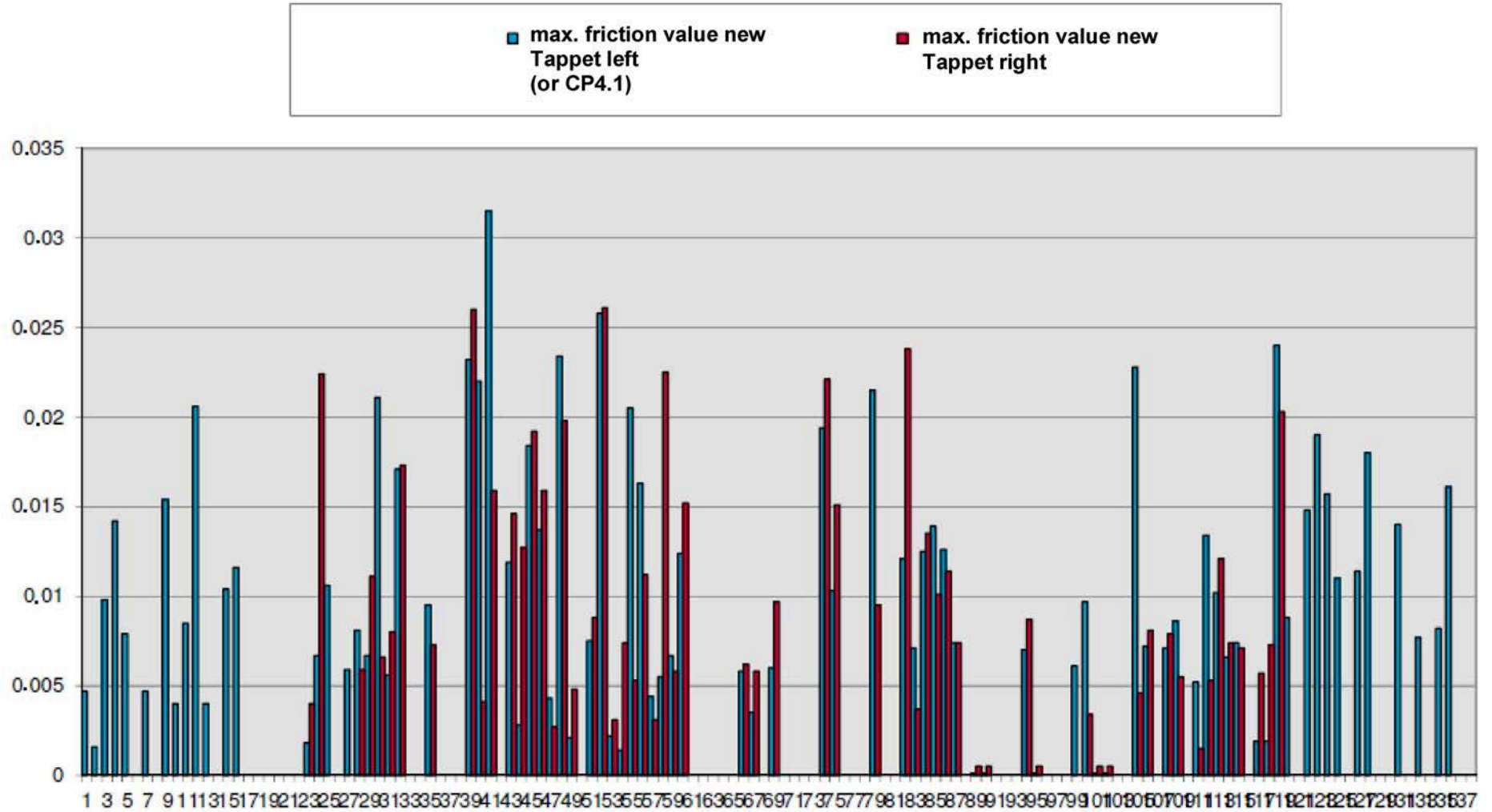


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Repair date beyond registration date



Maximum coefficient of friction tappet new



Status of drivetrain damage



Worldwide on-field failures (based on Non-responsive content removed list dated 02.04.2009)

Observation period from each vehicle SOP up to June 2008

Non-responsive content removed

→ 41 x CP4.2 / delivery quantity 550	-> 74,545 ppm
→ 5 x CP4.1 / delivery quantity 2,303	-> 2,171 ppm

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→ 31 x CP4.2 / delivery quantity 1,267	-> 24,467 ppm
→ 2 x CP4.1 / delivery quantity 1,225	-> 1,632 ppm

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→ 11 x CP4.2 / delivery quantity 18,839	-> 584 ppm
→ 16 x CP4.1 / delivery quantity 61,246	-> 261 ppm

→ **After DM WK 20/2008 no field failures in the aforementioned markets.**



Field failures worldwide (excluding testing and ER)

VW vehicles total: **120/27** reported / thereof diagnosed and confirmed

- 4-cylinder █████ (CP4.1): 34/5 (Tiguan, Passat)
- 4-cylinder US07 (CP4.1): 8/3 (Jetta)
- 6-cylinder (CP4.2): 78/19 (Touareg, Phaeton)

Audi vehicles total: **121/73** reported / thereof diagnosed and confirmed

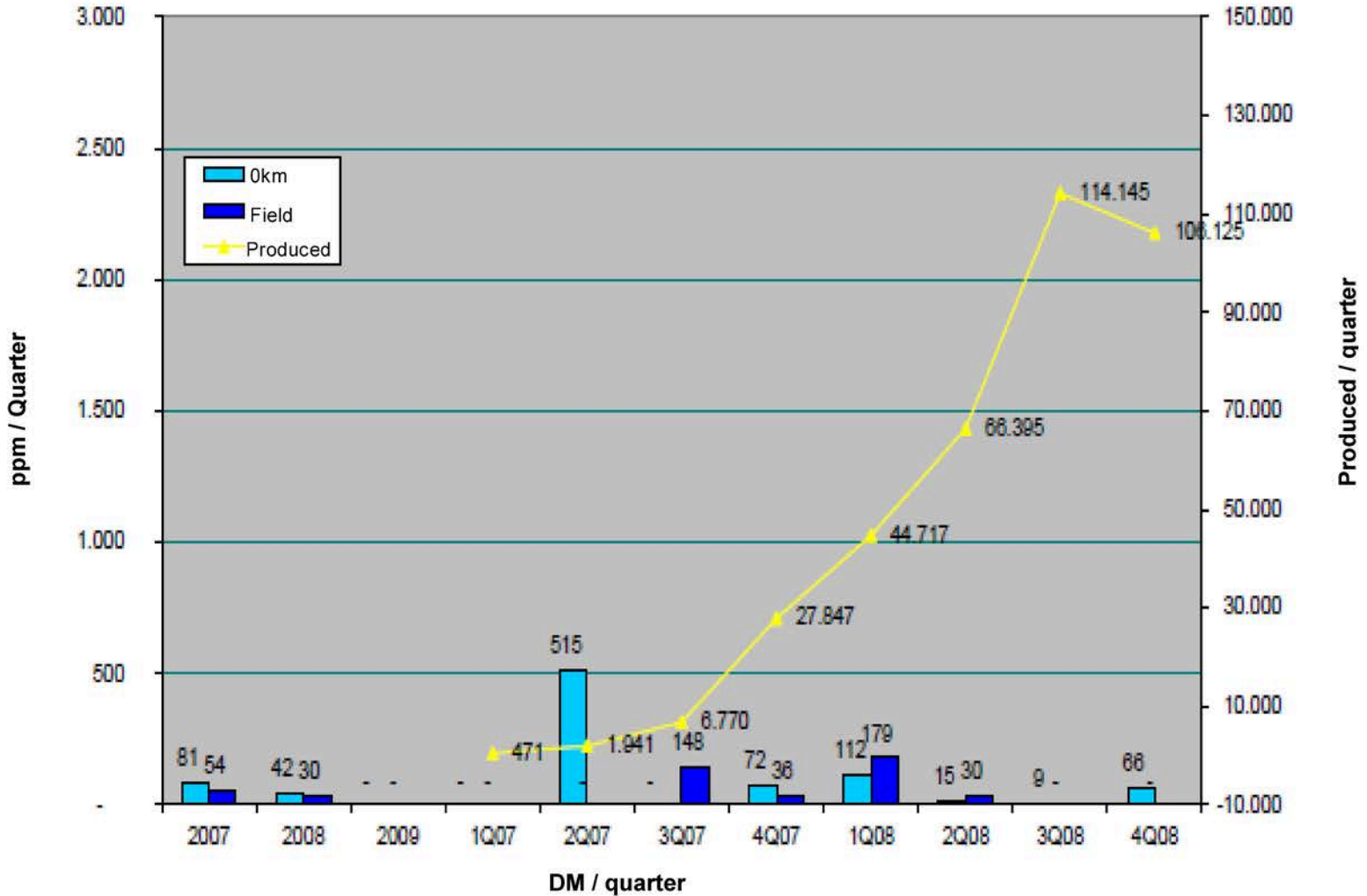
- 4-cylinder █████ (CP4.1): 16/8 (B8)
- 6-cylinder (CP4.2): 105/65 (B8, Q7)

Status: WK 06.09



CP4.1 VW / Audi - Quarterly Overview

Drivetrain damage VW / Audi CP4.1



Including BA 40 = Field goods
 BA 70 = outside the RB warranty for testing

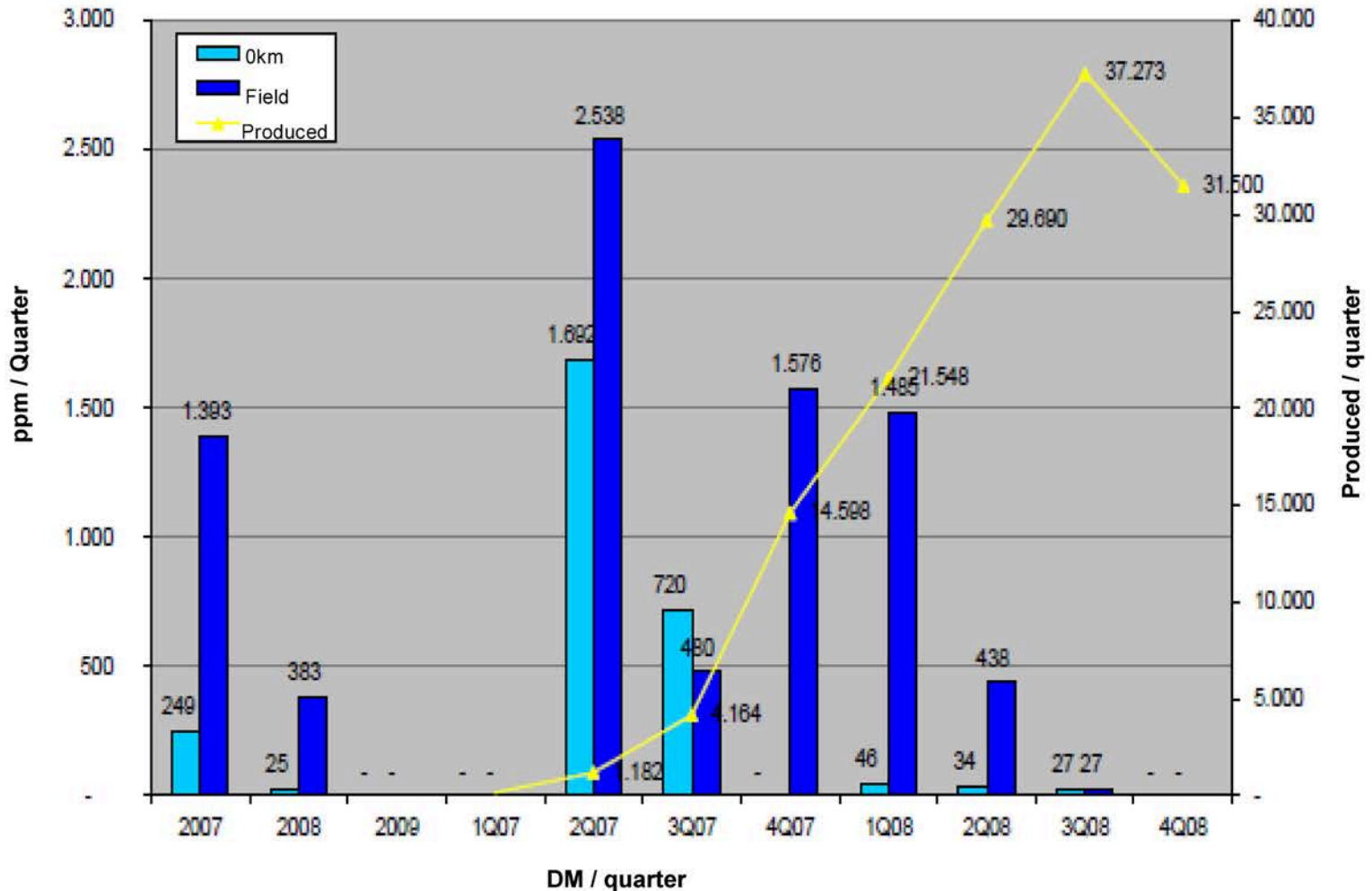
Appendix 9 to SVW 982 154 - 8. Steering Committee Diesel Systems



BOSCH

CP4.2 VW / Audi - Quarterly Overview

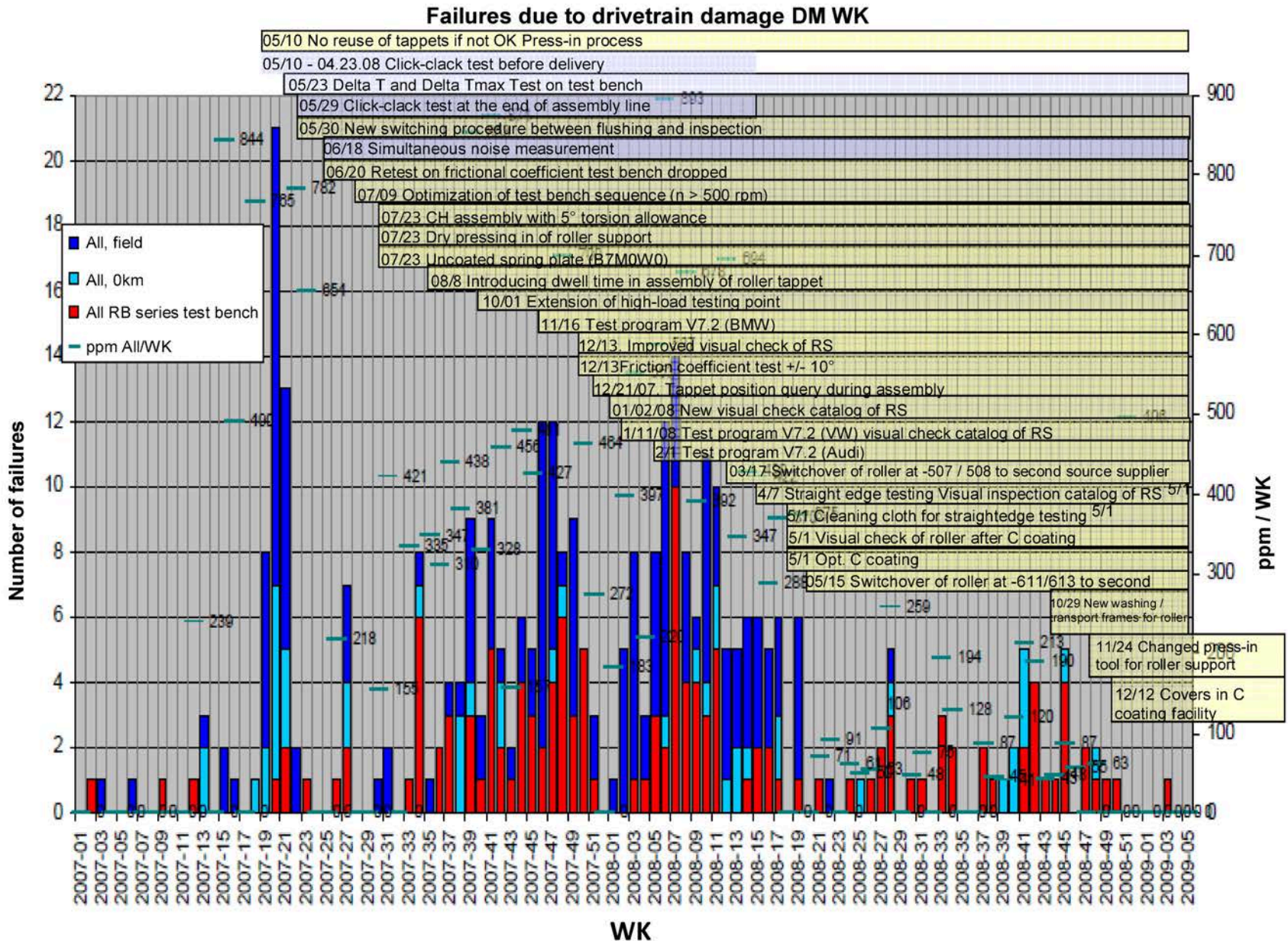
Drivetrain damage Audi / VW - CP4.2



Including BA 40 = Field goods
 BA 70 = outside the RB warranty for testing



Overview of drivetrain damage



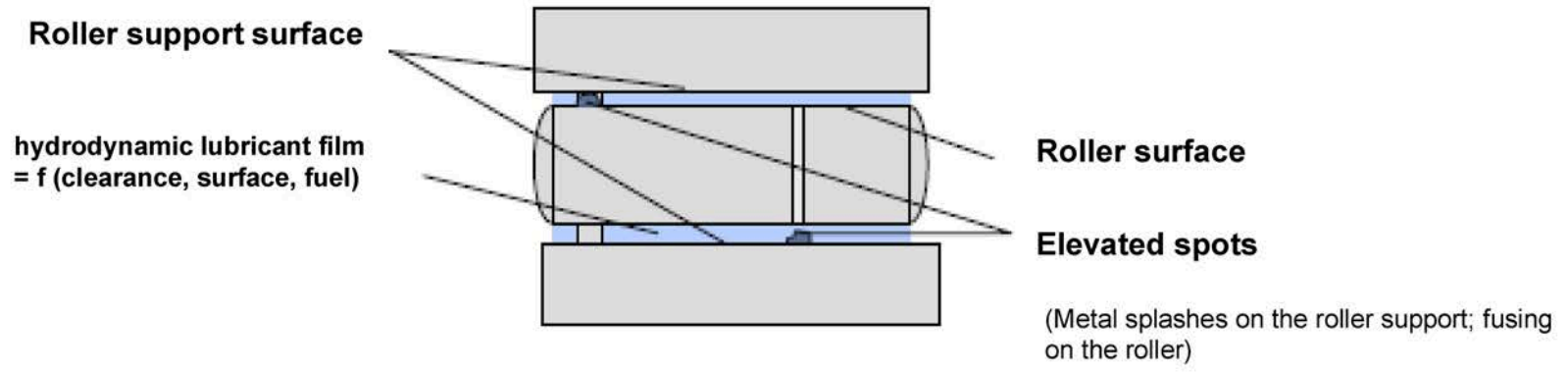
Appendix 9 to Non-responsive content removed - 8. Steering Committee Diesel Systems




CP4 Drivetrain damage: Damage mechanism

- Unacceptably high mixed friction between roller and roller support cause "local" contacts during operation
- The C coating is disrupted (wear and erosion of the C coating), the coefficient of friction between roller and roller support increases
- Stiff roller -> Wear -> Particle formation -> Drivetrain damage

Intensification factors: Fuel with low viscosity; elevated spots on roller (e.g. fusing) and in the roller support (e.g. metal splashes); surface of roller/roller support

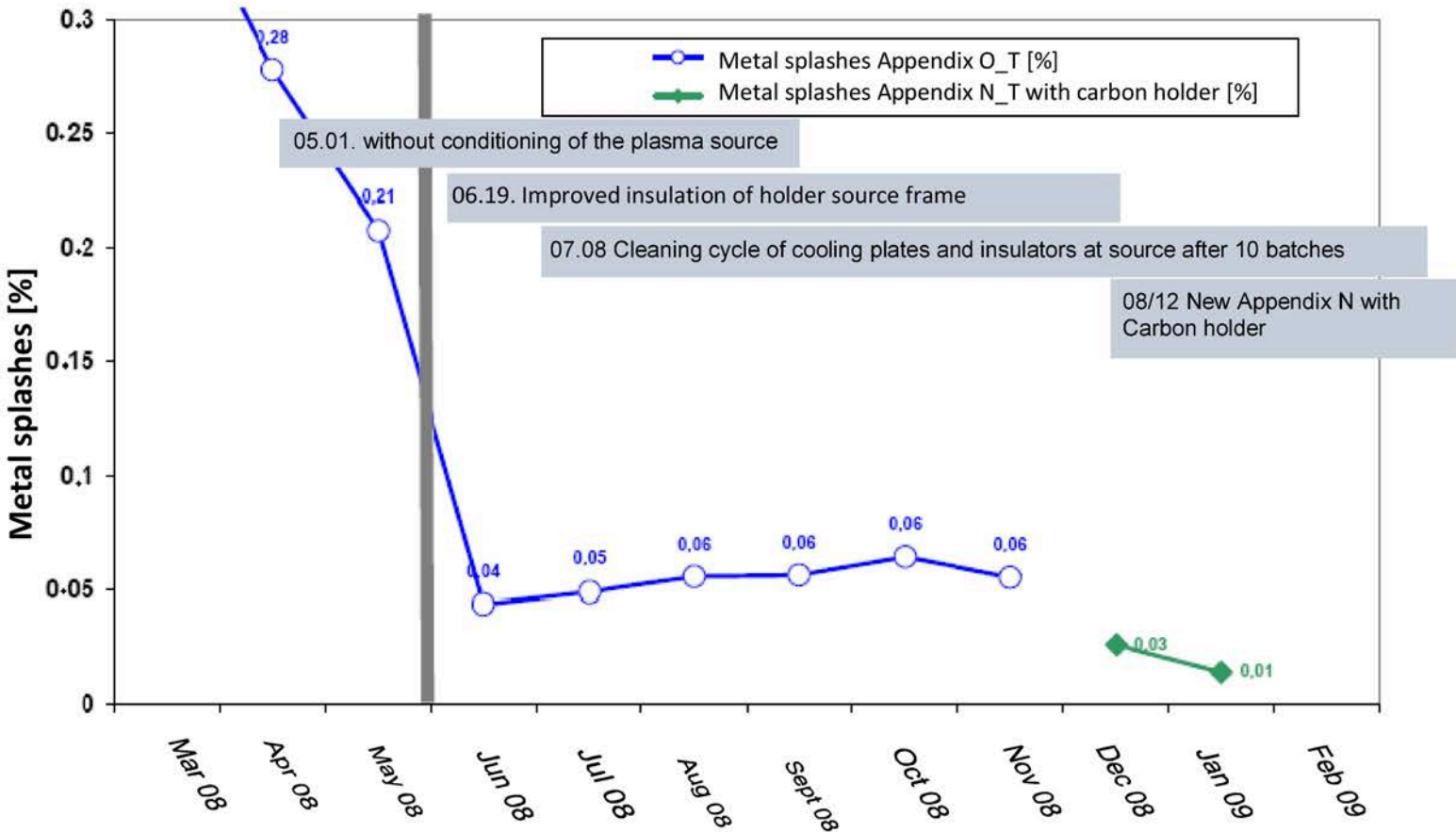


Explanation of terms: "Metal splashes"


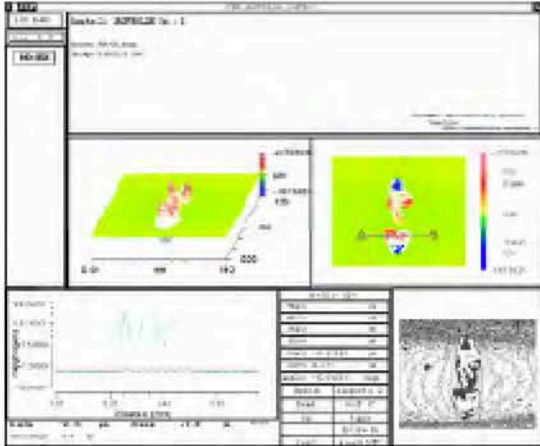
 <p>A microscopic image showing a circular metal splash on a green surface. The splash is roughly spherical with some internal structure visible. A small white label is present in the bottom right corner of the image.</p>	<p>Affected component: Roller support</p> <p>Remark: Metal splashes are frequently rough-finished and then become visible. Depending on the size and height, a visible shadow is also created by the finishing process</p>
	<p>Cause: During the C3 coating process of the RS, ambient material is entrained and deposits on the component. There are different shapes, sizes and degrees of metal splashes. Depending on the time of occurrence, the metal splashes are finally coated with C3</p>

Development of metal splashes on roller support

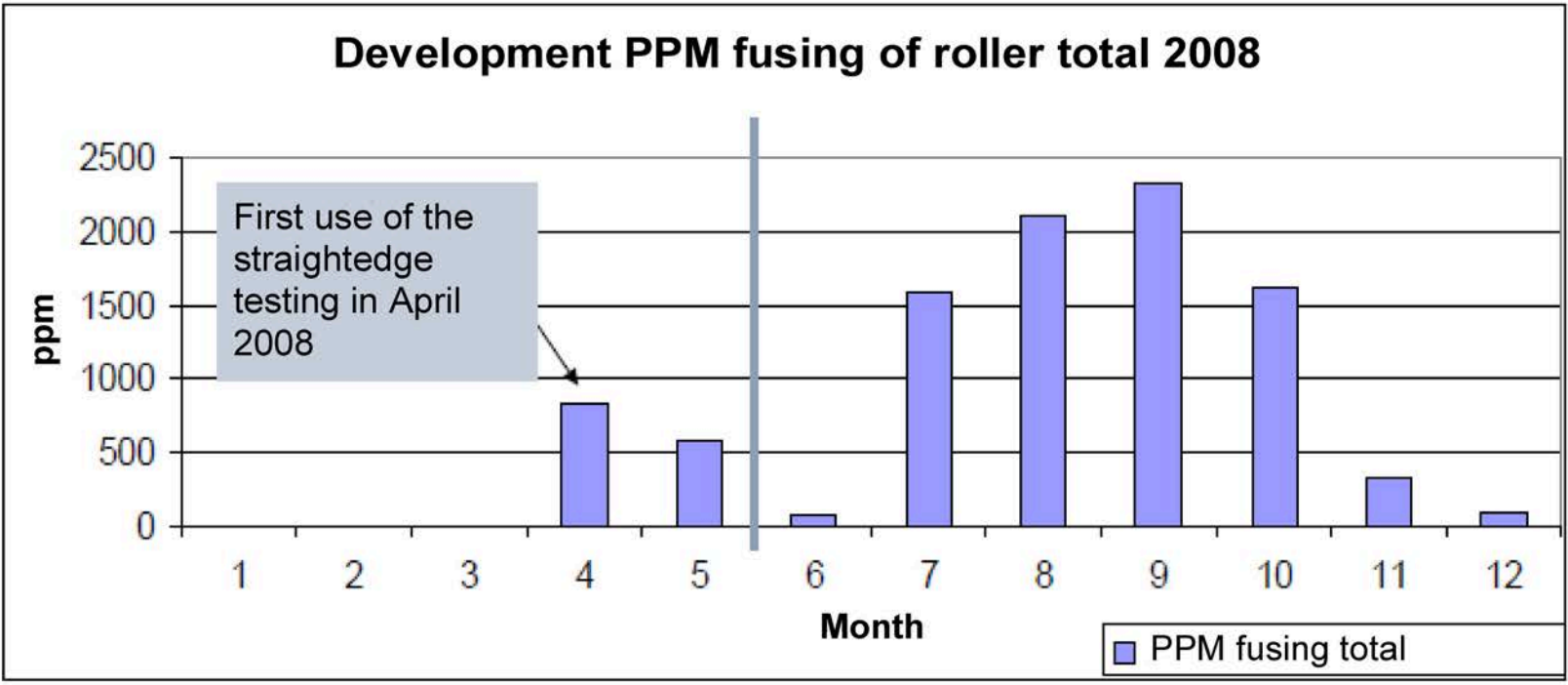
Monthly trend 2008 + 2009
Metal splashes in CP4 - roller support after band finishing



Explanation of terms: "Fusing"

	<p>Affected component: Roller</p>
	<p>Suspected cause: Fusing occur during the C3 coating process of the roller end due to insufficient contacting between the rollers in the holder. Partly excessive current flows and leads to material melts of the roller having depressions and elevations. Occurrence is strongly scattered</p>

Development of the fusing



Friction coefficient examinations

Assignment

Calculation of the coefficients of friction between roller / roller supports with "boundary" roller surfaces (supplier 1 & 2) in combination with different fuels

Results

- Little influence of the roller surface on the coefficient of friction with EN590 recognizable
- Boundary coefficient of friction with "boundary" roller surfaces of a supplier 1, but below limit (0.035@300 revolutions of roller, 600 N)
- Coefficient of friction not OK for "boundary" roller surfaces (supplier 1) @ Sweden diesel & GDK570
- Coefficient of friction OK for "boundary" roller surfaces (supplier 2) @ Sweden diesel & GDK570

Assessment

Rollers from supplier 1 show greater sensitivity to coefficient of friction during measurement with low viscosity fuels. Measure: Optimization of quality Roller surface supplier 1 at supplier 2 level.



Task Force drivetrain - additional measures

1. Reduce surface texture of roller from supplier 1
Introduction of supplier 2: CP4.1 WK12/08(Fe); WK04/08(JhP)
CP4.2 WK20/08(Fe); WK44/08(JhP)
2. Performing challenge trials with poorly lubricating fuel and boundary parts
3. Retesting of the camshaft with respect to drivetrain damage, e.g. particle transfer -> performing challenge trials
4. Joint verification of the start-up conditions in the engine plants / vehicle plants (-> Audi).
5. Evaluating and analyzing the results of roller camera documentation after friction coefficient test



Summary

- Significant reduction in drivetrain damage since WK20 2008 (in particular field),
- Since then only RB internal failures and 0km (CP7)
(Causes of these failures are being analyzed)
- Measures for fault detection and avoidance in the plant show impact
(especially straightedge testing & optimized visual inspection catalog of roller support)
- Additional measures (see previous slide) is under implementation
- Fuel impact (viscosity) on coefficient of friction is proven



Open measures

- Line scan camera system to scan the RS bore WK 19

- Camera documentation of roller after friction coefficient test is under progress

- New concept of roller holders for C coating (critical) D: open



Review Bosch FCT cases for VW/Audi 2.0L TDI up to January 2009



Summary

		Audi	VW	
Total known	(IQIS+FCT)	45 cases	36 cases	(9*)
Reported to FCT		30 cases	21 cases	(6*)
Analyzed on-site		8 cases	5 cases	(3*)

Distribution of the major errors focuses of the cases reported to FCT:

Hydraulic faults	13 cases	13 cases
Electrical faults	11 cases	4 cases
Engine mechanics	4 cases	3 cases
Cause of fault unknown	2 cases	1 case

*Status up to VW review 06.19.2008



VW field failures Non-responsive content removed from 6.19.08 to 01.19.09 (from Bosch warranty system)

CP4.1

GE	Customer complaint	QC no.	Cust. Ref. No.	1 Part no.	DM	CS	Failure D.	Mileage [km]	VIN	Error text	OSA
B	Leaking; liquid loss of diesel	230002229012	VA 98866	0445010507	4/7/2008	5/14/2008	8/11/2008	3901	3C8E234655	Shaft seal flange leaking	without
B	Fuel loss	230002294951	VA 98950	0445010507	3/14/2008	4/16/2008	10/14/2008	27372	3CZ8E208532	Shaft seal flange leaking	without
B	Rail pressure too low	230002284765	VA 98914	0445010507	1/16/2008	3/17/2008	9/19/2008	10380	5NZ8W026463	Pump drivetrain damage	without
B	Leaking, loss of fuel	230002234230	VA 98873	0445010507	10/18/2007	1/2/2008	2/22/2008	30	5N8W011353	Leaking at the shaft seal	without
C	Engine stopped while driving	230002165195	VA 98799	0445010507	1/22/2008	4/1/2008	5/5/2008	3452	5NZ8W036616	Not OK Fuel	1664
S	Vehicle will not start	230002254823	VA 98884	0445010507	10/29/2007	1/16/2008	8/1/2008	20816	5N8W014390	OK according to specification	without
S	Engine does not start. Fuel rail /	230002254821	VA 98885	0445010507	7/6/2008	8/3/2008	8/4/2008	1065	5N9W010496	OK according to specification	without
S	Engine jerks when accelerating.	230002293065	VA 98945	0445010507	8/21/2007	11/9/2007	9/24/2008	12815	5N8W002189	OK according to specification	without
S	Stiff, engine does not start.	230002259785	VA 98890	0445010507	9/17/2007	11/9/2007	5/21/2008	9051	5N8W003445	OK according to specification	without
O	Engine does not start	230002347357	VA 98983	0445010507	2/13/2008	5/23/2008	10/21/2008	15884	3C8E230001		without
O	Engine does not start up	230002348978	VA 98982	0445010507	10/8/2007	9/25/2008	9/25/2008	6532	5N8W006469		without
O	Function not OK	230002348979	VA 98982	0445010507	11/29/2007	2/7/2008	11/11/2008	40837	5N8W017664		without
O	Function not OK	230002348980	VA 98982	0445010507	10/2/2007	11/30/2007	10/6/2008	22362	5N8W005842		without
O	High pressure fuel pump (HPP) is leaking	230002348981	VA 98982	0445010507	1/24/2008	3/29/2008	12/1/2008	16350	3CZ8E190050		without

CRI3.2

GE	Customer complaint	QC no.	Cust. Ref. No.	1 Part no.	DM	CS	Failure D.	Mileage [km]	VIN	Error text	OSA
C	leaking	230002206366	VA 98840	0445116030	5/16/2008	8/1/2008	8/4/2008	3333	3C9E512520	Foreign objects from the outside	1710
C	Engine does not start;	230002216696	VA 98856	0445116030	2/15/2008	6/11/2008	7/9/2008	3348	3CZ8E242833	Foreign objects from the outside	1728
S	Electrical fault	230002211193	VA 98852	0445116030	3/26/2008	5/6/2008	7/29/2008	14092	3C8E231884	OK according to specification	without
O	Loss of fuel at the return line port	230002346982	VA 98984	0445116030	5/10/2008	6/28/2008	10/31/2008	4749	5NZ9W008027	RL O-ring damaged	without

EDC17 No complaints

Diesel Systems



AUDI field failures of submarket Non-responsive content removed until 01.19.09

(from Bosch warranty system)

GE	Customer complaint	QC no.	QTS no.	Part no.	DM	CS	Failure D.	Mileage [km]	VIN	Error text	OSA
CP4.1	B Rail pressure not OK	230001917421	2864439	0445010507	9/17/2007	12/11/2007	1/4/2008	350	8K48A003378	intake valve leaking	1533
	B Veh. will not start.	230002070696	2974476	0445010507	1/11/2008	3/26/2008	3/26/2008	25	8K48N006273	Pump drivetrain damage	1623
	B Engine will not start.	230002158348	3051740	0445010507	3/15/2008	4/4/2008	4/24/2008	814	8K58A037278	Pump drivetrain damage	without
	B Electrical faults	230002177333	3070039	0445010507	3/15/2008	5/6/2008	7/4/2008	4682	8K68A039265	Pump drivetrain damage	without
	B Preheat light is lit up, vehicle stopped	230002125197	3016558	0445010507	3/12/2008	4/17/2008	5/5/2008	1584	8K18A035821	tappet spring is broken	1635
	B Mechanical fault	230001930606	2875958	0445010507	10/5/2007	12/6/2007	12/13/2007	365	8K08A002485	MU O-ring sheared off	1535
	B leaking	230001992667	2943041	0445010507	11/18/2007	1/15/2008	3/12/2008	6793	8K69A000578	MU O-ring sheared off	1620
	C Engine has stopped and does not restart	230002225640	3118777	0445010507	2/29/2008	4/16/2008	7/28/2008	20422	8K88N022279	Not OK Fuel	1738
	S Breakdown will not start.	230002139769	3031672	0445010507	11/5/2007	2/8/2008	5/27/2008	4057	8KX8N002048	OK - Original not submitted	1647
	O Generator control lights up sporadically	230002283240	3179166	0445010507	4/30/2008	6/23/2008	10/8/2008	17355	8K19A033066		without
GE	Customer complaint	QC no.	QTS no.	Part no.	DM	CS	Failure D.	Mileage [km]	VIN	Error text	OSA
CRI3.2	B Engine stopped while driving	230002250477	3146228	0445116030	7/4/2008	8/15/2008	9/9/2008	2202	8K49A068667	Particles in the return pipe	1725
	B Engine stopped while driving	230002297332	3205241	0445116030	4/23/2008	10/16/2008	10/18/2008	1500	8K39A019637	Particles in the return pipe	without
	C Connecting rod broken	230001941819	2906283	0445116030	1/3/2008	1/23/2008	1/23/2008	28	8K28A002522	Engine failure, injector damaged	1555
	C Veh. will not start.	230002043566	2961515	0445116030	1/10/2008	3/26/2008	3/26/2008	25	8K48N006273	Foreign objects from the outside	1623
	C Veh. will not start.	230002043567	2961515	0445116030	1/10/2008	3/26/2008	3/26/2008	25	8K48N006273	Foreign objects from the outside	1623
	C Veh. will not start.	230002070697	2961515	0445116030	1/10/2008	3/26/2008	3/26/2008	25	8K48N006273	Foreign objects from the outside	1623
	C Veh. will not start.	230002070698	2961515	0445116030	1/10/2008	3/26/2008	3/26/2008	25	8K48N006273	Foreign objects from the outside	1623
	C Spray pattern not OK 1 hole clogged	230002216497	3088144	0445116030	3/19/2008	5/6/2008	7/1/2008	4739	8K69A006042	Particles in the nozzle spray hole	without
	S Engine irregular when idling	230002156418	3046621	0445116030	12/1/2007	1/28/2008	4/1/2008	8552	8K58N004256	OK according to specification	without
	S Engine stopped while driving	230002250476	3146228	0445116030	7/4/2008	8/15/2008	9/9/2008	2202	8K49A068667	OK according to specification	1725
	S Engine stopped while driving	230002250482	3146228	0445116030	7/4/2008	8/15/2008	9/9/2008	2202	8K49A068667	OK according to specification	1725
	S Engine stopped while driving	230002250483	3146228	0445116030	7/4/2008	8/15/2008	9/9/2008	2202	8K49A068667	OK according to specification	1725
	O Vehicle smells of diesel.	230002349569	3240975	0445116030	7/21/2008	5/30/2008	12/22/2008	48969	8K79A012688		without
	GE	Customer complaint	QC no.	QTS no.	Part no.	DM	CS	Failure D.	Mileage [km]	VIN	Error text
EDC17	B Engine hums and stops	230001981754	2935479	0281014235	11/22/2007	1/30/2008	2/19/2008	6	8K58A008962	Short-circuit capacitor	1604
	B Engine has stopped while driving	230002151338	3034801	0281014235	11/23/2007	2/8/2008	5/22/2008	15196	8K48A010962	Foreign object in Q1 adhesive	without
	B Engine stopped while driving.	230002135455	3023186	0281014235	3/4/2008	3/15/2008	4/28/2008	251	8K88A031667	Short-circuit capacitor	1653
	B Vehicle during the freeway driving	230002229377	3120076	0281014592	6/3/2008	7/29/2008	8/26/2008	616	8K99A067546	DC-DC converter is burning down	1712
	C Engine does not start up	230002230861	3126268	0281014235	4/26/2008	7/8/2008	8/20/2008	8570	8K29A017264	Mechanically damaged	without
	S Preheat light is lit up and engine has	230002177332	3067281	0281014235	12/2/2007	1/17/2008	6/6/2008	27028	8K88A011077	OK according to specification	without
	S Exhaust control is lit up	230002197321	3078324	0281014235	4/3/2008	5/21/2008	6/27/2008	6011	8K69A007708	OK according to specification	without
	S Vehicle has no power.	230002242395	3133937	0281014235	11/19/2007	1/10/2008	9/2/2008	45729	8K98A008592	OK according to specification	without
	S Engine no longer starts	230002300707	0	0281014592	8/13/2008	9/10/2008	10/30/2008	1440	8K19N021959	CU OK (cable harness pin)	1788
	O Electrical faults	230002342492	3237051	0281014235	3/7/2008	4/1/2008	10/27/2008	17392	8KX8033453		without
	O Starter turns only when the ignition stops	230002347436	3240693	0281014235	4/29/2008	6/16/2008	11/28/2008	9871	8K69A021088		without

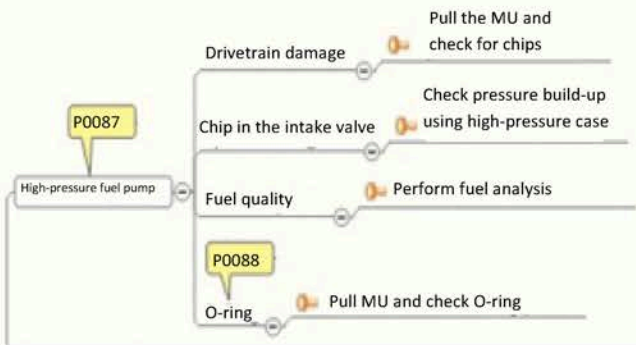
4 Diesel Systems



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FCT Review VW/AUDI 2.0L TDI

VW / AUDI error overview

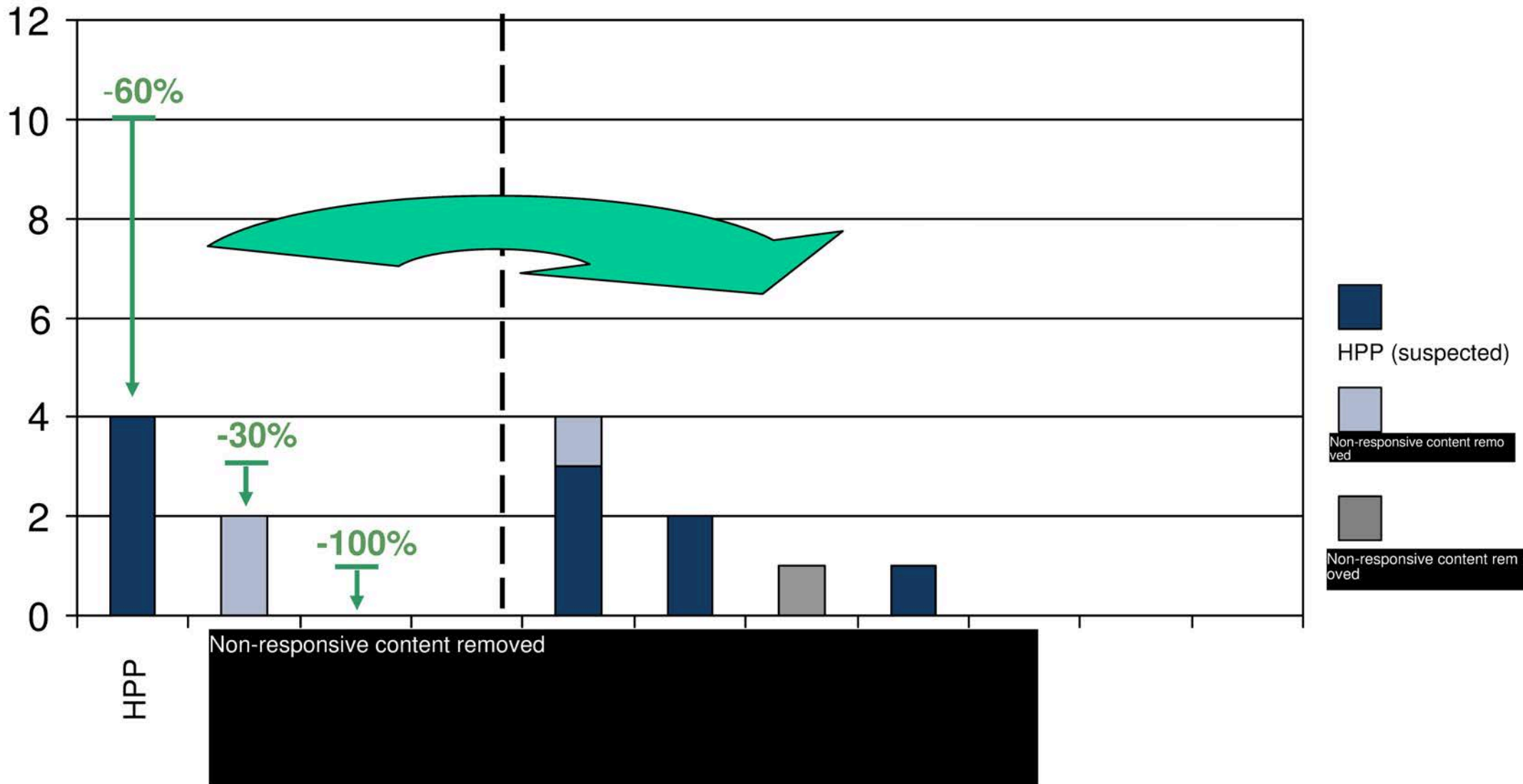


P Code List

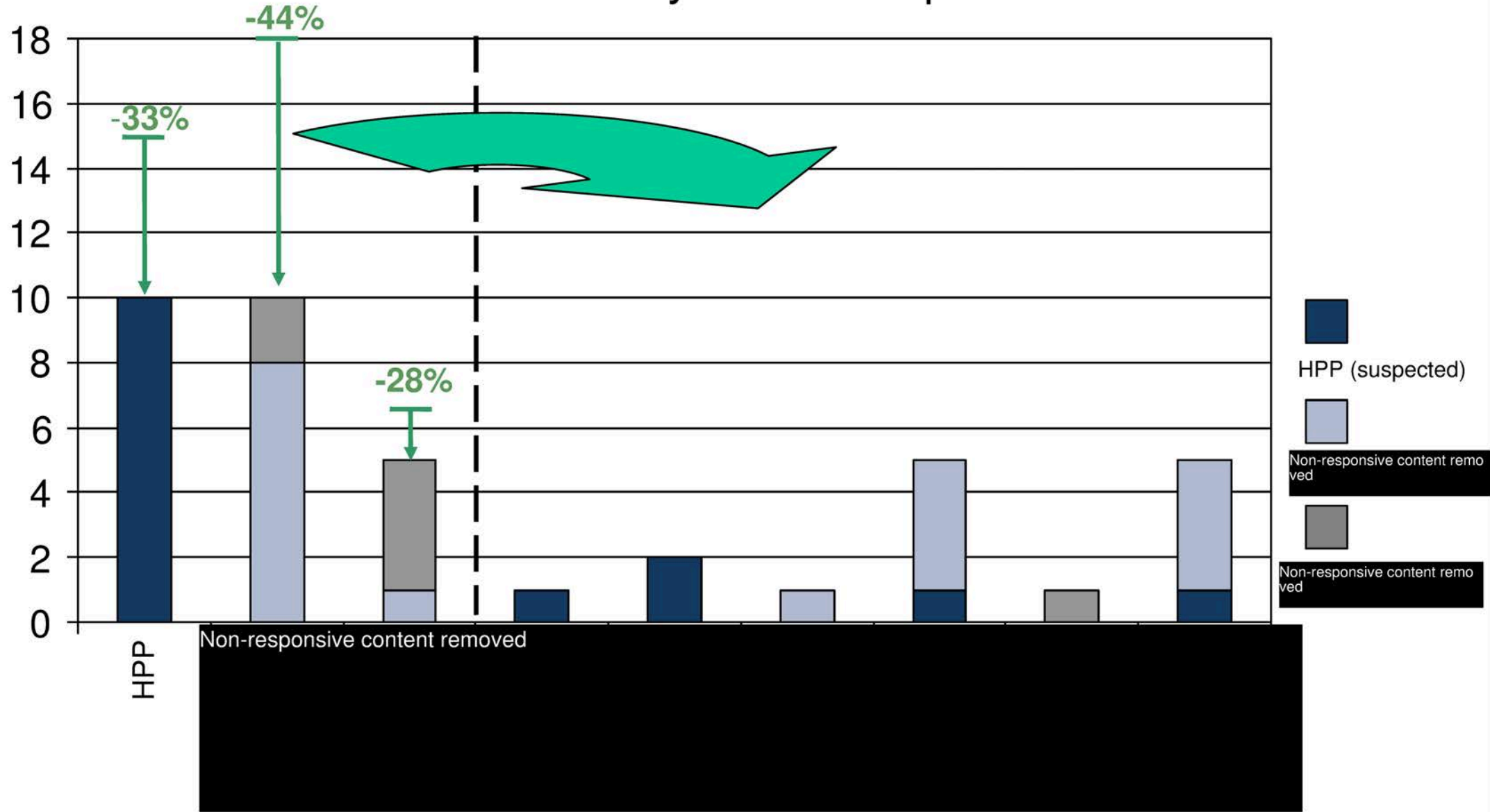
- P0087, 0088** Fuel rail / system pressure; too low – too high
- P0192, P0193** fuel pressure sensor G247, short-circuit to **positive** - to **ground**
- P2149**, supply to injector valve(s) B interruption,
- P020x**, injection valve cylinder x, electric fault in the circuit
- P0299** boost-pressure control, fallen below control limit
- P0302** cylinder. 2 misfiring detected



VW - causes determined by FCT



AUDI - causes determined by Field Competence Team



Conclusions

- Very good cooperation between VW and AUDI.
 - Open communication with TSC, I / GS and dealers.
 - A Common on-site processing of cases.
- Fast response time from WS report up to on-site operation.
- The agreed procedures have proven in the previous project period.
- What is striking is the S-error rate, i.e. cases where the replaced component corresponds to the specification (slides 3 and 4).
However, the cooperation between service, partner operations and Bosch-FCT did significantly reduce the potential S-error.
- The intensive cooperation led to important findings and conclusions for VW / AUDI and RB, especially for the guided troubleshooting.



Identified measures VW / Audi

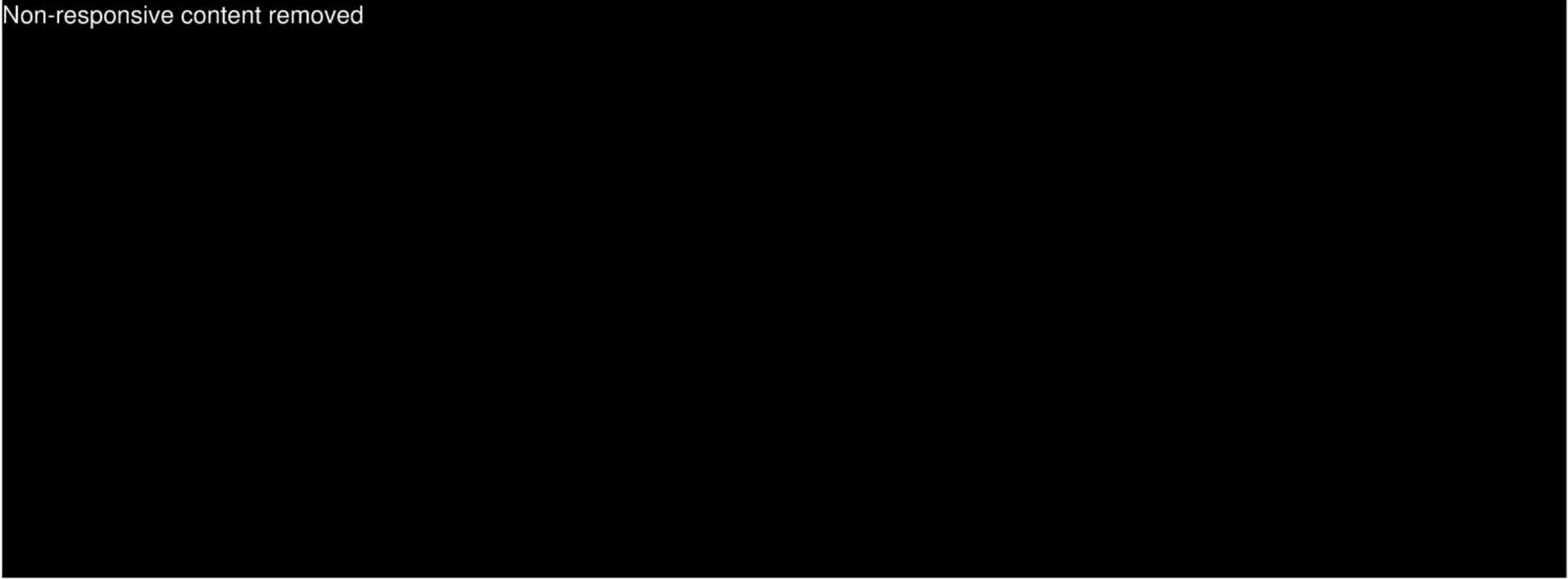
No	Measure	implement
1	Introduction of low-pressure test *	✓
2	Use of injector return line volumetric measurements with PRV adapter *	
3	Use of high-pressure cases *	
4	Pragmatic solutions for localizing faults in drivetrain damage (pull MU)	✓
5	Suggestions for improving the GFF by Field Competence Team	✓
6	Inclusion of electric faults in the GFF and mechanical faults in the repair manual. Guidelines for a uniform system	
7	Combination of rail pressure P-code and fault path for component demarcation *	
8	Adapt selection of displayed ambient conditions to P code *	
9	Illustrate rail pressure data uniformly in the tester (<i>target = hPa and actual = kPa</i>).	

* Backup slides



Outlook: New Projects

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Proposals for future cooperation:

- extension of mandatory reporting of specific components
- Exchange of information on changes in the GFF



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Feuerbach

06.08.2009

No. 2009_19

Minutes

Recipient Participant

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Invited by

Participants

Line

Minutes

Organiz.

Date / location **4.2.2009, 12:30 - 2:30 PM**

Topic **Review of field start-up support by the Bosch Field Competence Team (FCT)**

1. Overview of Mission Field Competence Team
see Appendix
2. Discussion of the FCT operations and results
In the VW field failures, 4 cases with replaced high-pressure fuel pump CP4.1 and 1 case for the injector CRI3.2 have been noticed, wherein the informed and no malfunction has been confirmed in the analysis of the in the Bosch analysis center. Justification by VW: The on-field complaints are not covered by the VW obligation to report. The VW partner workshop can therefore independently component replacement. An extension of the mandatory reporting current vehicle models is not intended.
Note VW: The VW partner company will not be re-debited for the replaced when the guided troubleshooting (GFF) has recommended the component replacement, but a detailed investigation of the component at Bosch does not confirm any errors.



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6/8/2009

No. 2009_19

Minutes

Review of on-field support by the Bosch Field Competence Team (FCT)

Comment Audi: With eight on-site operations, less FCT support was unexpectedly required by Audi. However, on-site analysis was no longer required during detection of chips in the fuel system after the first cases. The processing time between failure date / FCT use at VW/Audi partner company and completion of the component analysis in the Bosch analysis center is high. An evaluation of the processing time will be created to find the cause.

3. Possible improvement measures (see Attachment slide # 9)

- Pcode assignment to fault diagnosis paths of engine control unit: Identical Pcodes are partly used for different fault diagnosis paths (example P0087, rail pressure too low). By distinguishing the different fault paths, it could be distinguished better between the different root causes in Service. ⇒ Under review by persons in charge of the application.
- Improvements in guided troubleshooting (GFF)
The GFF will be optimized cyclically in a GFF team (personnel from Audi and VW) and supplemented.
Check whether employees from VW commercial vehicles can participate in the GFF team.
Bosch FCT can give information on possible improvements based on specific cases of support. For further support, a request should be submitted by Sales to the responsible Development Department [REDACTED].
- The feasibility of the suggestions for improvement of the [REDACTED] which have not been implemented previously is to be assessed jointly by VW and Audi.
- Establishment of a central VW office, from where information on Field Competence Team operations come in a pooled manner and via which feedback is made.
- Check how the knowhow transfer of experience from the FCT operations to the residents of the VW / Audi engine plants is possible. In particular, the knowhow transfer of the residents among themselves should also be ensured, for example in job rotation.
- Bosch FCT offers support even for preproduction and verification vehicles. VW / Audi test feasibility.
- The FCT at DS supports primary cases in the German market. In other markets, there is the possibility to receive support

R: [REDACTED]

D: WK26/09

R: [REDACTED]

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D: WK26/09

R: [REDACTED]

guided troubleshooting team

R: [REDACTED]

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Feuerbach

6/8/2009

No. 2009_19

Minutes

Review of on-field support by the Bosch Field Competence Team (FCT)

from the regional companies (e.g. for SCR in the US market) in case of on-field problems. There is already an exchange of information between the FCT and the regional companies.

4. Further cooperation

VW, Audi and Bosch assess the start-up support from FCT as being very positive. Possible structural improvements are cited under 3. Therefore, further collaboration in future projects is desired. For the following projects / market launches, support by FCT is planned:

- Start-up of the R4 2.0 l engine Gen2 (CRI3.2 and sleeve) in commercial vehicles (e.g. T5) from about WK31/2009. At VW on-field support is not provided by the TSC, but by the VW Commercial Vehicles Service Center (NSC). Bosch asks VW to pass on the experience gathered in the previous R4 start-ups by the TSC to the NSC team.
- Startup of SCR system on the German market. (Support in the North American market is provided by the regional company).
- Start-up of CRI2.5 in the R4 unit after about WK43/2009

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D: WK26/09

CP4 robustness

Agenda

Technical Specifications for passenger cars	P. 2
Technical Specifications Development MD - & OHW	P. 3
Approved fuels (fuel properties)	P. 4
What does "Rest of World" fuel mean	P. 5
Comparison of drive concepts	P. 6
Anti-wear package (HFRR, viscosity)	P. 7,8



CP4 robustness

Main characteristics of CP4 for car applications

Rail pressure	2000bar
Piston diameter / stroke	6.5mm / 6.75mm*
*New piston stroke stages: (6 / 6.5 / 7)mm	
Fuels	without AWP: EN590 with AWP: US fuels with
service life of	300,000 km
Fuel inlet temperature of	70°C



CP4 robustness

Development of main characteristics of CP4 for MD & OHW

Rail pressure MD / OHW	2,500 bar / 2,000 bar
piston diameter / stroke	6.5mm / 7.5mm
Fuels	with AWP: US fuels
with service life MD / OHW	750,000 km / 10,000 h
and fuel inlet temperature of	80°C

Development focus: Robustness increase of drivetrain (P. 7,8)



Robustness CP 4**Approval for the following fuels****without AWP:** EN590**with AWP:** ASTM 975-05 (US fuels with HFRR 520 μ m)**Approval verified by testing****@ R.B. with EN590 / GDK570**

- | | |
|--------------|---|
| 1) Lubricity | 460 μ m / 570 μ m |
| 2) Viscosity | 2.5mm ² /s / 1.9mm ² /s |

Random trials with GDK650, kerosene, gasoline, water, particles.

@ Customer: Verification in target market with country-specific fuel

Robustness CP 4

Approval for **Rest of World (RoW)** fuels

What do "RoW" fuels refer to?

- 1) Low lubricity
- 2) Low viscosity
- 3) High particle contamination, high water content, low proportion of additives

For 1 & 2) robustness measures, see pages 7, 8

For 3) particle and water limits (similar to EN590 / ASTM 975-05) should be ensured by filter or water separator.



Robustness CP 4**Comparison of pump drive concepts for RoW use**

Drive concept	lubricity	Viscosity
Eccentric drive (CP3, CP1H, competitors)	--	+
Roller cam drive (CP4)	+	0

Roller cam drive has the greater potential @ RoW applications



Robustness CP 4

Increase robustness of drivetrain (anti-wear package)

1) Compared to fuels with poor lubricity

(= robustness increase compared to mixed friction)

1a) Improved roller support surface

In CP22 / 2 for W37 implemented through use of advanced C3 coating.

1b) Optimized tappet assembly

Pressing & friction-optimized tappet implemented for W36 & W37; series implementation possible upon customer approval.

1c) C coated high-pressure piston

In series production for W19 Bin5; implementation in series possible upon customer request.

1a) and 1b) are verified in the platform CP4 MD, OHW & CP4 car 22 / x.



CP4 robustness

Increase robustness of drivetrain (anti-wear package)

2) Compared to low-viscosity fuels

(= robustness increase of lubricating film (hydrodynamics) -> reduction in mixed friction content)

Lubricating film thickness_roller_RS = f (fuel, contamination, surfaces, component tolerances)

2a) Optimized roller (surface coefficients)

Parts of potential implemented by commissioning supplier 2 quality.

2b) Optimized roller support surface

In CP22 / 2 for W37 implemented through use of advanced C3 coating.

2c) Optimized component tolerances (clearances)

Is considered as part of CP4 platform development.

2a) and 2b) are verified in the platform CP4 MD, OHW & CP4 car 22 / x.



CP4 - strainer at intake valve**Status****1. Preferred solution: Single piece plastic strainer**

→ Premise: Uniform 100% switchover of the external contour of the IV plates from "cylindrical" to "stepped" for all customers (including customers who do not get a strainer and CP4.2)

2. Postponed: 2-piece plastic strainer

→ No change to the IV plate

→ Risks: Pressing (scraping of chips during assembly)



CP4 - strainer at intake valve



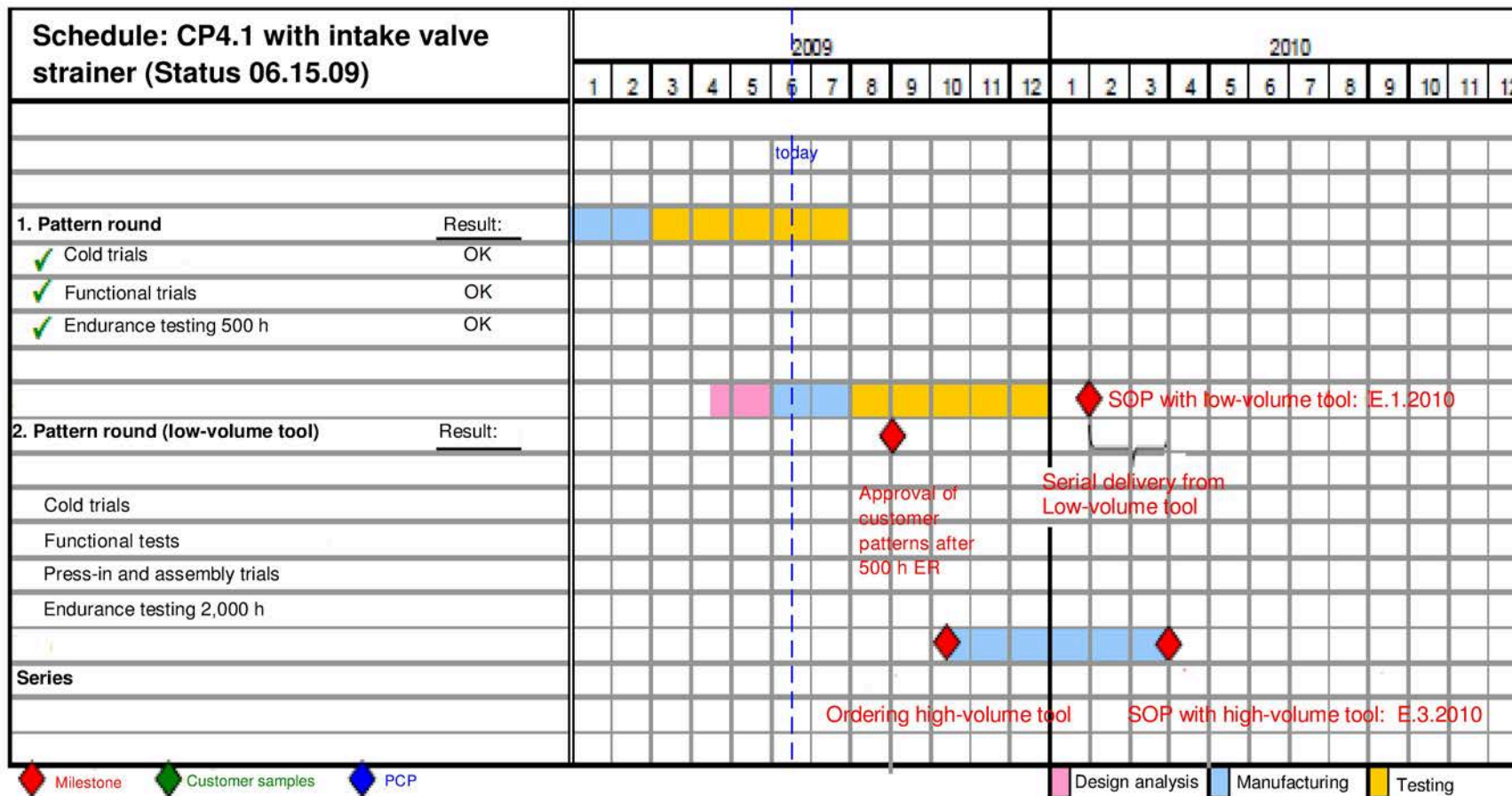
	1. Single piece plastic	2. Double piece plastic
Version		
Trial	<ul style="list-style-type: none"> - Basic trial of mesh size 100 µm OK. - Firm seat after ER / DT open - Cold trials and durability open - Press-in procedure 	<ul style="list-style-type: none"> - Basic trial of mesh size 100 µm OK. - Firm seat after ER / DT open - Cold trials and durability open - Press-in procedure
Remark	Preferred solution since 05.18.2009	Preferred solution up to 05.18.2009



CP4 - strainer at intake valve



Schedule





Diesel systems

From | Persons responsible | Phone | Fax

Feuerbach
October 23, 2009
No. 990158

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Protocol

Recipient Non-responsive content removed
Currently
Invited
Audi partici
Line
Protocol
Organis.

Date/location **October 21,2009 2:00 PM - Audi N** Non-responsive content removed

Topic **Technical meeting r.e. high-pressure fuel pump CP
Special topic - robustness CP4/water separation**

1. Use of CRS in trest of world (RoW)

On account of returns from various markets, Audi is unsure about the use of the CP4 worldwide. Audi's Quality Assurance is not prepared to approve further use of the CP4 if the failure situation does not improve.

The technical discussion r.e. the CP4 at this agreed date.

Further meetings Audi/Bosch with top level on October 27, 2009 in Non-responsive content removed

and together with VW on December 08, 2009 in Non-responsive content removed

2. Slides robustness of the CP4

See attachment

Malfunctions as a result of poor lubricity / viscosity / water were detected by Bosch on the CP4 and the CP3/CP1H - irrespective of the drive concept. Bosch considers the drive concept of the CP4 to be superior to that of the CP1H - CP3 drive concepts.

There is always a dependence on fuels which could present a risk, depending on the country and time of year.

Customer sample can be ordered with anti-wear package from February 2010 (see slide 24). *Note: The price of the anti-wear package option is established based on the ERs in 2010.*

A vehicle validation (see slide 25) is necessary for the approval in the target markets/target clusters and it would be practical for this to be carried out



Diesel systems

From	Persons responsible	Phone	Fax
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Feuerbach

October 23, 2009
no. 990158

Protocol

Technical discussion r.e. high-pressure fuel pump CP
robustness of the CP4/water separation

using borderline parts, as average pumps cannot be used due to the wide safety reserve.

3. Water separator (talk by Audi N/EA912 M Non-responsive content removed)

In the laboratory test, the fuel filters with water separators currently being used by Audi comply with the Bosch TCD.

In the vehicle (random sample), manually introduced water is partially dissolved again in the fuel flow. A remedy would be e.g. a "water trap", i.e. deflector for the separated water and separation from the fuel flow.

Tests were carried out with UIP, CP1H with GP & CP3.3 with GP. Bosch believes that the results cannot be transferred to CP4 with EFP, as the filter is run through much more often.

The current standard for the measurement of the degree of water separation is currently being revised, the new ISO16332 (new draft prov. E.2009) will take into consideration innovations with regard to the proportion of biodiesel, desulphurised fuel etc.. Bosch will draw upon this ISO for the fuel properties in the forthcoming TCD.

Audi has requested a representation of the changes - new/old TCD

Audi will clarify the further procedure internally.

4. Rail pressure deviation after cold start with B10

Audi has repeatedly established that with a cold start of a Q5 technology demonstration vehicle with fuel B10, the flow volume of the CP with a cold start reduces on the CFPP of the fuel and rail pressure deviation is detected. The hypothesis is the clogging of the MU filter with the paraffin flakes in the pipe volume after the fuel filter up to the CP.

The current Audi requirements on the cold start have not been achieved in this test.

Audi will draw up an internal fuel road map with the possible procedures. Bosch was asked to prepare a topic for the next TM (within the scope of CRI TM or CP TM or special meeting)

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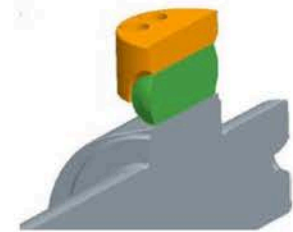
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CP4 robustness

Influence of fuel quality

Low lubricity (kerosene, water,...)

- Leads to increased wear in the roller / roller support combination in the start case (mixed friction area)



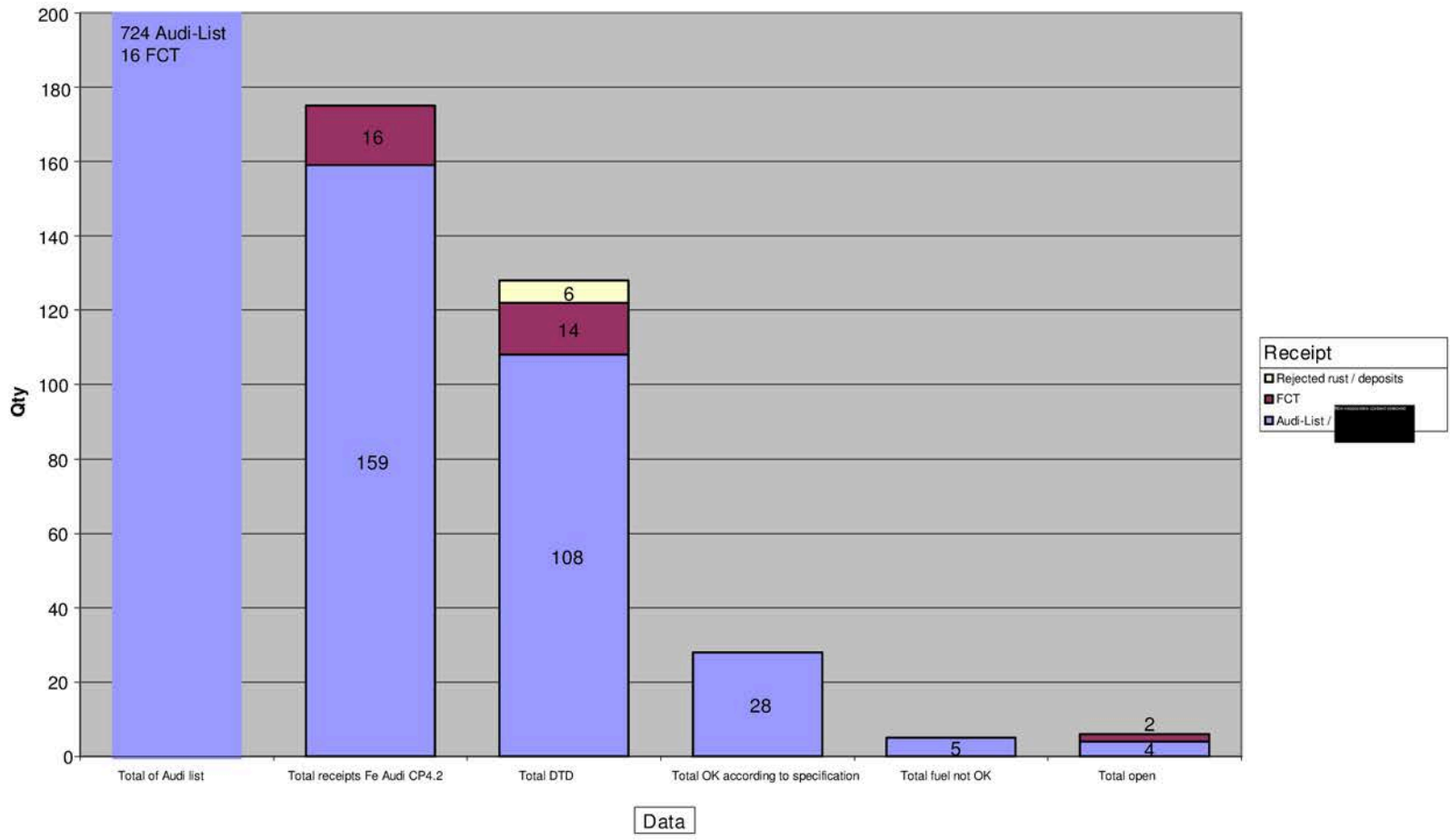
Less viscosity (kerosene, Non-responsive content removed diesel, water,...)

- Leads to low lubrication film thickness -> increased friction due to component contact
-> Increase in slip (idle status of roller)

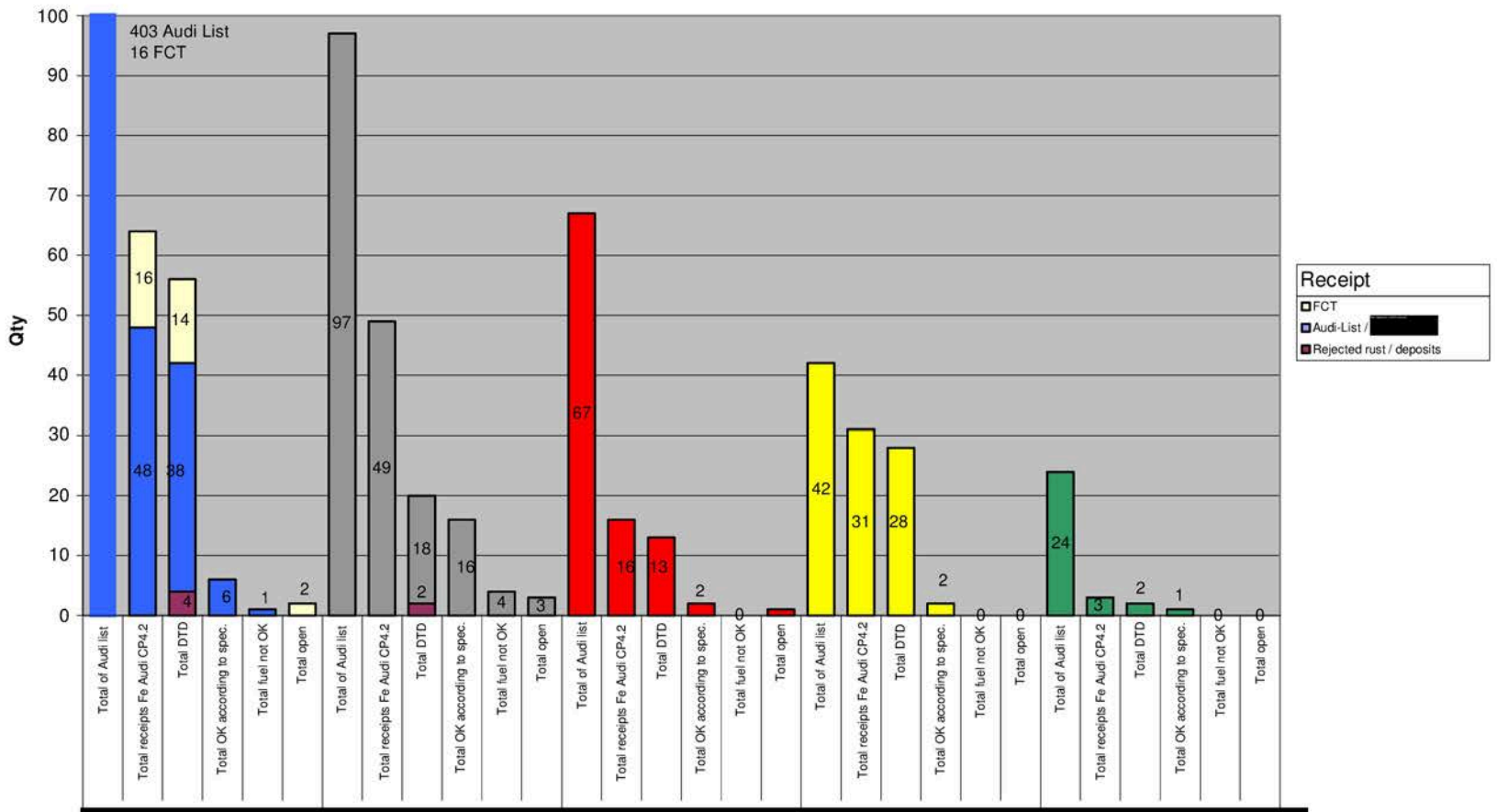
Water in fuel

- Influence as an emulsion, see lubricity and viscosity
- Free water can lead to hydrogen wear / corrosion fatigue and thereby damage the parts in rolling contact

TOP5 countries - All



TOP5 countries



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Country data



Summary

→ Status of new information since last update on 12/10/09:

Other analyses in the fuel samples from on-site actions in [redacted] support the results from the fuel survey in Northern Italy and the analyses from the problematic pumps. Further detailed analysis of the fuel samples and fuel filters will be complete by 1/22/10.

Information gathered to date supports the failure mechanisms presented in the last report.

- 1. Tribochemical wear
- 2. Deposit / coatings from algae and oxidation products and therefore a significant deterioration in frictional coefficient.
- 3. Corrosion on the surface of cams and roller

The analysis of the reference samples from the problematic production period indicates nothing unusual in relation to drawing-related features. Other detailed analyses (roller surface texture, ripple in roller support, roundness with Fourier analysis, local adhesion of coating with temperature analysis) will be completed by 01/20/10.

Summary

→ Further action:

For the purpose of practically confirming the damage hypotheses, reappear tests will be carried out on the hydraulic test bench with boundary sample parts and fuels from 1/14/10 onwards. A test schedule has been drawn up.

Measures to increase robustness (roller surface texture, roller support and play) are defined and their effectiveness will be verified with the same test parameters. A test schedule has been drawn up, partial results will be available by the end of week 01/2010

Return of the requested 40 good pumps from [redacted] and 20 good pumps [redacted] is agreed to WK 03/2010.

Mechanism whereby the tappet is turned, roller lifted from the camshaft depending on the engine vibrations on the pump drive, is to be examined on the engine with AUDI. Technical meeting for this purpose 01/12/2010

Operating conditions / Environment / System

Local FCT team in Non-responsive content removed

Status: 18 vehicles examined on-site and 4 systems received from damaged parts stores. Complete fuel injection systems including fuel filters and fuel pumps have been sent to Bosch for analysis.

Result: 12/12 cases of drivetrain damage from local actions.
2/4 cases of drivetrain damage from damaged parts stores systems.
7/7 analyses of low pressure circuits showed nothing unusual.

Special features: In 3 vehicles, free water (>> 200 ppm) found in fuel.
4 vehicles with deposits in the tank (swirl pot)

- 1x reddish, sticky coatings,
- 1x white flocculation,
- 2x dark/ black particles



Fuels Findings

Status: 20 fuel samples analyzed from survey.
10 fuel samples analyzed from FCT.

Result: **Survey:**
Oxidation stability was found to be outside the tolerance in 4 fuel samples and the TAN (acid coefficient) is generally 2-3 times higher than usual, probably due to spilled biodiesel.

FCT:
No striking features identified in 8 fuel samples, in 2 fuel samples oxidation stability was outside the tolerance. In the first analysis of the coatings, algae were found in the fuel. Other deposits from other pumps are under analysis and probably also contain algae. Fuels containing microorganisms always contain free water. This is also consistent with the slight acidification of another fuel sample from the same damage scenario. Algae develop acids as metabolized material.



Summary of analysis results

Result of analysis of [REDACTED] pumps

17 out of 17 Bruss shaft seals more worn than known from trial

45 out of 54 pumps have signs of corrosion

11 out of 54 pumps have brown fuel deposits

45 out of 52 drivetrain failures have turned tappet bodies

22 out of 54 pumps have surface smoothing on the cam

9 out of 52 drivetrain failures have fatigue damage on the cam

3 out of 54 pumps have pitting on the cam

44 out of 103 roller supports are worn in the middle

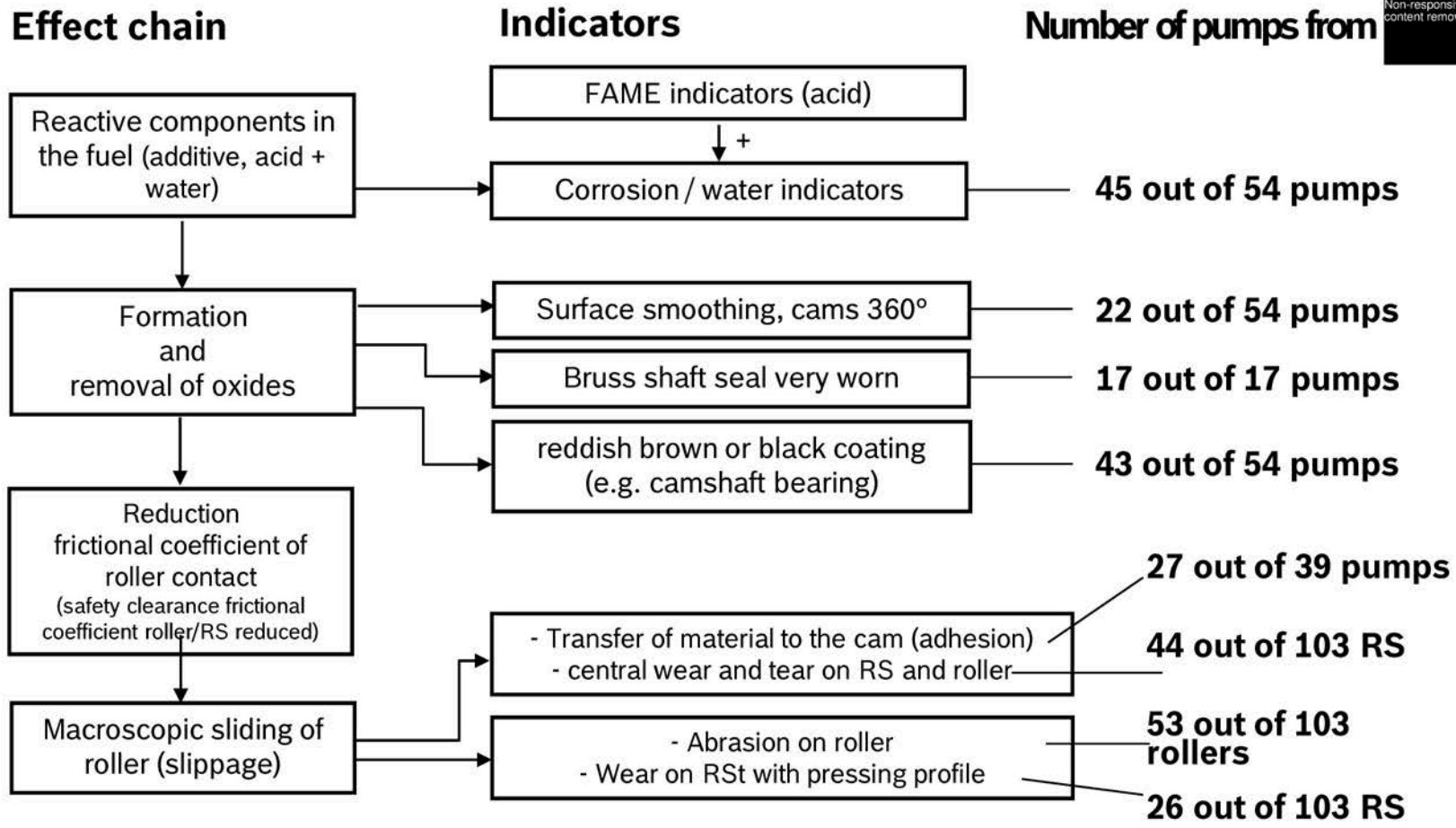
29 out of 103 roller supports are completely worn

26 out of 103 roller supports are worn in the shape of the press profile

1 x fuel sample tank: Algae

1 x wash mark with striations

Failure hypothesis 4: Fuel additives -> Tribochemicals



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Failure hypothesis 6: Fuel viscosity -> Boundary friction

Effect chain

Fuel additives reduce viscosity e.g. water, additives

Threshold value components

Boundary friction Floating/ rolling contact

Sluggish roller Roller slippage

Indicators

Water indicators

Bruss shaft seal very worn

Sink marks in Kaco camshaft seal

Roller texture

RS C coating

RS texture

RS straightness

Number of pumps from

45 out of 54 pumps

17 out of 17 pumps

8 out of 54 pumps

3 out of 54 pumps

27 out of 39 pumps

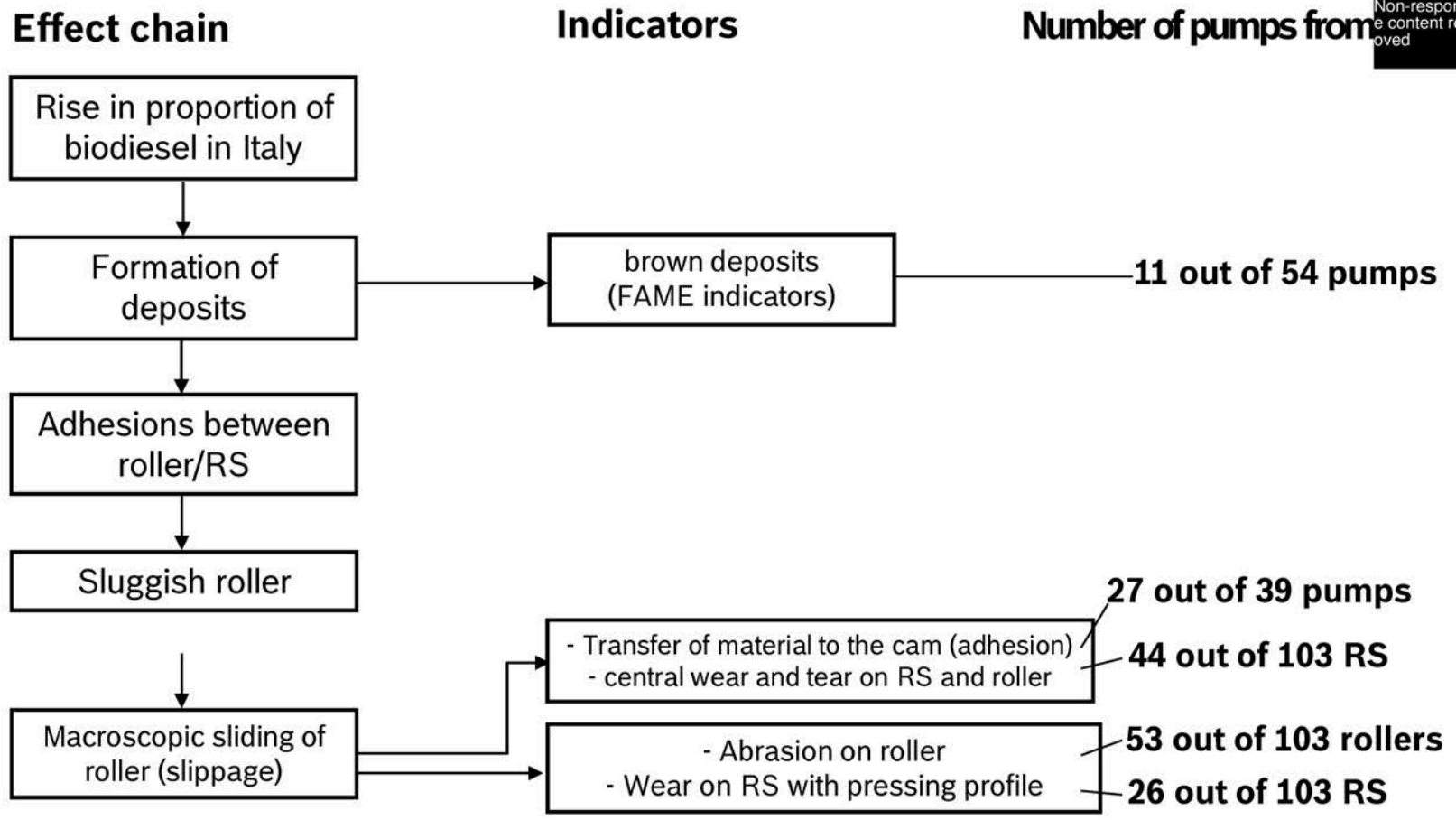
44 out of 103 RS

53 out of 103 rollers

26 out of 103 RS

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Failure hypothesis 3: Biodiesel -> adhesions



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Operating conditions / Environment / System

Procure 40 good pumps

Status: Vehicles identified, importer to contact owners. Importer has new pumps for replacement.

Result: t.b.d.

Further action: First returns not expected before WK 03/2010.

Special features: none



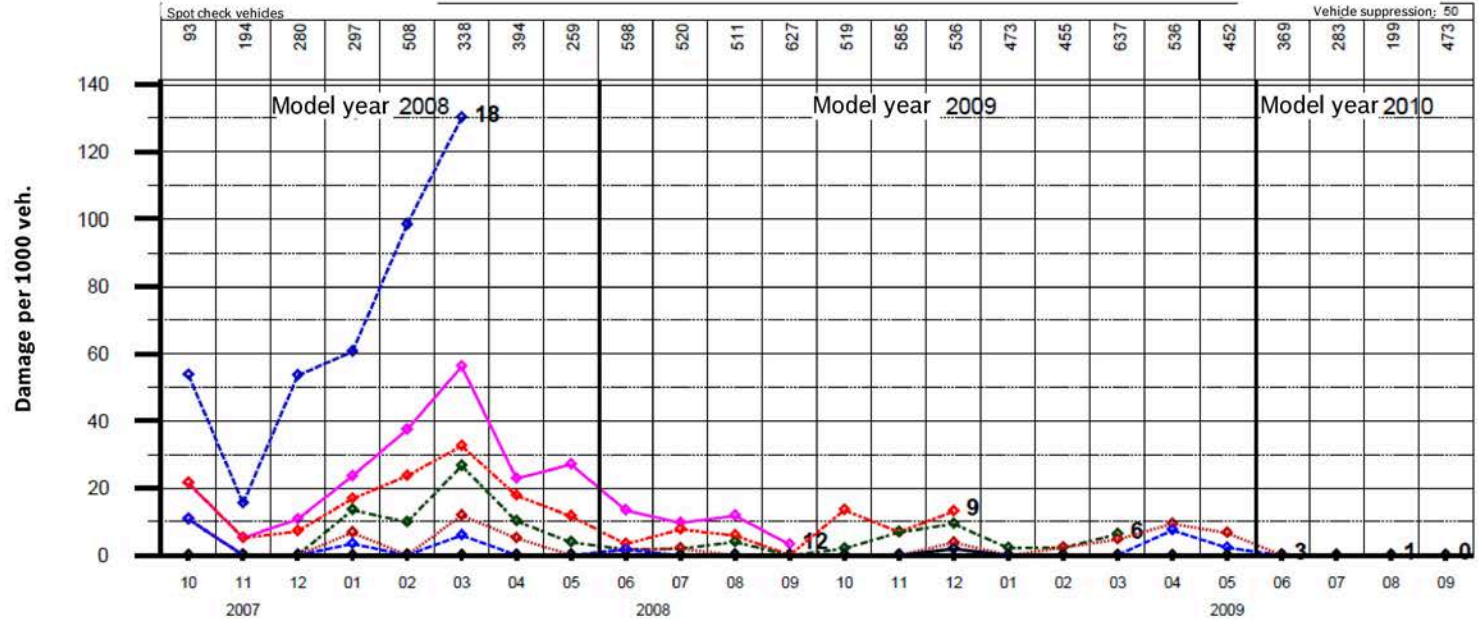
AQUA: Active quality analysis
 Status: 10/09-20.11.09 09:14
 Source/user: SAGA-Gew

Audi, market:

Confidential
 without PR numbers
 CNR 2374

MY 2008 - 2010, Offset: all (max. 2)
 CNR / Groups: High-pressure fuel pump

MY	MIS 0	MIS 1	MIS 3	MIS 6	MIS 9	MIS 12	MIS 18	MY Replacement	BD	SA 17	SA 10	SA 50	SA 18
2008	0,0	1,7	3,9	10,3	18,0	27,8	77,3	100,0 %	81,1 %	14,6 %	75 %	7,1 %	2,4 %
2009	0,2	1,1	2,2	4,4	7,5	13,7		96,3 %	86,3 %	13,8 %	80 %	3,8 %	1,3 %
2010	0,0	0,0	4,9					100,0 %	100,0 %	66,7 %	33,3 %		
Diff%	-100	-100	121,12										



Vehicles: : 3.389+9.366+4.312=17.067; Sold: 3.386+9.211+2.973=15.570; UP : 2.335+6.347+2.249=10.931 MY:2008+2009+2010 = Total

CP4 A4,A5,Q5,Q7 V6

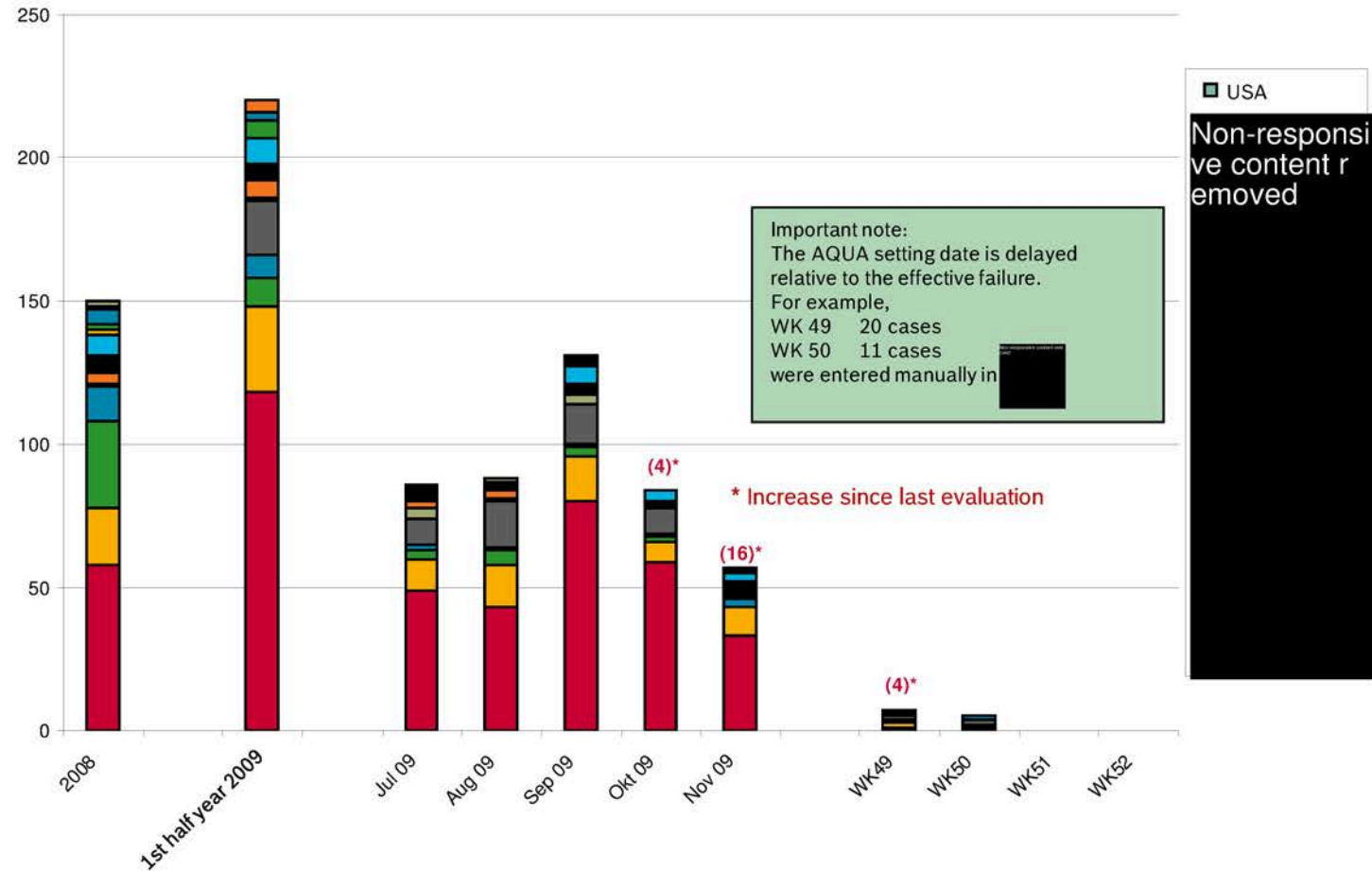
Diesel Systems

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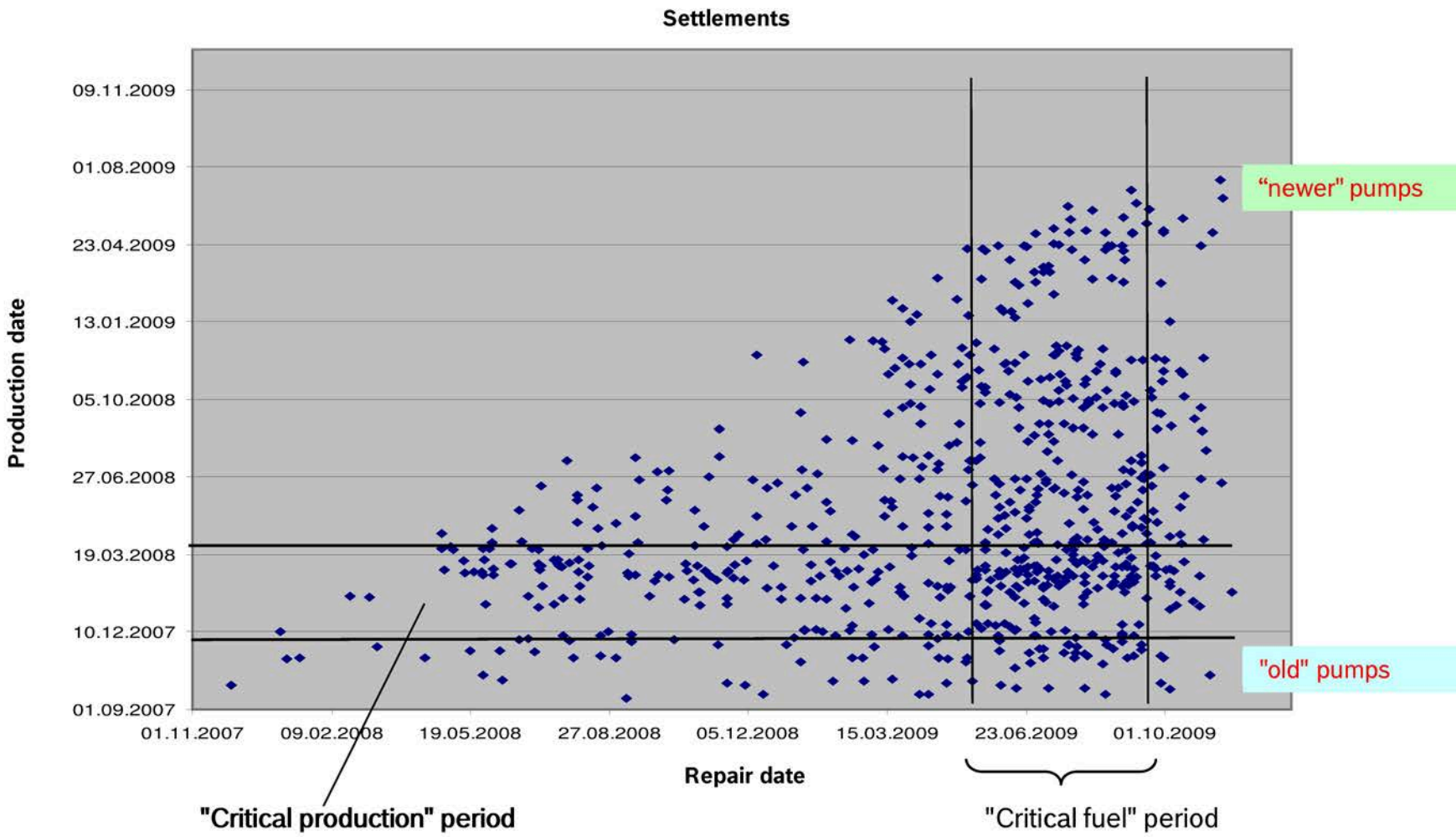
BOSCH

Settlements high-pressure fuel pump CP4.2 V6-TDI Audi (by setting date in AQUA)



Diesel Systems





Task force summary

→ Status of new information since last update on 1/20/2010 (changes in blue):

Task force work concentrates on the following key areas:

1. Analysis of field parts/fuel samples, good pumps, filtering, reserve samples from production.
2. Analysis of the differences between CP4.1 and CP4.2 in the case of critical fuels.
3. Reappear test of the differences between CP4.1 and CP4.2 and confirmation of the damage mechanisms.
4. Introduction of anti-wear package 1 (C2 coating, reduced play on roller/roller support, 100% avoidance of fusing and metal spatter)
Implementation decision by RB/AUDI after positive completion of validation
Start of WK 9/2010
5. Definition of anti-wear package 2 (RoW use) after completion of points 1 and 2.
This needs to be checked and validated with boundary fuel (already defined with AUDI).

1. Summary of analysis

- Other analyses in the fuel samples from on-site actions in [redacted] support the results from the fuel survey in Northern [redacted] and the analyses from the problematic pumps. The mineral oil industry in [redacted] confirms in principle the poor fuel results (water, aged biofuel)

The analyses in relation to pumps, fuel samples and particles / residues from local actions are complete. In some cases oxidation stability (aging) was outside the standard; in addition, particles of plastic and traces of algae were found in some tanks and pumps. One of the special features in [redacted] is the use of the **Tunap 183** additive to clean the fuel injection system in service. **According to the manufacturers, Tunap 183 is supposed to improve lubrication (HFRR value). Evaluation of the information by the Bosch and Audi laboratories. Verification of influence through tests run by Bosch.**
Tests concluded in week 8/2010



1. Summary of analysis

→ Return of the requested 40 good pumps from [redacted] and 20 good pumps from [redacted].

First returns announced from [redacted] (5 pumps) and [redacted] (4 pumps). 4 pumps received from Italy on 1/25/2010. Pumps from [redacted] still outstanding.

1 out of 4 pumps has signs of previous damage to the roller/ camshaft in TDC, same results as with 1 pump from returns from on-site action.

Similar damage was found on an as yet still working V12-TDI pump from [redacted] (sister pump of drivetrain damage after 1,600 km), where the roller was at a significant slope on the cam and there were signs of corrosion on the roller.

These signs of damage indicate sluggish rollers in conjunction with poor quality fuel.

Further detailed analysis required, completion by 2/3/2010.

1. Summary of analysis

Information gathered to date supports the failure mechanisms presented in the last report.

- 1. Tribochemical wear
- 2. Deposit / coatings from algae and oxidation products and therefore a significant deterioration in frictional coefficient.
- 3. Corrosion on the surface of cams and roller

Analysis of reference samples:

The analysis of the reference samples from the problematic production period (up to May 2008) indicates nothing unusual in relation to drawing-related features. Other detailed analyses (roller surface texture, ripple in roller support, roundness with Fourier analysis, local adhesion of coating with temperature analysis) are complete.

Analyses to date confirm the production status at the time, with splashes of metal on the roller support; also the surfaces of the C coatings indicate abnormalities that are still under investigation. Will be concluded on a further 25 parts by 2/3/2010.



2. Summary of differences between CP4.1 and CP4.2

- The MIS12 (MY08) failure quota of the CP4.2 is up to 10 times higher in [redacted] than the CP4.1.
- The MIS 12 (MY08) of CP4.2 is approximately 10 times higher in [redacted] than in [redacted]
- The MIS 12 (MY08) of CP4.2 is approximately 2 times higher in [redacted] than in MY09.

Conclusions:

- In addition to the influence of the fuel quality, there must also be design and application-specific differences between CP4.1 and CP4.2.
- Concentration of further work on an analysis of the differences between CP4.1 and CP4.2 (see slide 6 and 7).

2. Summary of differences between CP4.1 and CP4.2

Further action:

Implement examinations

- The flow and pressure conditions in the tappet chamber of both pump types.
Initial investigations of flow conditions indicate now differences.
- Influence of the low pressure circuit.
The plan is to reproduce the entire low pressure circuit of 4/6-cyl. engines on the test bench in order to test individual influences, such as water ingress from the tank to the pump. D. 2/24/2010
- the tappet position when stopping (position of roller with cam TDC)
Initial analysis showed that the tappet position in 6-cylinder engines in approx. 10% of cases can be just before or at TDC after the motor stops. When the engine is restarted the roller must start from the instable position at TDC This could cause the tappet to turn.
In the case of 4-cylinder engines this critical position does not exist, however this is to be confirmed again by VW/AUDI by means of measurement data on the vehicle. D. 2/3/2010

3. Reappear test for differences between CP4.1 and CP4.2

Further action:

Validation with EN590 shows a turned tappet on the camshaft of less than one degree. Further investigations are required on the test bench in relation to the startup of the roller at TDC with critical fuel (Arctic diesel). D. 2/3/2010

Measurements need to be carried out using kerosene on the complete engine at AUDI in Non-responsive content removed in WK 5/2010.

4. Summary of anti-wear package 1.

→ Further action:

Measures to increase robustness (cam roller surface texture, roller support and play) are defined and their effectiveness will be verified with the same test parameters. A test schedule has been drawn up, **partial results** will be available by the **end of WK 8/2010**. The latest information shows that the roughness of the roller support is the decisive parameter in increasing robustness.

According to a simulation, narrowing tolerance R_v from 1.3 to **0.8 μm** increases the safety factor of the frictional coefficient by **approx. 50%**.

Investigations into the creation of roughness in the roller support shows that roughness is primarily determined by the C3 coating and not the processing.



4. Summary of anti-wear package 1.

Roughness measurements on roller supports with C2 coating show a clear improvement in roughness.

Changes in process technology from C3 sputter coating to C2 plasma coating on the roller support and roller enables quality to be improved by avoiding 100% of fusings and metal spatter.

That is why it is necessary to switch to C2 coating.

The basic test with EN590 and GDK 570 for C2 coating is complete.

The "rest of the world" trials are still outstanding.

Further action:

- In case of positive validation of the anti-wear package with boundary samples and critical fuels (Kerosene, Arctic Diesel, WCF, FCF) by the end of WK 8/2010 , a series introduction was decided for pumps V6-TDI EU5 + BIN5 series and W36. Production readiness is assured from week 9/2010 onwards.
- This will confirm the schedule requirements from Audi from the last task force.



4. Summary of anti-wear package 1.

- A further objective is to enable the anti-wear package on a provisional basis in customer service worldwide.
After the anti-wear package is installed in series, the first 400 pumps will be provided for customer service.

