

EA02-025

TEXAS INSTRUMENTS, INC.'S

9/10/03 ATTACHMENT TO ODI

REQUEST #3

BOX 5

PARTS A - P

PART C

PRESSURE SWITCH DATA

FORM 21605

TEST NO. 249-15-76

| | | | |
|------------------------------------|---------------------------|------------------------------|-----------------------|
| DEVICE 7715L3-3 | DATE REQUESTED 9/11/84 | REQUESTED BY Steve Offlow | REQUESTED COMPL. DATE |
| PERFORMED BY Jeffrey D. Baccaro | DATE STARTED 9/2/85 | DATE COMPLETED | APPROVED BY |

PROJECT TITLE: Speed Control Deactivate PS

CUSTOMER:

PURPOSE OF TEST: Next Pass

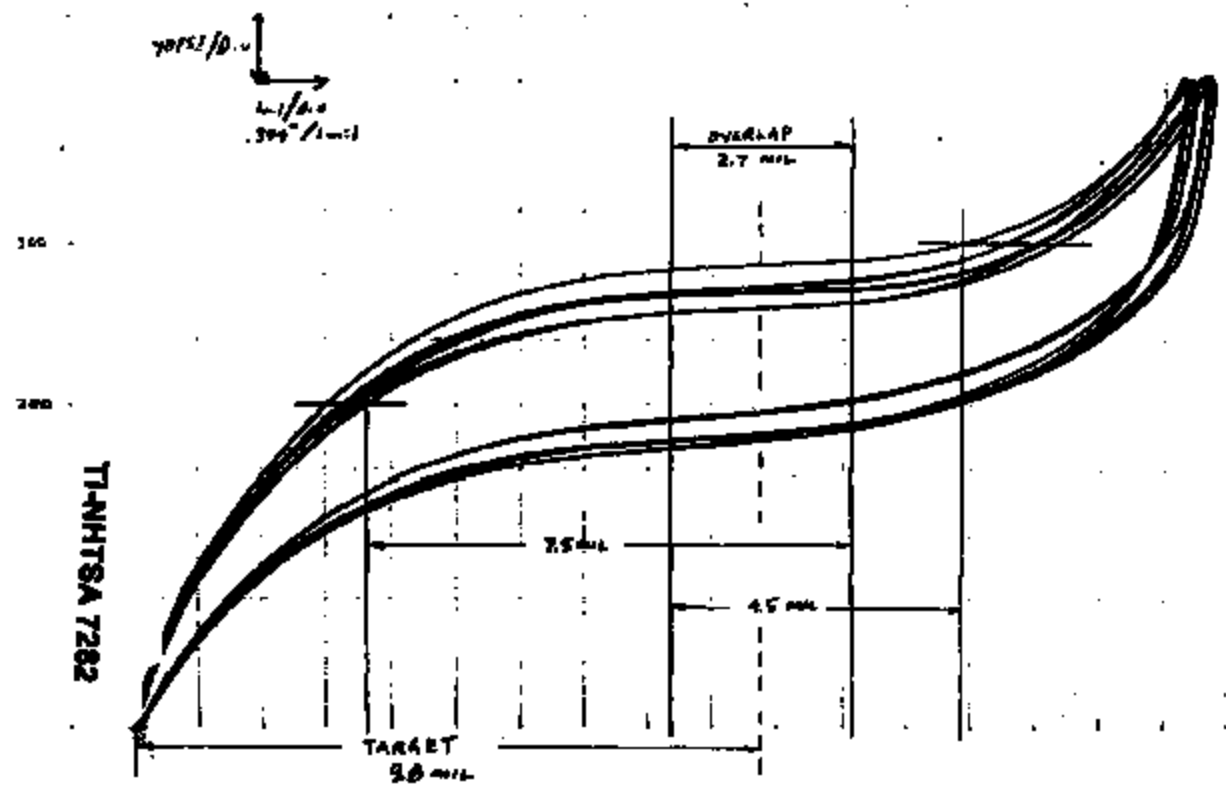
PROCEDURE:

| Device # | RT | | -40 | | +125 | | +150 | | +175 | | Bar dia. | Sump dia. | Pin dia. | offset |
|----------|---------|-----|---------|-----|---------|-----|------|-----|---------|------|----------|-----------|----------|--------|
| | Act | Ref | Act | Ref | Act | Ref | Act | Ref | Act | Ref | | | | |
| 54-15-1 | 250 | 121 | 268 | 151 | 227 | 169 | 178 | 150 | | | | | | |
| - 2 | 249 | 129 | 265 | 151 | 237 | 122 | 223 | 166 | | | | | | |
| - 7 | 226 | 169 | 250 | 143 | 214 | 156 | 199 | 145 | | | | | | |
| - 7 | 236 | 173 | 252 | 159 | 222 | 164 | 202 | 156 | 91.3 | 46.2 | 145.1 | | | |
| - 7 | 232 | 169 | 258 | 159 | 216 | 161 | 206 | 154 | | | | | | |
| - 6 | 223 | 169 | 249 | 159 | 202 | 150 | 188 | 140 | 149-135 | 70.9 | 46.6 | 145.0 | | |
| - 7 | 241 | 166 | 247 | 152 | 209 | 156 | 198 | 143 | | | | | | |
| - 9 | 255 | 181 | 265 | 158 | 232 | 170 | 206 | 158 | | | | | | |
| - 7 | 259 | 127 | 271 | 151 | 232 | 162 | 188 | 138 | | | | | | |
| - 10 | 248 | 132 | 251 | 152 | 206 | 157 | 211 | 161 | | | | | | |
| - 6 | 228 | 131 | 255 | 152 | 211 | 160 | 208 | 156 | | | | | | |
| - 11 | 232 | 120 | 240 | 155 | 216 | 166 | 208 | 159 | | | | | | |
| - 13 | 235 | 168 | 259 | 156 | 215 | 162 | 216 | 148 | 190-137 | 71.4 | 46.9 | 144.8 | | |
| - 17 | 232 | 122 | 249 | 156 | 219 | 172 | 213 | 158 | | | | | | |
| - 15 | 236 | 172 | 253 | 150 | 221 | 169 | 206 | 157 | | | | | | |
| - 4 | 231 | 160 | 240 | 158 | 215 | 165 | 196 | 150 | | | | | | |
| - 17 | 232 | 169 | 258 | 152 | 212 | 166 | 200 | 153 | | | | | | |
| - 19 | 255 | 125 | 271 | 152 | 214 | 169 | 228 | 157 | | | | | | |
| - 15 | 237 | 120 | 256 | 159 | 210 | 161 | 196 | 138 | | | | | | |
| - 21 | 250 | 183 | 268 | 203 | 239 | 128 | 215 | 164 | | | | | | |
| - 21 | 230 | 163 | 248 | 159 | 215 | 159 | 186 | 150 | | | | | | |
| - 21 | 236 | 124 | 253 | 152 | 211 | 170 | 205 | 158 | | | | | | |
| - 19 | 247 | 171 | 258 | 156 | 214 | 173 | 208 | 152 | | | | | | |
| - 14 | 248 | 176 | 240 | 174 | 224 | 179 | 197 | 160 | | | | | | |
| 25 | 258-206 | | 267-217 | | 233-217 | | | | | | | | | |
| 26 | 257-216 | | 276-217 | | 239-226 | | | | | | | | | |
| 27 | 243-219 | | 262-222 | | 223-208 | | | | | | | | | |

TI-NHTSA 7281

RANGES: 3.00V 10.00V 2.500V
 OFFSETS: 0.0V 0.0V 0.1V
 TOTAL TIME: 1.00S
 POST-TRIG: 0.0S
 TRIGGER: MAN
 11:12:08 04 NOV 92

JD



Sample #1 6102
 Sample #2 1.2
 Sample #3 2.1
 Sample #4 0.1
 Sample #5 0.1
 Sample #6 0.1

HIGHLIGHTS
Stephen B. Offiler
Week Ending 92-11-06

Handwritten signature
92-11-06



AUSTRALIA: We have halted efforts on the full-round Kaption diaphragm design. Engineers at FOA and BCIA have basically finalized their decision to remain with the standard diaphragm configuration. This is based on:

- The full-round diaphragm was costly.
- We were (barely) able to demonstrate a 500K cycle life at 90% reliability and 90% confidence in one combined vacuum & Impulse experiment with 6 devices; we have not communicated the fact that repeatability of this test can be rather poor.
- FOA has offered to reduce the cycling pressure to 1000 psi, and we have responded that this will increase our confidence that we can pass Impulse testing.

FOA is asking for a detailed timing chart for completion of ISR, as well as a print update to include a note regarding modification to the ES procedure to combine vacuum and Impulse and to revise the parameters (vac 0.3 - 0.5 mmHg and Impulse at 1000 psi).

FOA has contacted Tim Andresen, who is now aware of the vacuum issue. He has requested that we complete a combined vacuum & Impulse test using the NAAO vacuum level on a low-priority basis. This will be comprehended in the upcoming plans for the CCPS cycler, which will also be occupied with LT and Cupri validation tests.

LT SILENT: We are proceeding with plans to convert all LT production (77PSL2-3 and 77PSL3-3) over to a single part number (L3-3) using a silent disc. Mfg. has completed a production lot of sensors using a truck silent disc. We checked a couple of the pilots on the noise equipment and confirmed they are quiet. We have completed a hatched-curve study per Dale's technique to determine preload target. The pin window on these is somewhat narrower than the original truck proto's characterized back in April. As a result, some compromise assumptions were made (max. temp decrease to 150 C and upper spec. increase to 325 psi) which provided a more than adequate pin target tolerance. These assumptions have not been communicated to LT Eng. Production has completed a build of 150 devices at this preload (with 100% yield) which we will be using for internal and Ford validation testing. We are performing a low and high temperature characterization on 24 to confirm the preload assumptions. The remainder of the production lot will not be final-assembled until we've completed this confirmation.

For validation LT Eng. is requesting an Impulse test plus a one-time high and low temperature characterization on 96 devices. This will be piggybacked with our temp. char. above; nonetheless, this represents a good deal of effort to complete. Jeff will be working Saturday. We are targeting the LT Eng. visit to Attleboro on Nov 17 for completion of these tests.

During the sensor build, we also constructed some special parts to help determine if the cup mod's on 27713 will also be required on 27288. This work will be conducted as a separate issue - given the 100% yield, with no rattlers identified, the priority is not high.

MISCELLANEOUS Discussion with Dave Key indicates the new laser disc-checking equipment is nearing completion. I have determined I characterized, known-quiet discs to him to commence correlation work.



**TEXAS
INSTRUMENTS**

Nov: 18, 1992

FACSIMILE TRANSMITTAL

TO:

Name: JOHN STORKEY
Location: KELSEY - HAYES
Mall Station:

Phone Number:

FAX Number: 313 684 5374

FROM:

ELAINE ROSE

TEXAS INSTRUMENTS MS 12-82²⁷

Phone Number: (508) 899-1907

FAX Number: (508) 899-3153

Total number of pages (including header page): 2

COMMENTS:

Part Number: E75C-2NB24-AA

Actuation: 350 - 450 PSI

Release: 120 min.

Differential: 50 min.

| | ACTUATION | RELEASE | DIFFERENTIAL |
|----------|-----------|---------|--------------|
| | 378 | 168 | 210 |
| | 431 | 152 | 279 |
| | 414 | 162 | 252 |
| | 412 | 154 | 258 |
| | 401 | 159 | 242 |
| | 413 | 132 | 281 |
| | 371 | 155 | 206 |
| | 398 | 160 | 228 |
| | 375 | 151 | 224 |
| | 356 | 172 | 184 |
| | 422 | 156 | 266 |
| | 425 | 154 | 271 |
| | 427 | 136 | 291 |
| | 365 | 159 | 206 |
| | 426 | 146 | 280 |
| | 412 | 164 | 248 |
| | 414 | 155 | 249 |
| | 423 | 131 | 292 |
| | 430 | 155 | 275 |
| | 410 | 150 | 260 |
| MIN | 365 | 131 | 194 |
| MAX | 436 | 172 | 292 |
| STD DEV: | 23.4505 | 11.3093 | 25.1763 |

.....

TRANSMISSION REPORT

| | |
|----------------------|----------------|
| TTI NO. | 313AR45374 |
| DATE AND TIME | 11 22 01:34 PM |
| DURATION | 0 |
| MODE | |
| PAGE | 04 |
| CODE | GOOD |

.....



**TEXAS
INSTRUMENTS**

Nov. 18, 1992

FACSIMILE TRANSMITTAL

TO:

Name: JOHN. STORKEY

Location: KELSEY - HAYES

Mail Station:

Phone Number:

FAX Number: 313-684-5374

FROM:

ELAINE ROSE (Q.A. TECH.)

TEXAS INSTRUMENTS MS 12-32

Phone Number: (508) 699-1907

FAX Number: (508) 699-3153

Total number of pages (including header page): 4

COMMENTS:

PART NUMBER: F2VC-9F924-AB

ACTUATION SPEC: 90 - 180 PSI

RELEASE SPEC: 30 PSI MIN.

| | ACTUATION | RELEASE |
|-----------------|------------------|----------------|
| | 138.0 | 60.1 |
| | 143.2 | 74.8 |
| | 146.0 | 64.5 |
| | 149.2 | 60.6 |
| | 144.0 | 61.6 |
| | 138.4 | 64.5 |
| | 137.0 | 62.8 |
| | 137.0 | 62.2 |
| | 131.4 | 66.7 |
| | 138.6 | 67.1 |
| | 136.9 | 66.3 |
| | 142.4 | 66.6 |
| | 132.4 | 60.9 |
| | 136.3 | 68.6 |
| | 139.3 | 48.2 |
| | 150.9 | 64.3 |
| | 146.3 | 64.8 |
| | 136.4 | 48.2 |
| | 141.6 | 61.7 |
| | 134.1 | 47.2 |
| MIN. | 131.4 | 47.2 |
| MAX. | 150.9 | 74.8 |
| STD DEV: | 4.7898 | 5.9166 |

PARTS LIST FOR SUPPLIER T095A
TEXAS INSTRUMENTS INC.
Page 1

| PART NUMBER | CHARACTERISTIC | CPK | <u>CP</u> | CP |
|-------------|----------------|-----|-----------|---------------|
| F2TA | 9C868 AA | | | |

| PART NUMBER | CHARACTERISTIC | CPK | | CP |
|-------------|----------------|-----------|---------|--------------|
| F3TA | 9F924 AA | ACTUATION | 3.49000 | 5.54 0.18000 |
| | | RELEASE | 3.05000 | 4.54 0.22000 |

| PART NUMBER | CHARACTERISTIC | CPK | | CP |
|-------------|----------------|-----------|---------|---------|
| F3TA | 9F924 AA | ACTUATION | 3.49000 | 0.18000 |
| | | RELEASE | 3.05000 | 0.22000 |

| PART NUMBER | CHARACTERISTIC | CPK | | CP |
|-------------|----------------|-----------|---------|---------|
| F2VC | 9F924 AB | ACTUATION | 3.49000 | 0.18000 |
| | | RELEASE | 3.05000 | 0.22000 |

| PART NUMBER | CHARACTERISTIC | CPK | | CP |
|-------------|----------------|-----------|---------|--------------------|
| E53C | 3N824 AA | ACTUATION | 1.60000 | 2.38000 |
| | | RELEASE | 4.07000 | 6.25 0.16000 |

| PART NUMBER | CHARACTERISTIC | CPK | | CP |
|-------------|----------------|-----------|---------|--------------|
| E57A | 3N824 AA | ACTUATION | 3.18000 | 4.76 0.21000 |
| | | RELEASE | 4.07000 | 6.25 0.16000 |

| PART NUMBER | CHARACTERISTIC | CPK | | CP |
|-------------|----------------|-----------|---------|---------|
| F3DC | 3N824 AA | ACTUATION | 3.18000 | 0.21000 |
| | | RELEASE | 4.07000 | 0.16000 |

| PART NUMBER | CHARACTERISTIC | CPK | | CP |
|-------------|----------------|-----------|---------|---------|
| E80C | 2C283 CA | ACTUATION | 3.18000 | 0.21000 |
| | | RELEASE | 4.07000 | 0.16000 |

| PART NUMBER | CHARACTERISTIC | CPK | | CP |
|-------------|----------------|-----------|---------|---------|
| E79C | 3N824 AA | ACTUATION | 3.18000 | 0.21000 |

PARTS LIST FOR SUPPLIER T095A
 TEXAS INSTRUMENTS INC.
 Page 2

| PART NUMBER | CHARACTERISTIC | CPK | CP |
|---------------|----------------|---------|--------------|
| E7SC 3N824 AA | RELEASE | 4.07000 | 6.25 0.16000 |

| PART NUMBER | CHARACTERISTIC | CPK | CP |
|---------------------------|---------------------------------|---------------------|--------------------|
| F3LH 19D594 AB | THREAD PITCH DIA. | 2.00000 | 2.20000 |
| | STEP DEPTH | 98.00000 | 0.00000 |
| | VERMINAL POSITION | 98.00000 | 0.00000 |
| | INSIDE DIAMETER | 98.00000 | 0.00000 |
| | OUTSIDE DIAMETER | 98.00000 | 0.00000 |
| | LOW PRESS. CALIBRAT. | 4.00000 | 4.10000 |
| | HIGH PRESS. CALIBR. | 4.20000 | 4.60000 |
| | THRD FIT TO MANIFOLD | 98.00000 | 0.00000 |
| | LEAK RATE | 98.00000 | 0.00000 |



**TEXAS
INSTRUMENTS**

Nov. 20, 1992

FACSIMILE TRANSMITTAL

TO: Name: *JOHN STORKEY*
 Location: *KELSEY-HAYES*
 Mail Station:
 Phone Number:
 FAX Number: *313-684-5374*

FROM:

TEXAS INSTRUMENTS MS 12-³⁷~~32~~
 Phone Number: (508) 899-1907
 FAX Number: (508) 899-3163

Total number of pages (including header page): *4*

COMMENTS:

11-20-92

John,

This should give you enough data to establish a good base file, for the 77PS.

In regards to the 57PS, the stored data we have is only a final report, after each run. This already has averages, etc. computed, individual piece data is not available.

We are not scheduled, at this time, to produce these switches until Jan '93. At which time I can send you the data you require.

If I can be of any further assistance, don't hesitate to call me.

Regards,
Elaine Rose

TI-NHTSA 7292

Pressure Tester

77PS PRESSURE TESTER

R&M RAMP RATE CHECK & ADJUSTMENT PROCEDURE

1. HAVE OPERATOR SET UP TEST LIMITS AS FOLLOWS WITH PRINT EVERY PIECE TURNED ON AND RUN RAMP RATE MASTERS THROUGH MACHINE.

LOW ACTUATION 300
HIGH ACTUATION 400

LOW RELEASE 150
HIGH RELEASE 200

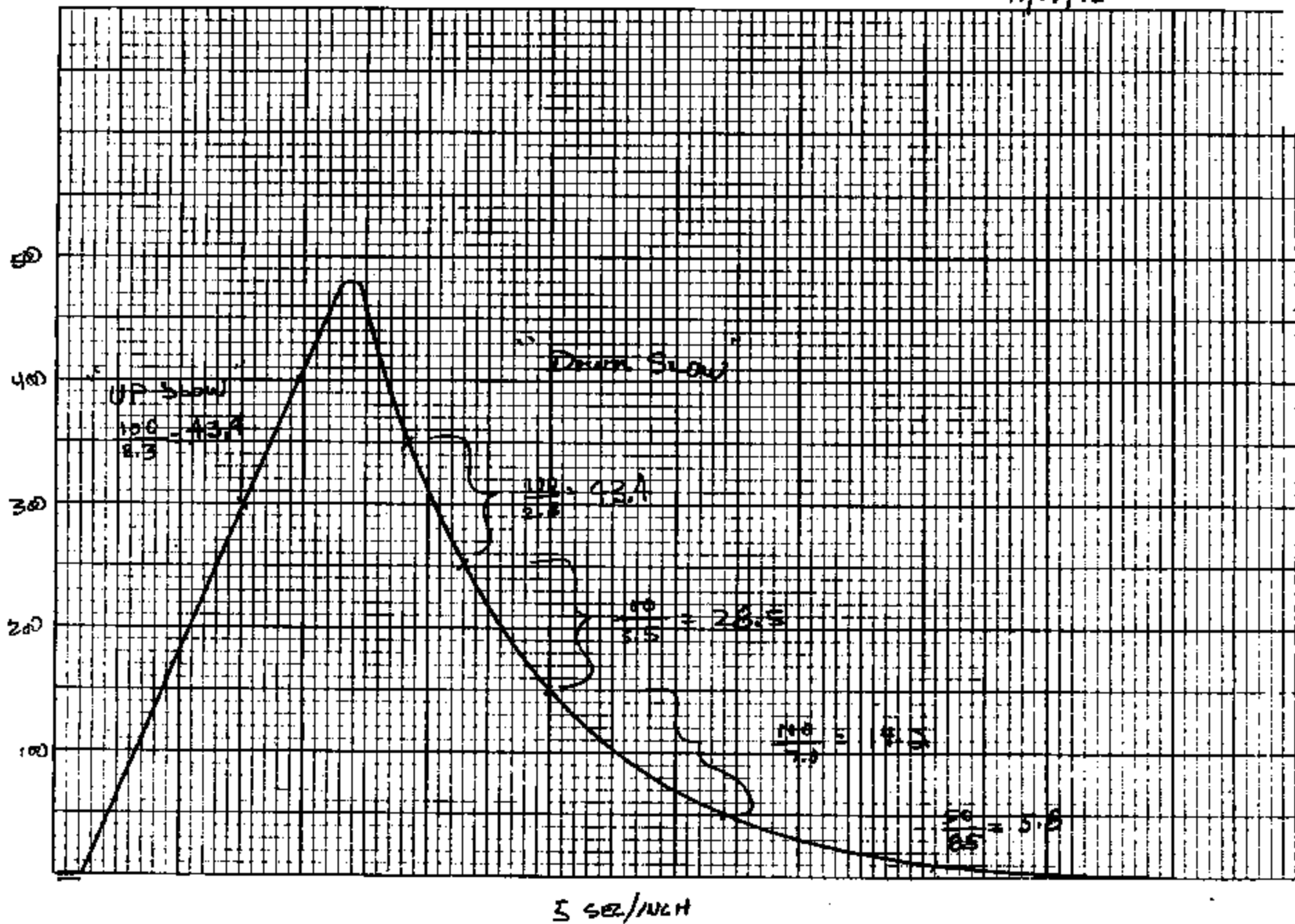
RAMP RATE 50

2. THE MRRU (MEASURED RAMP RATE UP) AND MRRD (MEASURED RAMP RATE DOWN) ON THE PRINT EVERY PIECE REPORT SHOULD BE WITHIN 40 TO 50 PSI PER SECOND.
IF ADJUSTMENT IS NEEDED, ADJUST THE SLOW UP OR SLOW DOWN FLOW CONTROLS AS REQUIRED.
3. AT ALL OTHER RANGES THE RAMP RATE DOWN WILL BE LOWER, DEPENDING ON HOW LOW THE LOW RELEASE, THE DOWN RAMP RATE CAN BE AS LOW AS 5 PSI PER SECOND. THIS IS ACCEPTABLE.

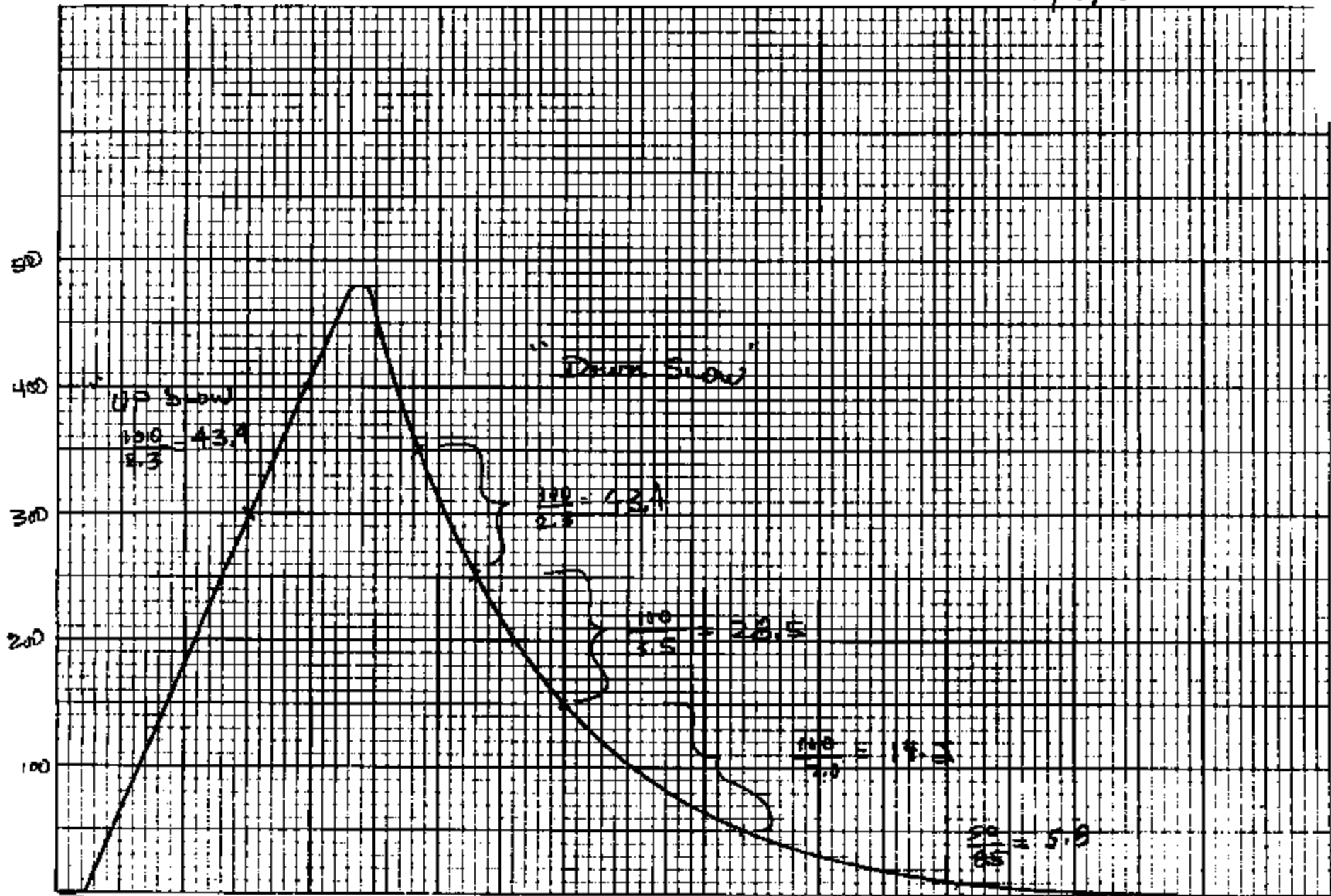
11/19/92

11/30/92 REV - CHANGED RELEASE RANGE

LOU ROCHA



11/19/92



5 sec/INCH

5-27-93

#121983 77PS PRES TESTER

RAMP RATE MASTERS

CYCLE TIME
REPERCENTAGE
OLD

2000 PER YOUNG

TI-NHT8A 7297

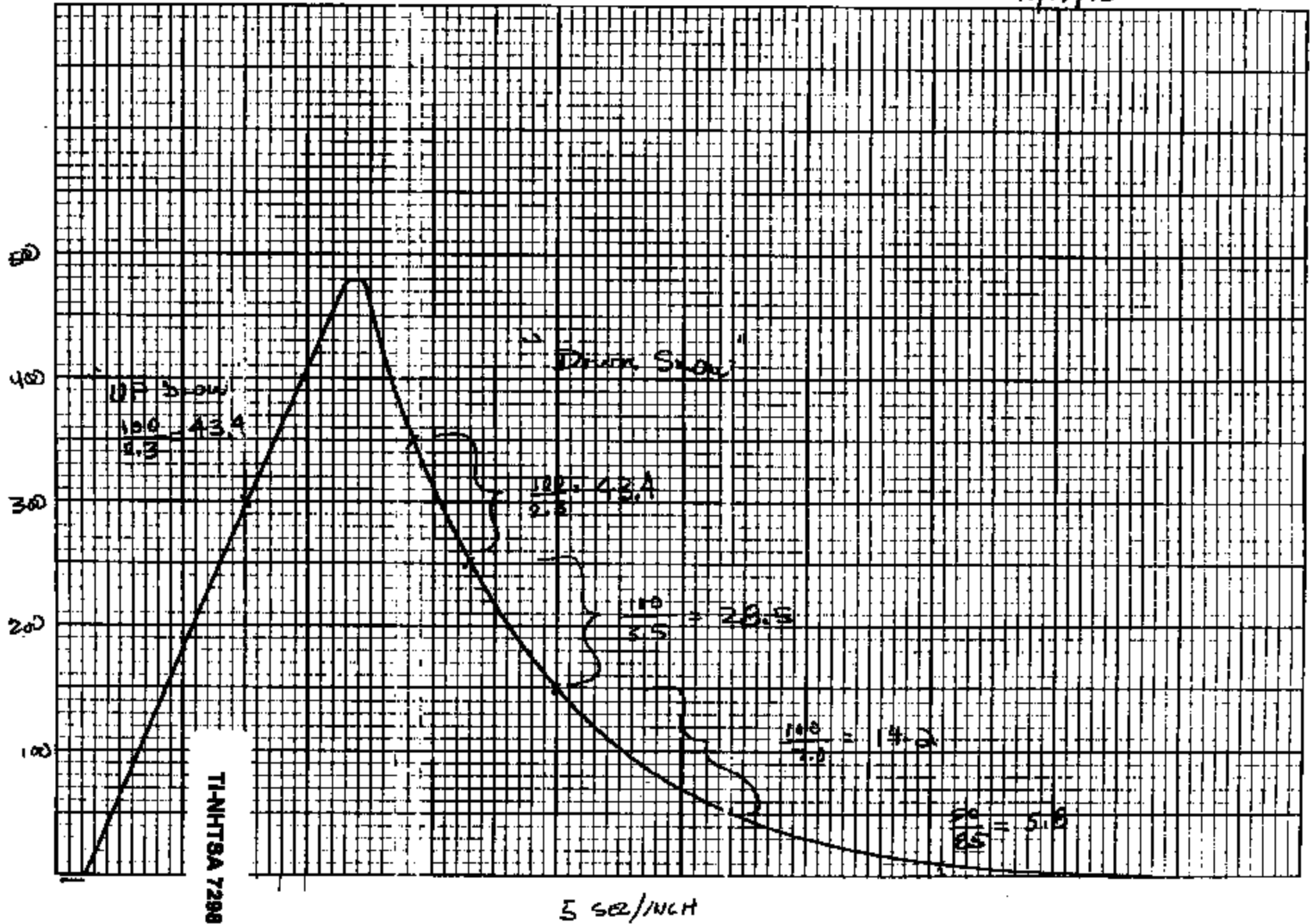
80
40



2
17.5
5 SEC/INCH

TRUCK

11/19/92



77PS PRESSURE TESTER

R&M RAMP RATE CHECK & ADJUSTMENT PROCEDURE

1. HAVE OPERATOR SET UP TEST LIMITS AS FOLLOWS WITH PRINT EVERY PIECE TURNED ON AND RUN DUMMY PARTS THROUGH MACHINE.

LOW ACTUATION 300
HIGH ACTUATION 400

LOW RELEASE 250
HIGH RELEASE 350

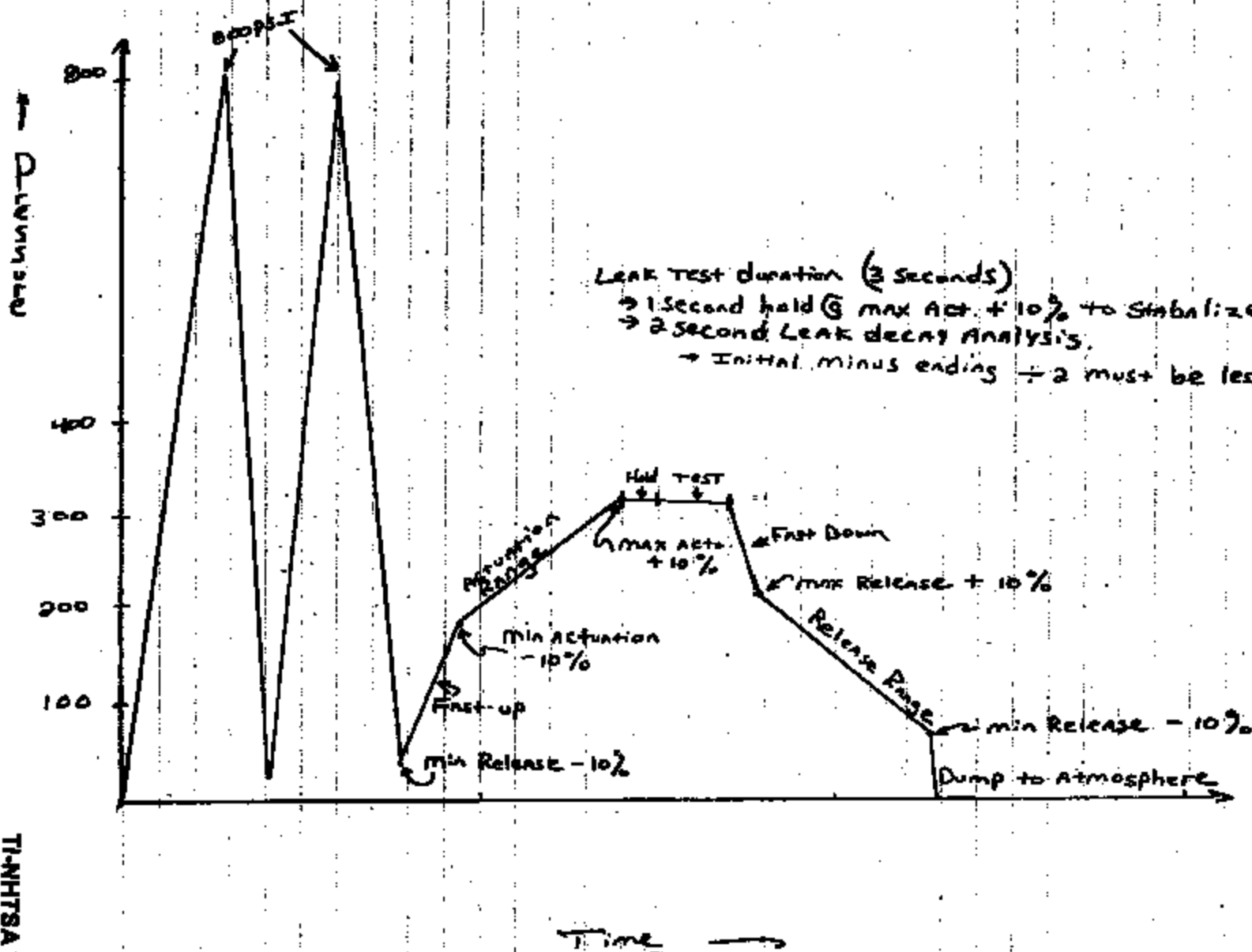
RAMP RATE 50

2. THE MRRU (MEASURED RAMP RATE UP) AND MRRD (MEASURED RAMP RATE DOWN) ON THE PRINT EVERY PIECE REPORT SHOULD BE WITHIN 40 TO 50 PSI PER SECOND.
IF ADJUSTMENT IS NEEDED, ADJUST THE SLOW UP OR SLOW DOWN FLOW CONTROLS AS REQUIRED.
3. AT ALL OTHER RANGES THE RAMP RATE DOWN WILL BE LOWER.
DEPENDING ON HOW LOW THE LOW RELEASE, THE DOWN RAMP RATE CAN BE AS LOW AS 5 PSI PER SECOND. THIS IS ACCEPTABLE.

11/19/92

LOU ROCHA

TPS Function Tester Ramp Profile

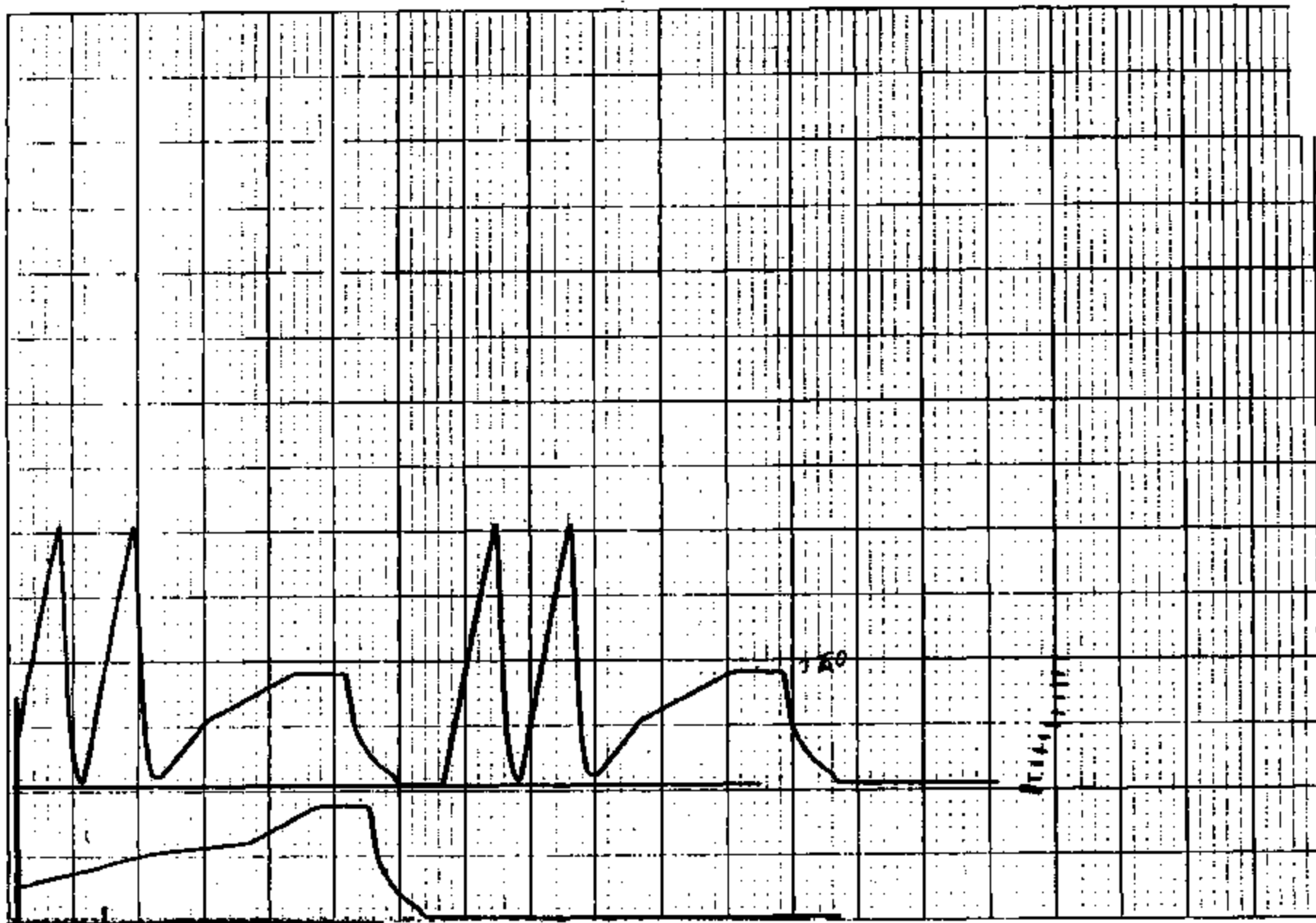


LEAK TEST duration (3 seconds)

→ 1 second hold @ max Act. + 10% to stabilize

→ 2 second Leak decay analysis

→ Initial minus ending ÷ 2 must be less than 10psi



Low,

3/10/92

We need to X-Y record the 77PS
Function tester during two different
test modes:

① Standard 77PSL2-1 Set-up.

② 77PSL2-1 Set-up without pre-cycles.
ie. Screen set to \odot PSI.

Can we try to get this done this
morning.

Thx

~~MATT~~

DP5L2-3

HEWLETT-PACKARD 9270-1005

5 sec/in

1V/in

2000lb TRANS

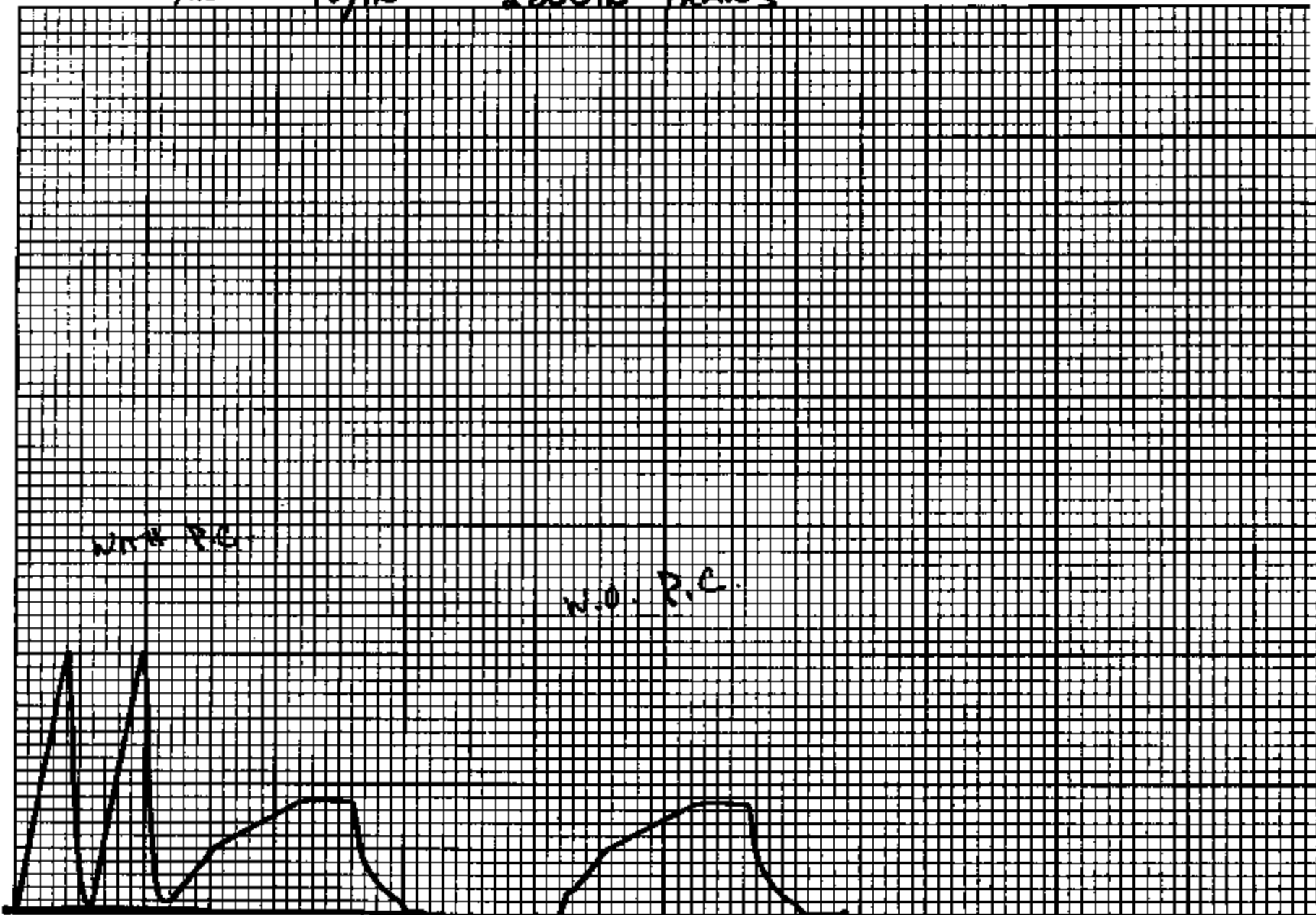
TI-NHTSA 7303

4000lb/in

N.O. P.C.

N.O. P.C.

5 sec/in



Manufacturing Systems Design
 Labor Report (Hours)
 Aug85

08/22/95
 Page 23

Department : PREC Expense Type : NORMAL

| Name | Week 1 | Week 2 | Week 3 | Week 4 | Week 5 | Total Hrs | Total \$ |
|-------------------|--------|--------|--------|--------|--------|-----------|----------|
| SECTION ELEC | 32 | 21 | 0 | 0 | 0 | 53 | 3,339 |
| PROJECT 253088039 | 32 | 21 | 0 | 0 | 0 | 53 | 3,339 |
| PCODE 88 | 32 | 21 | 0 | 0 | 0 | 53 | 3,339 |
| EXPENSE NORM | 239 | 431 | 285 | 0 | 0 | 955 | 48,708 |
| DEPT PREC | 312 | 533 | 405 | 0 | 0 | 1,250 | 64,576 |
| GRAND TOTALS | 1,157 | 1,536 | 1,418 | 0 | 0 | 4,111 | 212,374 |

MATT SELWEN -

PLEASE GET WITH JOHN K. TO NEGOTIATE
 A FAIR PRICE FOR LOU CAMARA'S TIME ON
 THE PRESSURE TESTER. LET ME KNOW WHAT WE
 SETTLE ON.

THANKS

John P.

Manufacturing Systems Design
Labor Report (Hours)
Aug85

08/22/95
Page 22

Department : PRRC Expense Type : NORMAL

| Name | Week 1 | Week 2 | Week 3 | Week 4 | Week 5 | Total Hrs | Total \$ |
|-------------------|--------|--------|--------|--------|--------|-----------|----------|
| PROJECT 8196069 | 8 | 1 | 7 | 0 | 0 | 16 | 704 |
| PCODE 69 | 36 | 98 | 91 | 0 | 0 | 225 | 10,622 |
| NAME CSOD | 2 | 0 | 2 | 0 | 0 | 4 | 176 |
| SECTION ELEC | 2 | 0 | 2 | 0 | 0 | 4 | 176 |
| PROJECT 8196086 | 2 | 0 | 2 | 0 | 0 | 4 | 176 |
| PCODE 86 | 2 | 0 | 2 | 0 | 0 | 4 | 176 |
| NAME EKAD | 4 | 4 | 0 | 0 | 0 | 8 | 504 |
| SECTION MECH | 4 | 4 | 0 | 0 | 0 | 8 | 504 |
| PROJECT 253087010 | 4 | 4 | 0 | 0 | 0 | 8 | 504 |
| NAME MGIO | 0 | 0 | 3 | 0 | 0 | 3 | 189 |
| SECTION ELEC | 0 | 0 | 3 | 0 | 0 | 3 | 189 |
| PROJECT 253087015 | 0 | 0 | 3 | 0 | 0 | 3 | 189 |
| NAME EKAD | 0 | 4 | 2 | 0 | 0 | 6 | 378 |
| SECTION MECH | 0 | 4 | 2 | 0 | 0 | 6 | 378 |
| PROJECT 253087020 | 0 | 4 | 2 | 0 | 0 | 6 | 378 |
| NAME CSOD | 2 | 3 | 0 | 0 | 0 | 5 | 220 |
| SECTION ELEC | 2 | 3 | 0 | 0 | 0 | 5 | 220 |
| NAME EBAT | 0 | 0 | 7 | 0 | 0 | 7 | 308 |
| SECTION MECH | 0 | 0 | 7 | 0 | 0 | 7 | 308 |
| PROJECT 8196087 | 2 | 3 | 7 | 0 | 0 | 12 | 528 |
| PCODE 87 | 6 | 11 | 12 | 0 | 0 | 29 | 1,599 |
| NAME LCAN | 32 | 21 | 0 | 0 | 0 | 53 | 3,339 |

77PSL2-1

TI-NHTSA 7308

500 PSI TRANSDUCER

L0 ACT = 90

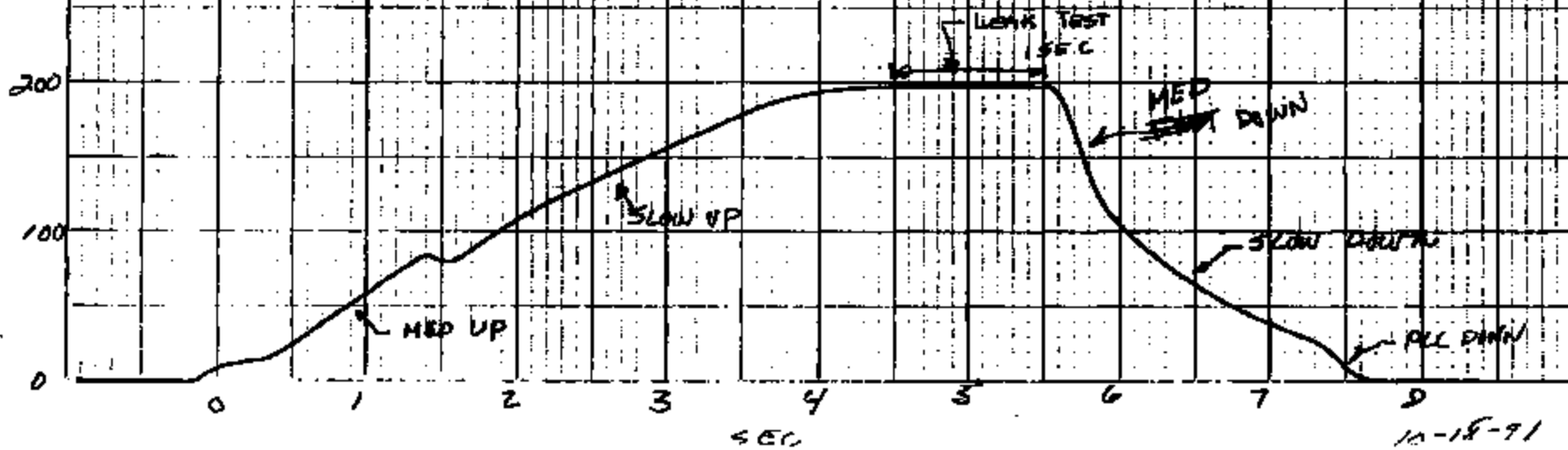
H1 ACT = 160

H1 REL = 100

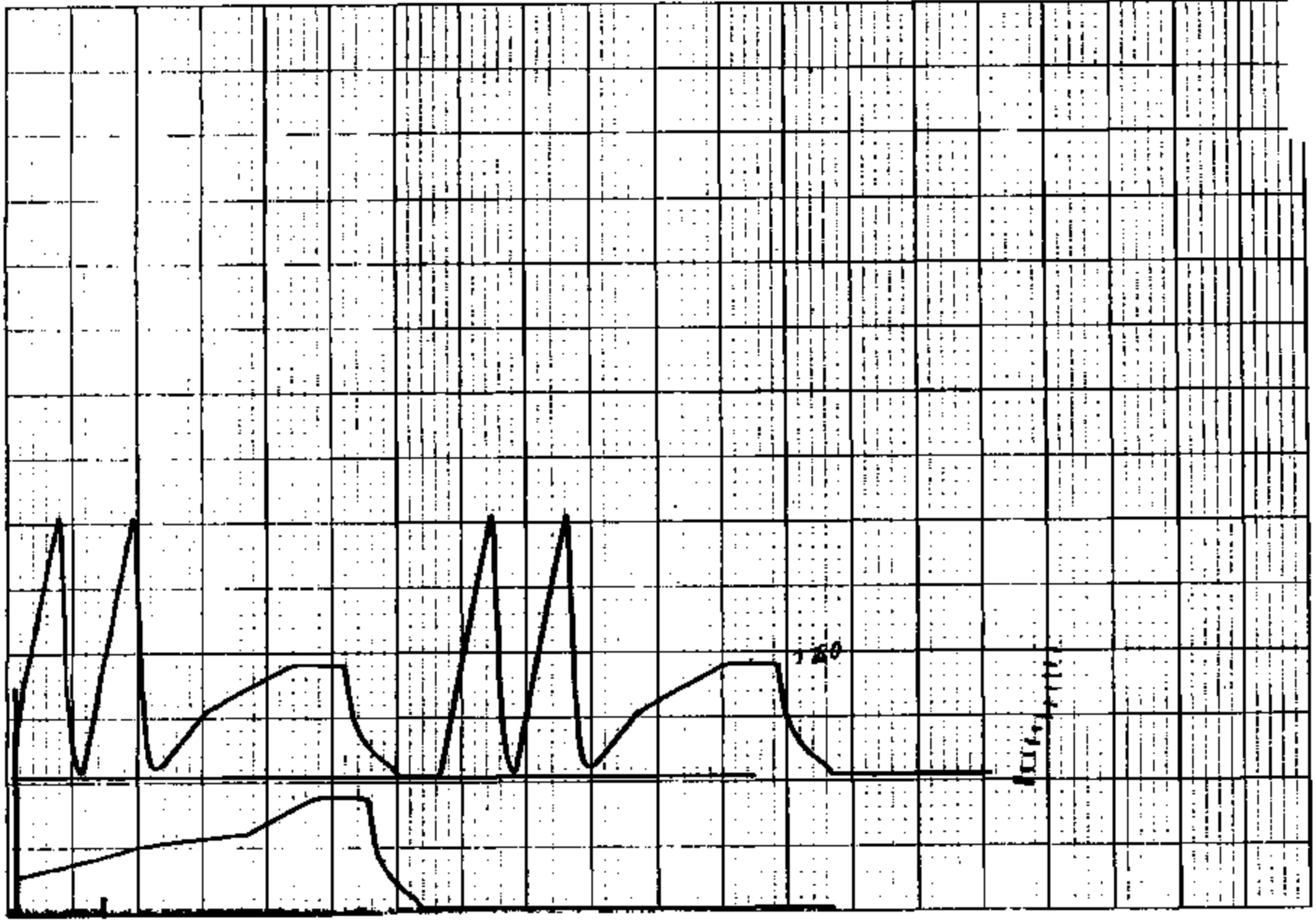
L0 REL = 150

Ramp Rate = 50

NOTE: ~~LOW~~ VALUES PLUMBED
FOR CON OFF = EXHAUST



10-18-71



TI-NHT8A 7307

TIPS THERMAL SWIFT EVALUATION

11/30/97

PBT

BASE EXPANSION

TEST #

R.T. → 150°C :

+ .0058"

209-15-12

R.T. → -40°C :

- .002"

204-15-23

ABRYL

R.T. → 150°C :

+ .0030"

302-15-24

R.T. → 182°C :

+ .0052"

77PSL2-1 Yields for 1992

| Data | Tested | Good | % |
|---------------------|---------------|---------------|--------------|
| January-92 | 14341 | 14209 | 99.1% |
| February-92 | 10689 | 10487 | 98.0% |
| March-92 | 28771 | 27980 | 97.3% |
| April-92 | 16827 | 16476 | 97.8% |
| May-92 | 12018 | 11138 | 92.7% |
| June-92 | 23443 | 23133 | 98.7% |
| July-92 | 11835 | 11873 | 99.5% |
| August-92 | 18636 | 18263 | 98.5% |
| September-92 | 11883 | 11562 | 98.0% |
| October-92 | 3838 | 3827 | 99.7% |
| November-92 | 0 | 0 | 0.0% |
| December-92 | 15839 | 15481 | 97.1% |
| Total | 162478 | 149010 | 97.7% |

77PSL2-1: Impulse Data Results 11/91 - 12/92

| | | | |
|-----------|-------|----|---|
| 10-Mar-92 | 4,000 | 10 | - |
| 11-Mar-92 | 4,000 | 10 | - |
| 12-Mar-92 | 4,000 | 10 | - |
| 18-Mar-92 | 4,000 | 10 | - |
| 23-Apr-92 | 2,000 | 5 | - |
| 2-May-92 | 2,000 | 5 | - |
| 5-May-92 | 2,000 | 5 | - |
| 6-May-92 | 2,000 | 5 | - |
| 14-Sep-92 | 2,000 | 5 | - |
| 22-Sep-92 | 4,000 | 10 | - |
| 30-Sep-92 | 4,000 | 10 | - |
| 7-Oct-92 | 4,000 | 10 | - |
| 7-Oct-92 | 4,000 | 10 | - |
| 16-Oct-92 | 4,000 | 10 | - |
| 21-Oct-92 | 2,000 | 5 | - |
| 20-Oct-92 | 4,000 | 10 | - |
| 29-Oct-92 | 4,000 | 10 | - |
| 29-Oct-92 | 4,000 | 10 | - |
| 30-Oct-92 | 4,000 | 10 | - |
| 4-Nov-92 | 4,000 | 10 | - |
| 10-Nov-92 | 4,000 | 10 | - |
| 10-Nov-92 | 4,000 | 10 | - |
| 11-Nov-92 | 4,000 | 10 | - |
| 17-Nov-92 | 2,000 | 5 | - |
| 20-Nov-92 | 4,000 | 10 | - |
| 4-Dec-92 | 2,000 | 5 | - |
| 9-Dec-92 | 2,000 | 5 | - |
| 14-Dec-92 | 2,000 | 5 | - |
| 16-Dec-92 | 4,000 | 10 | - |
| 16-Dec-92 | 4,000 | 10 | - |
| 16-Dec-92 | 4,000 | 10 | - |
| 21-Dec-92 | 2,000 | 5 | - |
| 21-Dec-92 | 4,000 | 10 | - |

| | | | |
|---------------|----------------|------------|----------|
| Totals | 265,650 | 665 | - |
|---------------|----------------|------------|----------|

*205 per Month
Feb 92*

-MSG N#- 00288465 FR-SBO1 TO-SBO1 SENT=12/02/92 03:24 PM
S#-096 ST=C DIV=0050 CC=00101 BY-SBO1 AT=12/02/92 03:24 PM

TO: Dave Crann EARN
Matt Sellers MJE2
Jeff DiDomenico DIDO

FR: Steve Offiler SBO1

SJ: Pass-Car Cup Modifications - Update

The plan to verify the Pass Car cup (27713) modification is as follows:

- 1) Build pilot lot using production equipment (approx. 30 pc)
- 2) Pressure-test for act/rel characteristics
- 3) Disassemble switch/sensor
- 4) Pre- and post-vacuum sensor dim. measurement
- 5) Determine magnitude of vacuum sensitivity, if any
- 6) Measure hysteresis curve on approx. 6 sensors
- 8) Build these 6, plus 18 more
- 9) Perform a standard Impulse test on the 24 devices
- 10) Disassemble switch/sensor
- 11) Pre- and post-vac sensor dim measurement
- 12) Determine if Impulse causes shifts in pre- and/or post-vac measurements

The first five items are complete. The cup change has been observed to cause these devices to actuate at lower pressures. This could be explained by the reduced disc envelope causing the converter bump to sit higher relative to the washer, giving increased effective wetted area and lower act. pressure. The pre- and post-vacuum measurements showed almost no shifts at all. Previous 50-pc test lots (car and truck) showed typically no shift except for a few devices shifting by about 1.7 mils; whereas 1/30 of these shifted by 0.8 mils and the rest exhibited no shift at all.

Two other areas which will be receiving attention immediately include: analysis of the environmental seal gland area for potential consolidation back to the red env seal; and completion of the "Change Checklist".

Regards, Steve O.

TI-NHTSA 7311

CNC SHOP - ORDER FORM

№ 009508

COST CENTER: 294 PRODUCT CODE: 088 CAPITAL PROJECT #: _____

REQUESTOR: MARY Ann King PHONE: 3583 MS: 12/20

CHECK WHICH CATEGORY PART DELIVERY IMPACTS:

_____ BILLING _____ TI CUSTOMER SCHEDULE _____ TI SCHEDULE _____ NON-CRITICAL

DATE REQUIRED: 1 1 SP OT BL MD

DRAWING #: 143434-4 PRINT REV: A CUSTOMER ORDER #: _____

PART DESCRIPTION: ALIGNMENT GAGE QTY: 1

WORK REQUESTED: MIKE POHL HAS PRINTS

105059

DICK GARIBAY

WORKORDER: 105059

CUSTOMER: 294/080

DEPT: PCA

CUSTOMER REF#: D03508

REQUESTOR: N KING

JOB DESC: NOT PAGE

QUANTITY ORDERED: 1

SPARE PART

DRAWING NUMBER: 8143-4 RA

ORGINATION DATE: 12/1/92

REQUIRE DATE: 01/31/93

CIRCLE REQUIRED OPERATIONS AND ENTER ESTIMATED HRS:

BO ED EO HA **04** JB CE BR ML

CIRCLE REQUIRED TREATMENT OPERATIONS:

BA BK CH CR HC HT NO RH TN V.E.

ENTER SEQUENCE OF OPERATIONS:

BT, HT, CE

HOURS PER OPERATION:

1 3

105059

MATERIAL REQUIREMENTS:

TOOLING REQUIREMENTS:

VALUE ENGINEERING:

MINUTES SAVED/PC: ORIGINATOR'S ENPS:

CHANGES MADE:

| SAMPLE NUMBER | | | | | | | | | | | SPEC RANGE | | NET | EMP |
|---------------|----|----|----|----|----|----|----|----|----|----|------------|-----|-----|-----|
| 11 | 10 | 09 | 08 | 07 | 06 | 05 | 04 | 03 | 02 | 01 | MIN/MAX | HOD | # | |
| | | | | | | | | | | | 095 | | | |
| | | | | | | | | | | | 095 | | | |
| | | | | | | | | | | | 1.24 | | | |
| | | | | | | | | | | | 1.24 | | | |
| | | | | | | | | | | | 1.13 | | | |
| | | | | | | | | | | | 1.13 | | | |
| | | | | | | | | | | | 1.22 | | | |
| | | | | | | | | | | | 1.22 | | | |
| | | | | | | | | | | | 1.13 | | | |
| | | | | | | | | | | | 1.13 | | | |

SPECIAL PLANNING NOTES:

**DRAWINGS AVAILABLE UPON
REQUEST**

CNC SHOP - ORDER FORM

No 003509

COST CENTER: 294 PRODUCT CODE: 088 CAPITAL PROJECT #: _____

REQUESTOR: MARY ANN KING PHONE: 3583 WS: 12/20

CHECK WHICH CATEGORY PART DELIVERY IMPACTS:

BILLING TI CUSTOMER SCHEDULE TI SCHEDULE NON-CRITICAL

DATE REQUIRED: 1 1 SP OT BL MD

DRAWING #: 143434-5 PRINT REV: A CUSTOMER ORDER #: _____

PART DESCRIPTION: ALIGNMENT GAGE QTY: 1

WORK REQUESTED: MIKE POHL HAS PRINTS

105060

FORM 22455

| SAMPLE NUMBER | | | | | | | | | | | SPEC RANGE | | NET | EMP |
|---------------|------|----|----|----|----|----|----|----|----|----|------------|-----|-----|-----|
| 11 | 10 | 09 | 08 | 07 | 06 | 05 | 04 | 03 | 02 | 01 | MIN/MAX | RCD | # | |
| + | 0002 | | | | | | | | | | 1.251 | | | |
| - | | | | | | | | | | | 1.25 | | | |
| + | 0003 | | | | | | | | | | 1.5139 | | | |
| - | | | | | | | | | | | 5.13 | | | |
| | | | | | | | | | | | 1.221 | | | |
| | | | | | | | | | | | 2.221 | | | |
| | | | | | | | | | | | 2.25 | | | |
| | | | | | | | | | | | OK | | | |
| | | | | | | | | | | | OK | | | |
| | | | | | | | | | | | OK | | | |
| | | | | | | | | | | | OK | | | |

TI CMC SHOP - FABRICATION WORKORDER

WORKORDER: 105060

CUSTOMER: 294/050 DEPT: PC6
 CUSTOMER REF#: 003509 REQUESTOR: M KING
 JOB DESC: ALIGNMENT BASE
 QUANTITY ORDERED: 1 SPARE PART
 DRAWING NUMBER: 14754-RA
 ORIGINATION DATE: 12/11/92 REQUIRED DATE: 01/31/93

CIRCLE REQUIRED OPERATIONS AND ENTER ESTIMATED HRS:

BO ED EO HA 4 JG CE BR WL

CIRCLE REQUIRED TREATMENT OPERATIONS:

BA BK CH CR HC NO RH TN V.E.

ENTER SEQUENCE OF OPERATIONS:

OT, HT, OT, CP

105060

HOURS PER OPERATION:

1 3

MATERIAL REQUIREMENTS:

TOOLING REQUIREMENTS:

VALUE ENGINEERING:

MINUTES SAVED/PC: _____ ORIGINATOR'S EMP#: _____

CHANGES MADE: _____

SPECIAL PLANNING NOTES:

**DRAWINGS AVAILABLE UPON
REQUEST**

27713-2 Cup Meeting 10/11/92

① Dis-Assemble remainder of devices from low act.
23 bases to be measured

Clair to
measure &
report.

② LS-2 Continuance of prod.

- Increase Hr temp test %
- Learn issues w/ Disc Curve & Continue w/ good curves.

*

③ Cup evals (-2)

2 Cups 27712-1 & 27713-2
2 Discs Low Act + Good/bad curve
process

→ Evaluate Curves
→ use AME to crimp.

+ Sigma

4 X TEST MATRIX

20 PSI (12) 27713-(A)
20 PSI (12) 27713-(B)
25 PSI (12) 27713-(C)
25 PSI (12) 27713-(D)
- Hand build
- AME crimp
- measure sensor X
- measure p-A curve

④ Disc envelope + HT check on 20 lb bad disc lot *

Test Matrix

12/11/92

Group A 20.57 / 11.78 + 27713 - 1
 Group B 20.57 / 11.78 + 27713 - 2
 Group C 25.3 / 16.7 + 27713 - 1
 Group D 25.3 / 16.7 + 27713 - 2

| A | | B | |
|-----|------------|-----|------------|
| | Sensor Dim | | Sensor Dim |
| A1 | 48.0 | B1 | 47.6 |
| A2 | 47.9 | B2 | 48.7 |
| A3 | 48.4 | B3 | 49.1 |
| A4 | 47.8 | B4 | 48.5 |
| A5 | 48.3 | B5 | 48.2 |
| A6 | 47.9 | B6 | 47.5 |
| A7 | 48.3 | B7 | 48.4 |
| A8 | 48.1 | B8 | 47.7 |
| A9 | 48.2 | B9 | 47.6 |
| A10 | 48.1 | B10 | 47.8 |
| A11 | 48.2 | B11 | 48.7 |
| A12 | 48.4 | B12 | 47.9 |

| C | | D | |
|-----|------------|-----|------------|
| | Sensor Dim | | Sensor Dim |
| C1 | 47.5 | D1 | 47.0 |
| C2 | 47.7 | D2 | 47.7 |
| C3 | 47.3 | D3 | 47.2 |
| C4 | 48.0 | D4 | 47.0 |
| C5 | 47.6 | D5 | 47.7 |
| C6 | 47.5 | D6 | 48.3 |
| C7 | 47.6 | D7 | 48.7 |
| C8 | 47.9 | D8 | 46.8 |
| C9 | 47.5 | D9 | 47.2 |
| C10 | 47.8 | D10 | 47.6 |
| C11 | 47.9 | D11 | 48.0 |
| C12 | 47.5 | D12 | 48.5 |

27389-2

Cer - Prod Part

~~.101~~
~~.107~~

.102
.103

~~.102~~
~~.108~~

.104
.105

4-19-2

27713-1

5-29-92

~~.012~~
~~.015~~

.012 4
.013

~~.090~~
~~.092~~

.090 4
.092

4-7-92

.013 4
.014

.090 4
.091

34

.013 4
.014

.090 4
.091

2-6

.013 4

.090/.091 4

1-30

.012 4
.015

.090 4
.091

1-28

.014 4
.015

.090 4
.091

Cheryl Bettinger
Bldg 11.
Converter

① Part number 27389-2

Dimensions * .101 / .107

* .162 / .168

~~Need Rec Insp or Bassett 20 data points~~

② Part number 27713-1 Cup

Dimensions * .012 / .015

* .090 / .092

~~Need Rec Insp or Valentine 20 data points~~

Each part take last 25 data points

**FORD NEXT GENERATION SPEED CONTROL (77PS)
MANUFACTURING CONTROL PLAN**

| PROCESS STEP DESCRIPTION | PRODUCT CHARACTERISTICS | EVALUATION METHOD | CONTROL METHOD | FREQUENCY OF TEST | REACTION PLAN |
|---|-----------------------------------|-------------------------------|-----------------------|--------------------------|-----------------------|
| BASE ASSEMBLY (AMI AUTOMATION) | TERMINAL HEIGHT | DIAL INDICATOR | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | TERMINAL PUSHOUT | FORCE GAGE/ DIAL INDICATOR | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | TERMINAL SEPERATION/ ALIGNMENT | PLUG GAGE | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | SPRING ANGLE (E) | COMPARATOR | X/R | 5pc/ 4 Hr. | SORT SINCE LAST CHECK |
| | SPRING CONTACT WIDTH | CALIPERS | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | SPRING TORQUE | FORCE GAGE | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | SPRING BUMP HEIGHT (E) | CALIPERS | X/R | 5pc/ 4 Hr. | SORT SINCE LAST CHECK |
| | RIVET HEIGHT | DIAL INDICATOR | X/R | 5Pc/ Hr. | SORT SINCE LAST CHECK |
| | CALIBRATION DEFORMATION | CUSTOM CONTINUITY SYSTEM | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| VISUAL QUALITY | VISUAL | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK | |
| SENSOR ASSEMBLY | CRIMP DIAMETER | CALIPERS | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | CRIMP HEIGHT | CALIPERS | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | VISUAL QUALITY | VISUAL | P | 5pc/ Hr. | SORT SINCE LAST CHECK |

CONFIDENTIAL

Revision: E

18 December 1992 MJS/cwr 050-0134

TI-NHTSA 7324

**FORD NEXT GENERATION SPEED CONTROL (77PS)
MANUFACTURING CONTROL PLAN**

| PROCESS STEP DESCRIPTION | PRODUCT CHARACTERISTICS | EVALUATION METHOD | CONTROL METHOD | FREQUENCY OF TEST | REACTION PLAN |
|--|--|--|-----------------------|--------------------------|---|
| FINAL ASSEMBLY (AMI AUTOMATION) | CRIMP DIAMETER (E) | GO/NO-GO GAGE | P | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | CRIMP HEIGHT (E) | GO/NO-GO GAGE | P | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | BASE TORQUE | TORQUE GAGE | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | CODE CRIMP RING/ DIAMETER-LEGIBILITY | PLUG-VISUAL | P | 5pc/ Hr. | SORT SINCE LAST CHECK |
| FUNCTION TESTER (CUSTOM) | ACTUATION/ RELEASE POINTS (Ford Significant Char.) | MASTERS | X/R | EACH SHIFT | TOOL ROOM/ ENGINEERING EVALUATIONS |
| | ACTUATION/ RELEASE POINTS | RAMP THROUGH PRESSURE RANGE | X/R | 100% | YIELD TRACKING/ SCRAP CONTROL |
| Q.C. AUDITS | OUTLINED IN DETAIL IN TEXAS INSTRUMENTS (QAS 208), FMC (THREADS / Ford Significant Char.) | | | | |

CONFIDENTIAL

Revision: E

TI-NHTSA 7325

18 December 1992 MJS/cst 05D-0134

**FORD (87PS)
MANUFACTURING CONTROL PLAN**

| PROCESS STEP DESCRIPTION | PRODUCT CHARACTERISTICS | EVALUATION METHOD | CONTROL METHOD | FREQUENCY OF TEST | REACTION PLAN |
|--|------------------------------------|-------------------------------|---------------------------|------------------------------|--------------------------|
| BASE ASSEMBLY (AM) AUTOMATION | TERMINAL HEIGHT | DIAL INDICATOR | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | TERMINAL PUSHOUT | FORCE GAGE/ DIAL INDICATOR | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | TERMINAL SEPERATION/ ALIGNMENT | PLUG GAGE | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | SPRING ANGLE (D) | COMPARATOR | X/R | 5pc/ 4 Hr. | SORT SINCE LAST CHECK |
| | SPRING CONTACT WIDTH | CALIPERS | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | SPRING TORQUE | FORCE GAGE | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | SPRING BUMP HEIGHT (D) | CALIPERS | X/R | 5pc/ 4 Hr. | SORT SINCE LAST CHECK |
| | RIVET HEIGHT | DIAL INDICATOR | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | CALIBRATION DEFORMATION | CUSTOM CONTINUITY SYSTEM | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | VISUAL QUALITY | VISUAL | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| SENSOR ASSEMBLY | CRIMP DIAMETER | CALIPERS | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | CRIMP HEIGHT | CALIPERS | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | VISUAL QUALITY | VISUAL | P | 5pc/ Hr. | SORT SINCE LAST CHECK |

CONFIDENTIAL

Revision: D

18 December 1992 MJS/cnr 050-0134

TI-NHTSA 7326

**FORD (87PS)
MANUFACTURING CONTROL PLAN**

| PROCESS STEP DESCRIPTION | PRODUCT CHARACTERISTICS | EVALUATION METHOD | CONTROL METHOD | FREQUENCY OF TEST | REACTION PLAN |
|--|--|--|-----------------------|--------------------------|---|
| FINAL ASSEMBLY (AMI AUTOMATION) | CRIMP DIAMETER (D) | GO/NO-GO GAGE | P | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | CRIMP HEIGHT (D) | GO/NO-GO GAGE | P | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | BASE TORQUE | TORQUE GAGE | X/R | 5pc/ Hr. | SORT SINCE LAST CHECK |
| | CODE CRIMP RING/ DIAMETER-LEGIBILITY | PLUG-VISUAL | P | 5pc/ Hr. | SORT SINCE LAST CHECK |
| FUNCTION TESTER (CUSTOM) | ACTUATION/ RELEASE POINTS (Ford Significant Char.) | MASTERS | X/R | EACH SHIFT | TOOL ROOM/ ENGINEERING EVALUATIONS |
| | ACTUATION/ RELEASE POINTS | RAMP THROUGH PRESSURE RANGE | X/R | 100% | YIELD TRACKING/ SCRAP CONTROL |
| Q.C. AUDITS | OUTLINED IN DETAIL IN TEXAS INSTRUMENTS (QAS 200), FMC (THREADS / Ford Significant Char.) | | | | |

CONFIDENTIAL

Revision: D

16 December 1992 MJS/cmr 050-0134

TI-NHTSA 7327

Engineering Review - 77AS

12 / 92

PS 1 of 2

Issue: 27713-2 Cup process validation by design eng uncovered issues related to sensor performance and dimensional stability.

27713-1 Cup Validation

27713-2 Cup

Sensor Dimensional Variability

.255 typical

.5 - .6 typical



+/- .30 Base
+/- .30 Pin
+/- .30 Sensor

+/- 1.0

+/- 0.5

+/- 0.8

+/- 1.0

+/- 0.5

+/- 1.8

+/- .30 Total

+/- 2.3

+/- 3.3

Target pre-load = 6.5 - 7.0

Temp Shift = 4.0 ish? (problem)

Disc Pre-deflection

None observed

Significant Amount = ?
since

Actuation (near side by side)

127 PSI typ

106 PSI typ.

Engineering Review - 77PS

12/16/92
PS 2 of 2

Production Outlook:
VOLUMES

| | L2-1 | L3-1 | L5-2 |
|--------|-------|-------|------|
| Dec 92 | - | 3.1K | 1.9K |
| JAN 93 | 20.7K | 15.5K | 3.1K |
| Feb 93 | ↓ | ↓ | ↓ |

Device

Proposed Processes

* 77PS L2-1 (snap)
77PS L3-1 (quirr)

Plan was to use (27713-2) CUP
- Eliminate loose disc fallout
- Allow conversion to red env. Ser 1

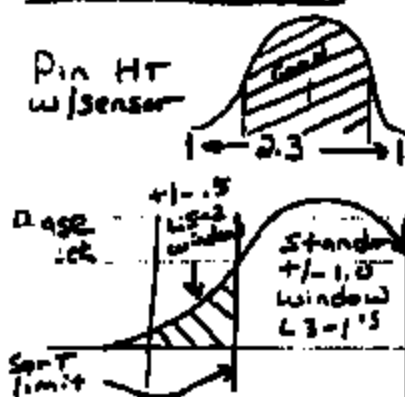
Proposed plan is to convert back to (27713-1) CUP and use standard L2-1/L3 processes. No vacuum sort for Ω .

77PS L5-2

Plan was to use (27713-2) CUP
- Eliminate loose disc fallout
- CIA for vacuum dependency
- Eliminate 100% vacuum sort
- Allow conversion to red env. Ser 1

Proposed Plan #1 is to revert back to (27713-1) CUP and use standard L5-2 processes. Continue vacuum sort 100%.

For Example



Proposed Plan #2 is to build with (27713-2) CUP accepting wider 3 σ on sensor, and compensating with pin height and base check sorters on-line to bring +/- 3 σ effective spring pre-deflection in-line with (27713-1) CUP performance

Re-cut's

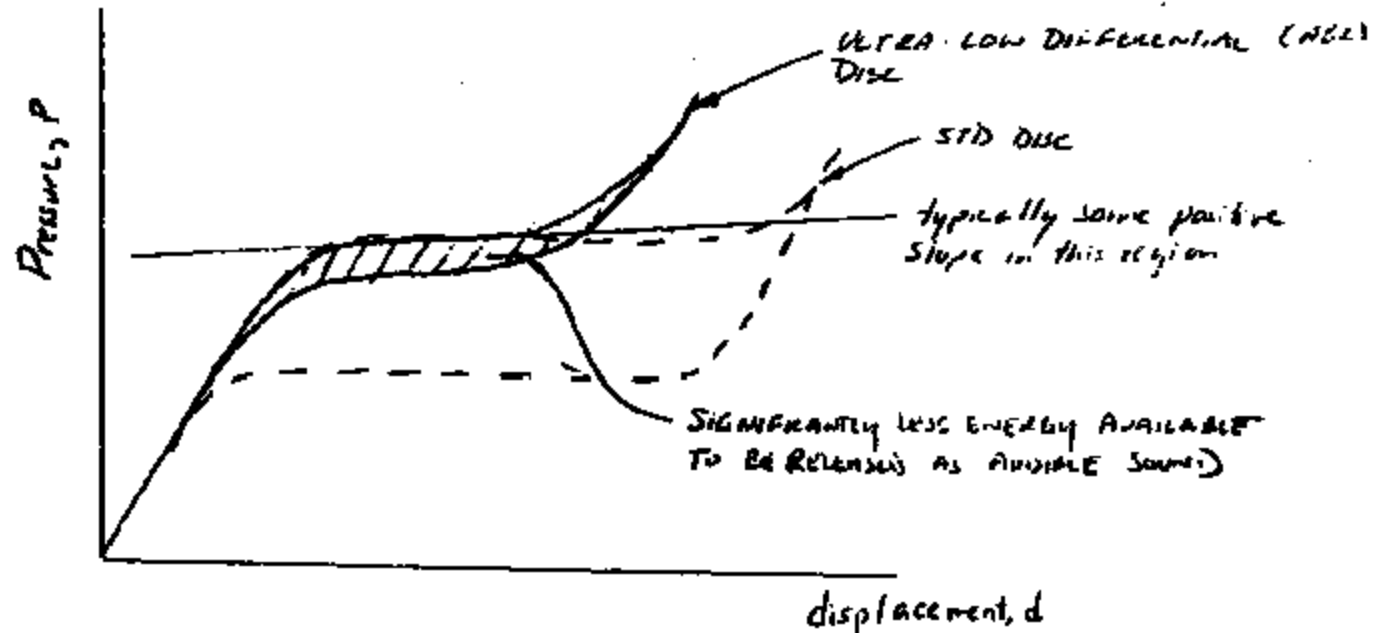
[Signature]

**DRAWINGS AVAILABLE UPON
REQUEST**

QUIET SWITCH

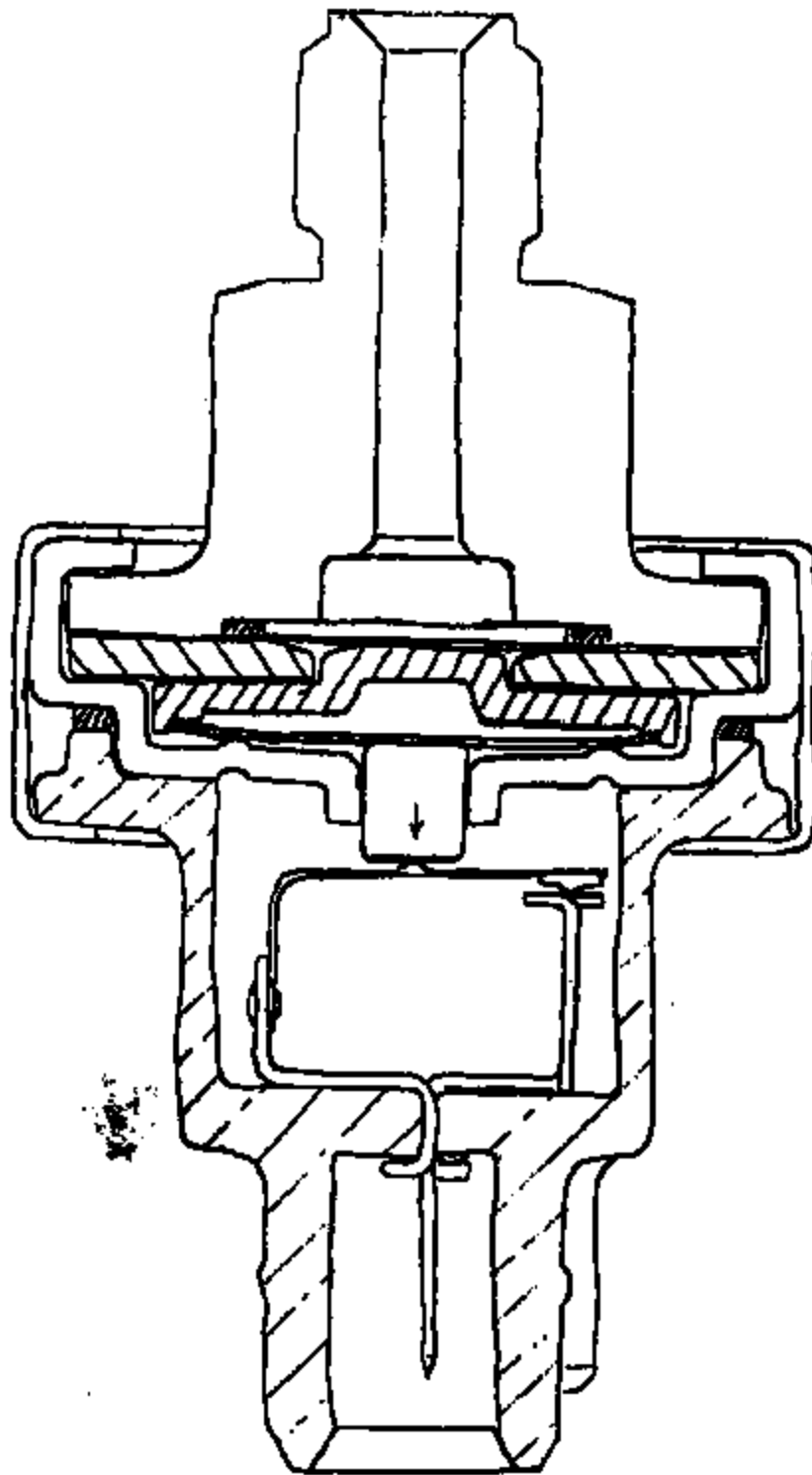
DISC TECHNOLOGY

THROUGH PROPRIETARY DISC TECHNOLOGY, THE HYSTERESIS OR DIFFERENTIAL IS REDUCED TO A MINIMAL VALUE, MAKING THE DISC INAUDIBLE TO OUR STANDARD DISC AND DEVICE MEASUREMENT EQUIPMENT.



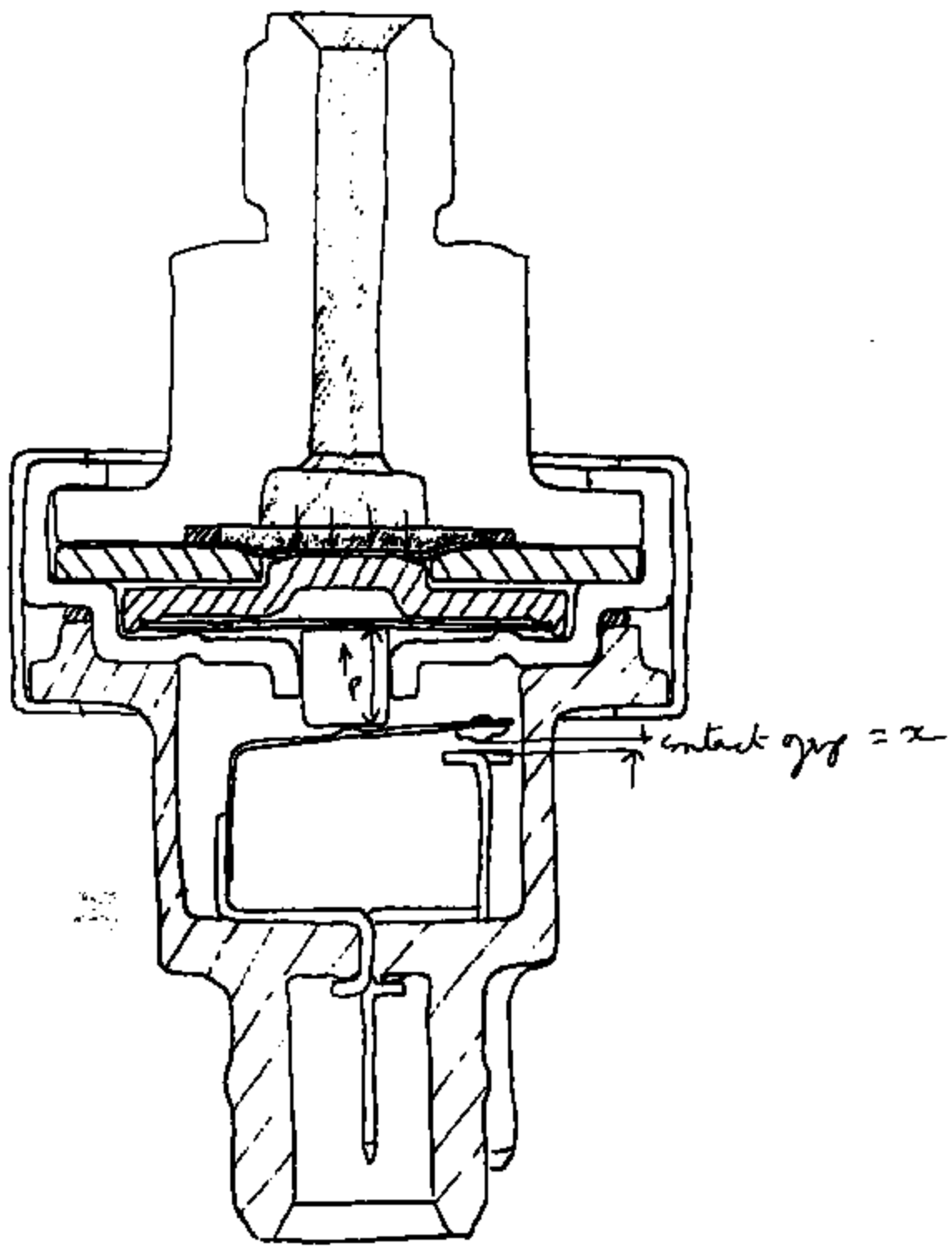
(A212)

UN-PRESSURIZED
CONTACTS CLOSED

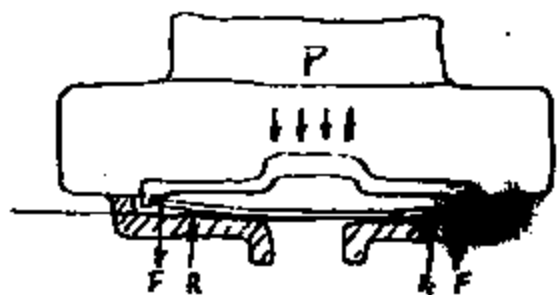


TI-NHTSA 7332

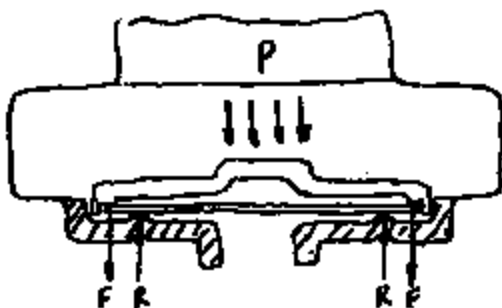
PRESSURE
CONTACTS OPEN



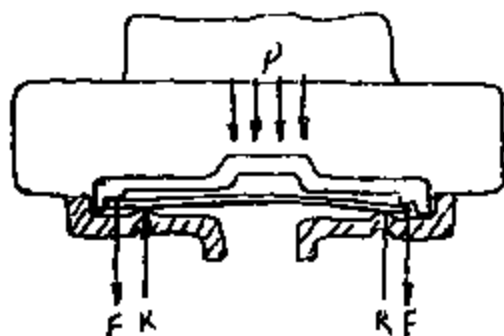
SENSOR ASSEMBLY PRESSURE VS. DISPLACEMENT



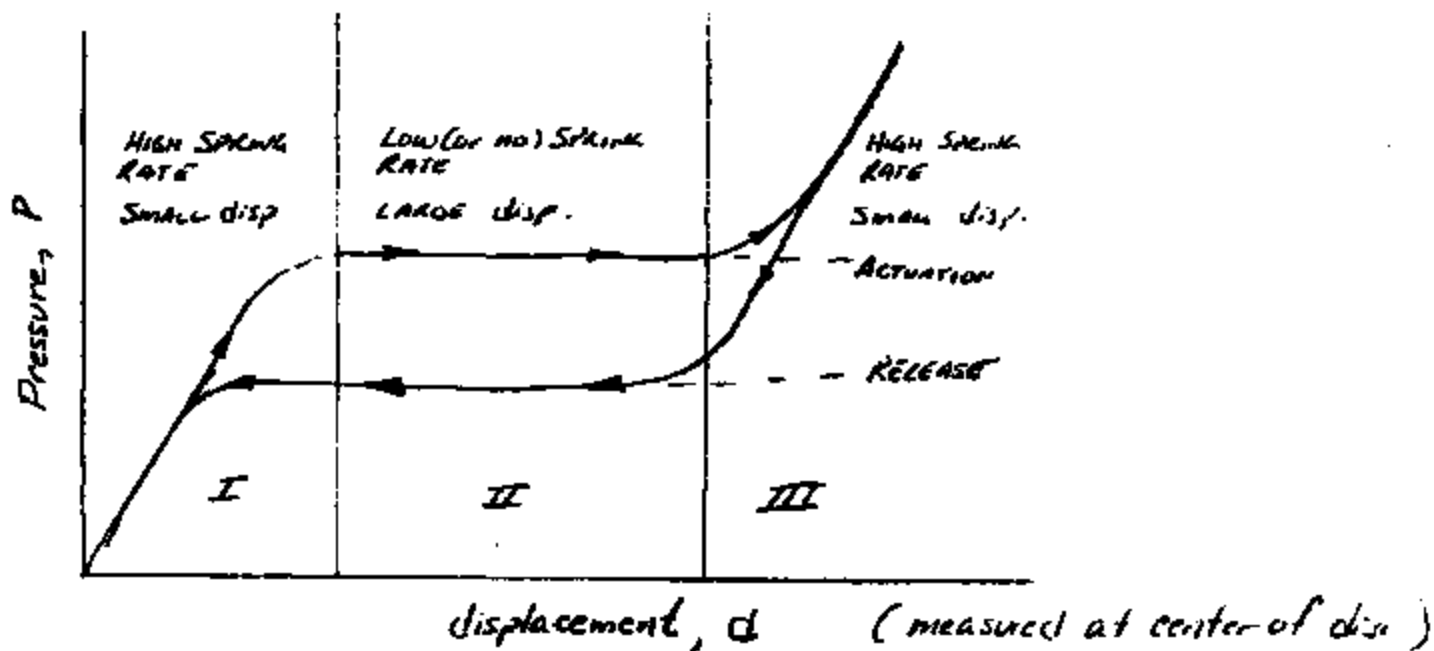
I. INITIAL PRESSURE APPLY RANGE



II. SNAP RANGE

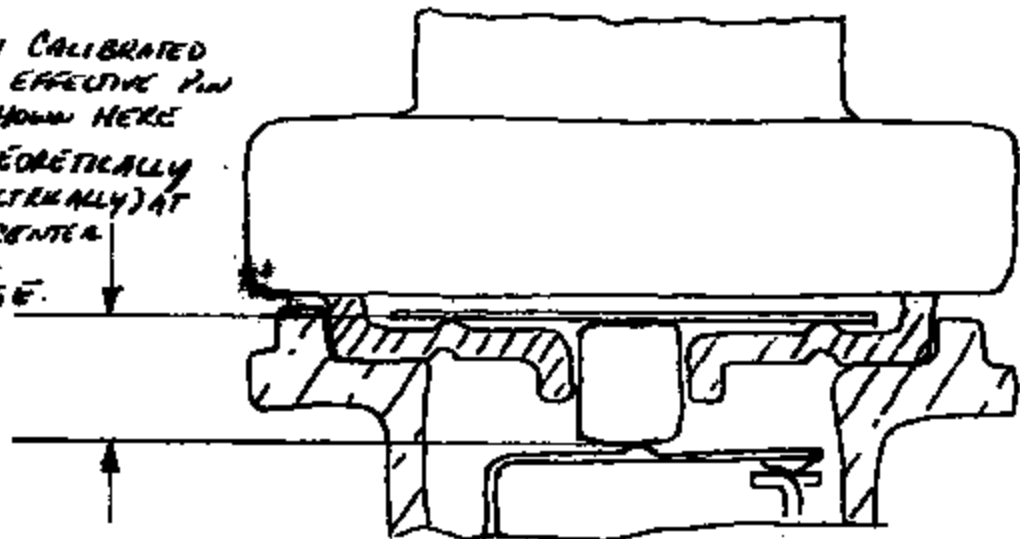


III. OVERPRESSURE RANGE

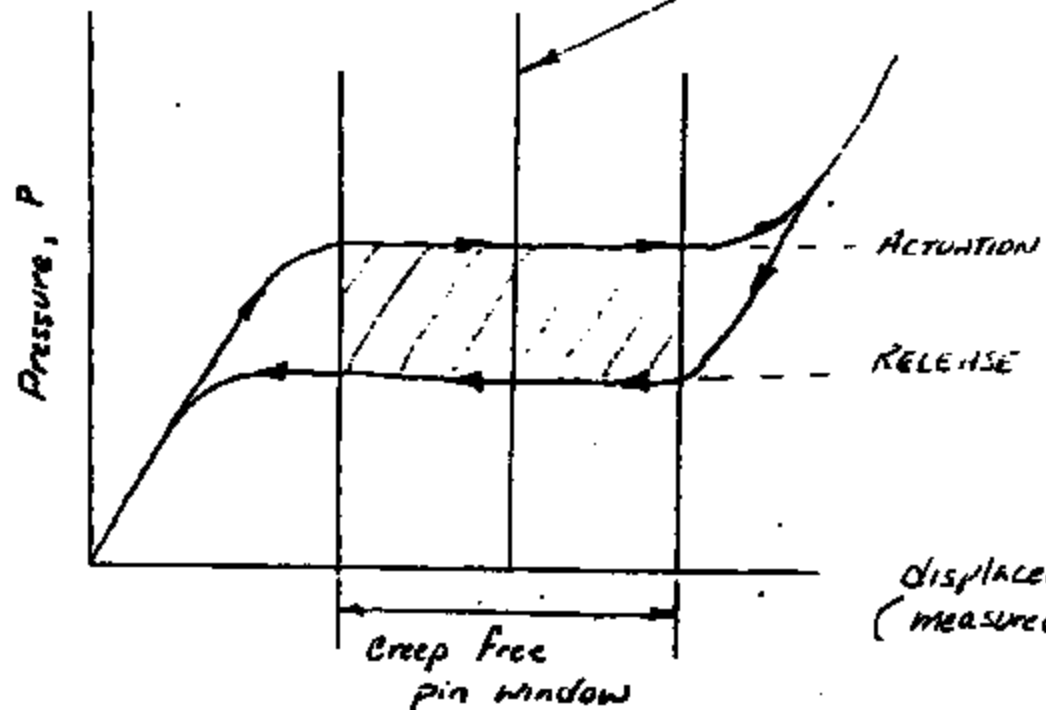


SENSOR DEPICTED AT THE ACTIVATION OR RELEASE PRESSURE WHERE THE DISC PASSES THROUGH INSTABILITY POINT

A SWITCH CALIBRATED WITH AN EFFECTIVE PIN LENGTH SHOWN HERE WOULD THEORETICALLY SWITCH (ELECTRICALLY) AT THE EXACT CENTER OF THE DISC SWAP RANGE.



CENTER OF PIN WINDOW WHERE DISC PASSES THROUGH A FLAT POSITION AS IT SWAPS



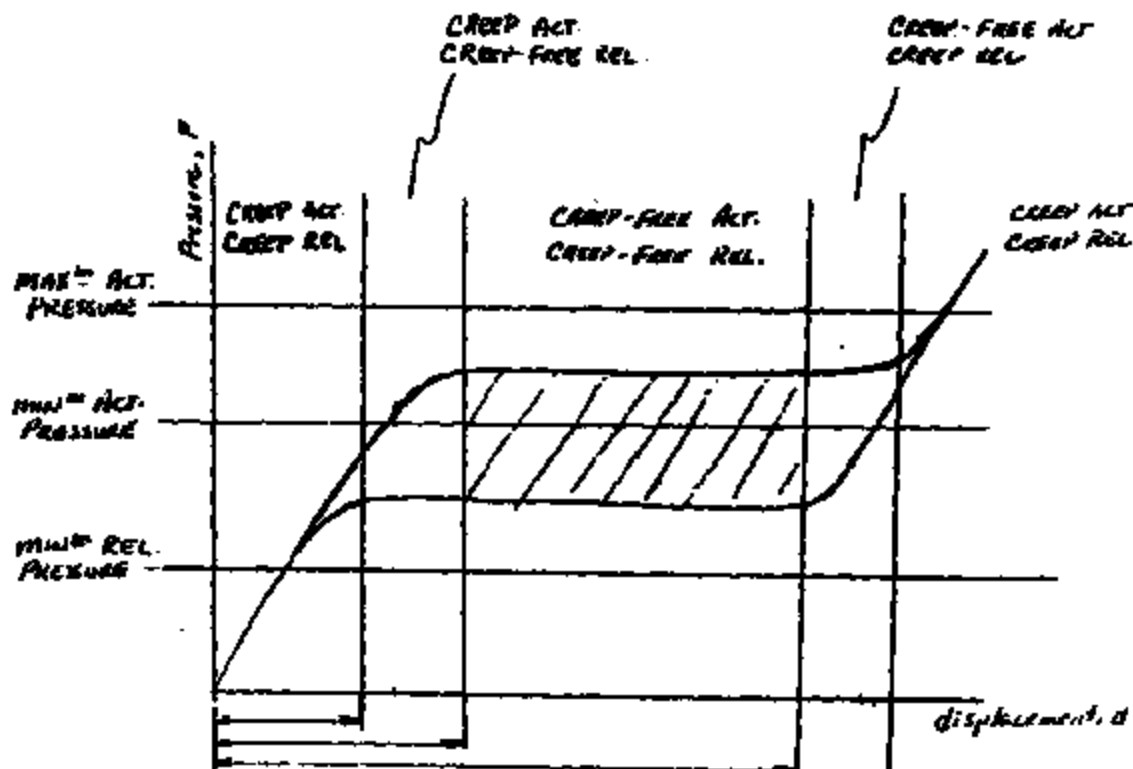
TI-NHTSA 7335

STANDARD (NON-QUICK) SWITCH

REGIONS WITHIN THE P-d CURVE ARE CORRELATED TO BASE CALIBRATION USING A "WINDOW" CALIBRATION

DISC SNAP IS COMPARED TO CHANGE IN CONTINUITY ON A TIME BASIS

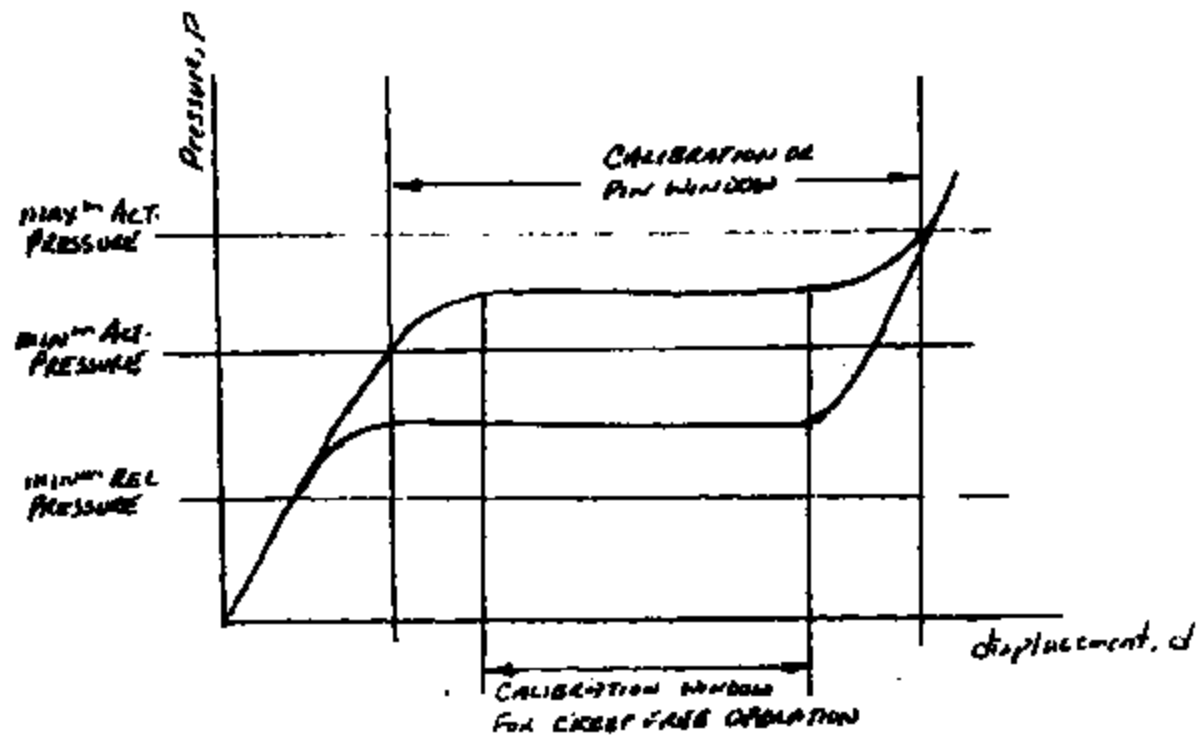
ACTUATION AND RELEASE "TIME" CORRELATE TO SPECIFIC REGIONS OF THE P-d CURVE

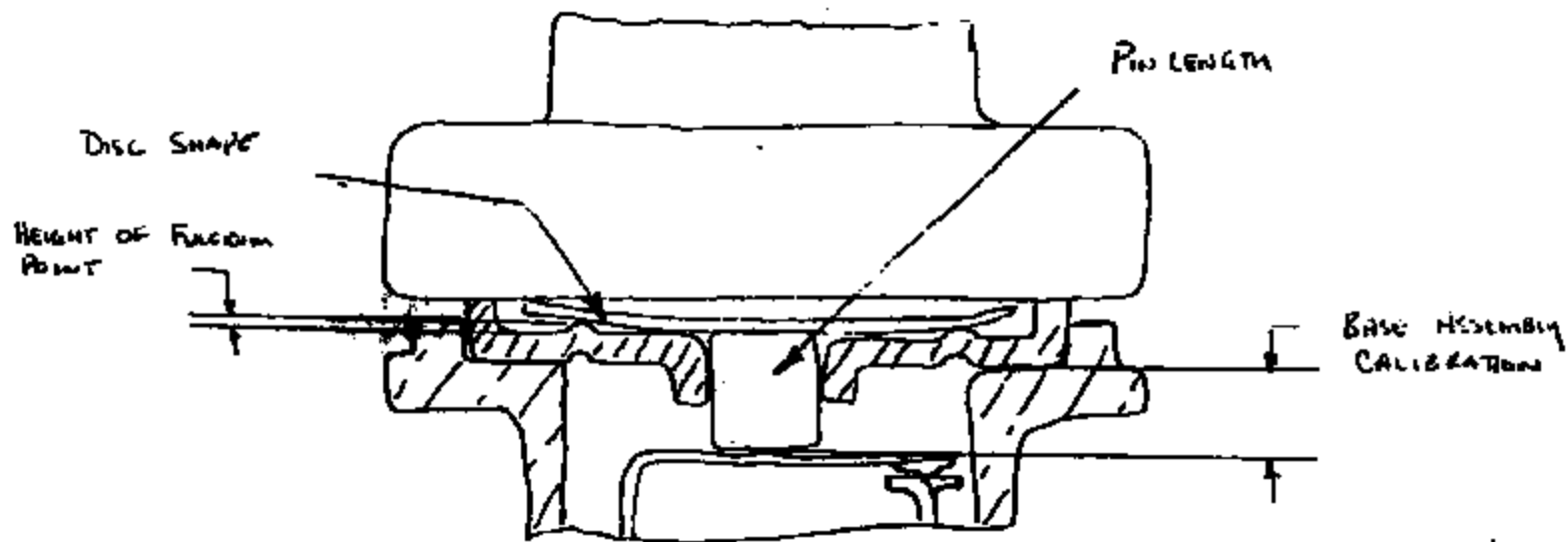


THESE POINTS ON THE PRESSURE-DISPLACEMENT CURVE CORRELATE TO BASE CALIBRATION

A PREMISE WITH THE NGSC SYSTEM HAS BEEN THAT CREEP FREE OPERATION CONSTRAINTS AREN'T NECESSARY DUE TO THE WAY THE SWITCH OPERATES IN THE SYSTEM.

A WIDER CALIBRATION WINDOW RESULTS; MAKING THE BUILD PROCESS MORE ROBUST TO ASSEMBLY TOLERANCES





CONTRIBUTORS TO ASSEMBLY TOLERANCES INCLUDE:

Component

PIN LENGTH VARIATIONS -

BASE ASM. CALIBRATION - EACH IS CALIBRATED TO A PRESET TARGET VALUE, BUT VARIABILITY EXISTS

DISC SHAPE - CAN VARY FROM LOT TO LOT, USUALLY NOT SIGNIFICANT

HEIGHT OF FULCRUM POINT IN CUP - TYPICALLY SEE LITTLE VARIABILITY WITHIN A LOT, BUT LOT TO LOT VARIABILITY EXISTS.

Assembly

SENSOR CRIMPING OPERATION - CAN AFFECT THE DIMENSION FROM THE CUP REFERENCE SURFACE TO THE CENTER OF THE PIN

FINAL CRIMPING OPERATION - CAN AFFECT THE "EFFECTIVE PIN LENGTH"
(SENSOR-TO-BASE CRIMP)

ADDITIONALLY, THE CENTERING OF THE ACTUATION & RELEASE PRESSURES ARE DEPENDANT UPON DISC CALIBRATION AND PRESSURE-TO-FEEL AMPLIFICATION RATIO.

BUCKET SWITCH

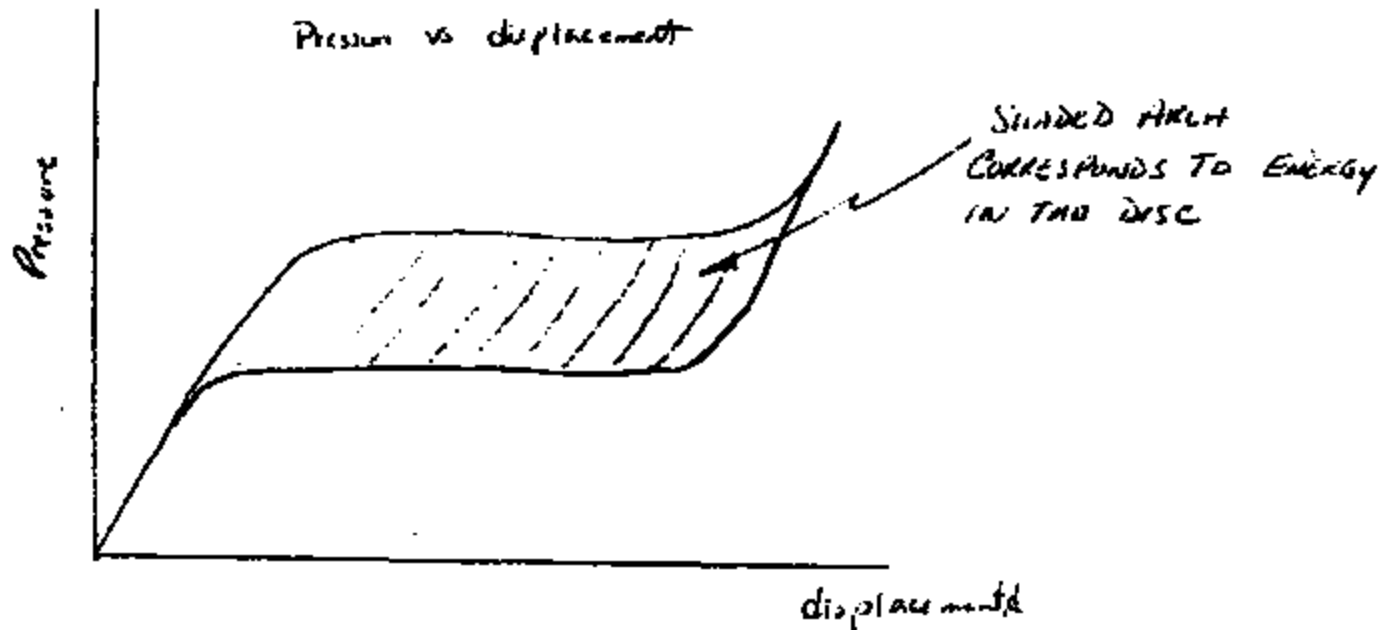
DISC TECHNOLOGY

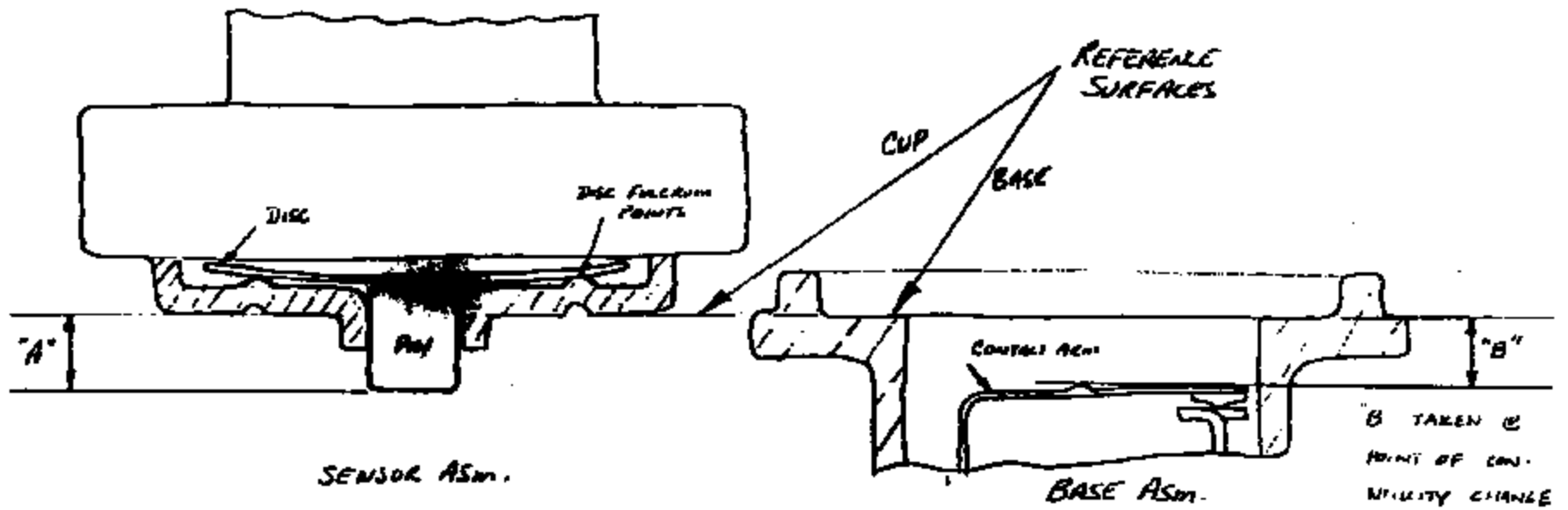
Discs used in standard (non-quiet) switches have a built in hysteresis which provides a relatively large difference in switch activation and release pressure.

The hysteresis differential - also provides for a relatively large calibration or pinning range.

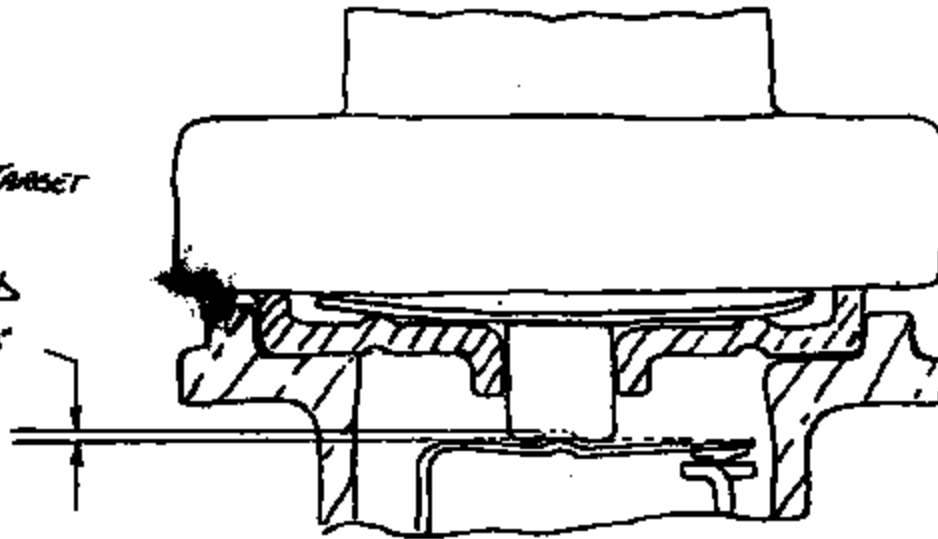
The area under the P-d curve is indicative of the energy received as audible noise during the snap.

STANDARD DISC

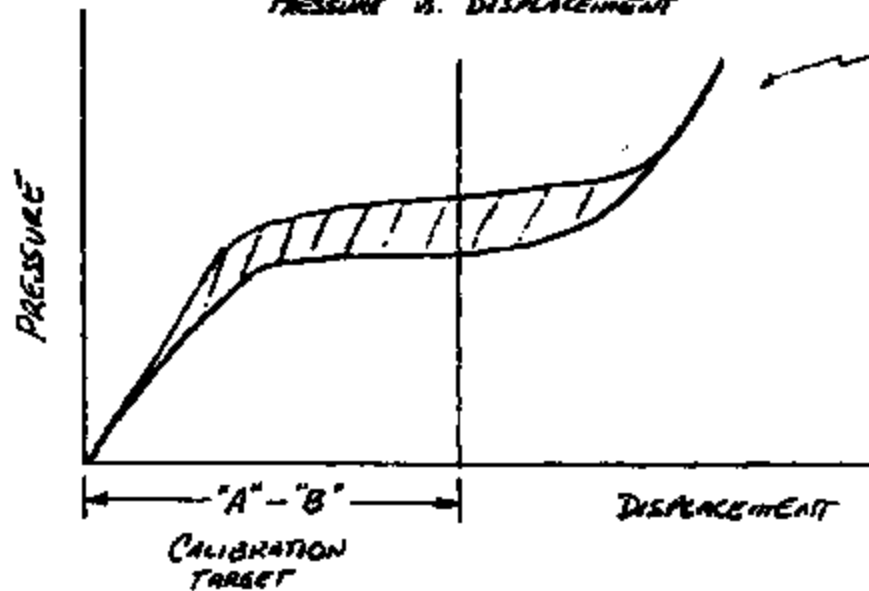




CALIBRATION TARGET
OR
ARM PRELOAD
"A-B"

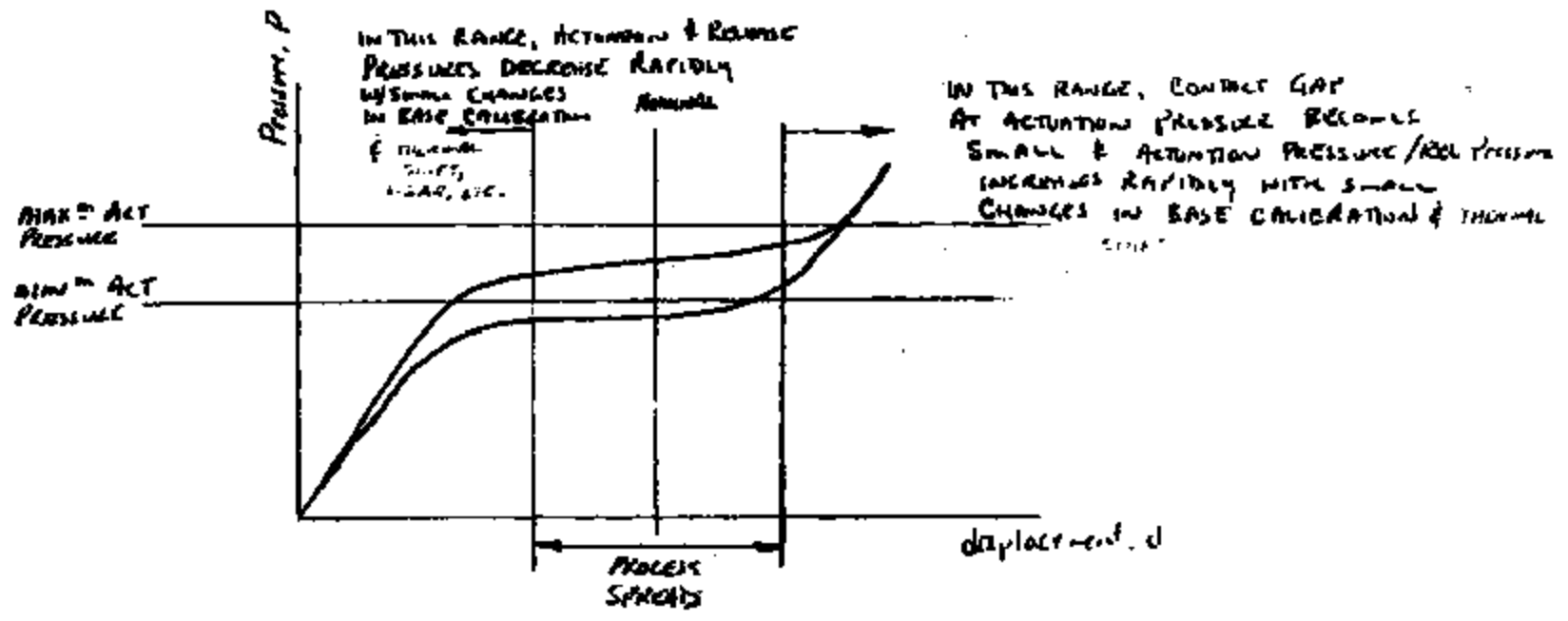


SENSOR ASM.
PRESSURE VS. DISPLACEMENT



CURVE DESCRIBES
MOTION OF DISC/PIN
AS PRESSURE IS
APPLIED.

CR T SWITCH



Q4 SWITCH

WITH WHAT WE KNOW OF THE QUIET SWITCH TODAY, THERE ARE SEVERAL KEY AREAS TO ITS SUCCESS:

- ① PRODUCING THE DISC ITSELF, WHICH IS NO LONGER AUDIBLE.
- ② PRODUCING SWITCHES WITH THE REDUCED CALIBRATION WINDOWS.
- ③ DETERMINING WHAT THE CALIBRATION WINDOW IS, BECAUSE THE STD. PROCEDURE - WHICH RELIES ON "HEARING" + DISC SNAP - NO LONGER APPLIES
- ④ MINIMIZING ASSEMBLY TOLERANCES TO MAXIMIZE THE NUMBER OF SWITCHES PRODUCED WITHIN THE CALIBRATION WINDOWS.
- ⑤ MAXIMIZING THE STABILITY OF THE CALIBRATION IN SERVICE; i.e. CHANGING TO A MORE STABLE BASE MATERIAL
- ⑥ PROVING THROUGH TESTING THAT:
 - a. SWITCHES ARE, IN FACT, INAUDIBLE IN THE VEHICLE
 - b. THE CHECKS IN PLACE IN PRESENT MANUFACTURING PROCESSES ARE SUCCESSFUL IN PROVIDING SWITCHES THAT MEET ALL OTHER PERFORMANCE REQUIREMENTS

| Date | Tested | Good | % | Failure Modes | |
|--------------|--------------|--------------|--------------|---------------|----------|
| Dec-82 | | | | | |
| 12/19 | 19 | 19 | 100.0% | | |
| | 220 | 211 | 95.9% | | |
| | 1885 | 1491 | 88.5% | cont 8 | echl 188 |
| | 50 | 46 | 92.0% | | |
| 12/15 | 1044 | 1042 | 99.8% | | |
| | 708 | 707 | 99.9% | | |
| | 1084 | 1082 | 99.8% | | |
| | 1028 | 1027 | 99.9% | | |
| 12/19 | 409 | 371 | 90.7% | cont 1 | echl 37 |
| | 50 | 50 | 100.0% | | |
| | 1378 | 1258 | 91.3% | cont 7 | echl 113 |
| 12/16 | 540 | 540 | 100.0% | | |
| | 424 | 423 | 99.8% | | |
| | 824 | 822 | 99.8% | | |
| | 80 | 80 | 100.0% | | |
| | 932 | 930 | 99.8% | | |
| | 478 | 476 | 100.0% | | |
| | 228 | 228 | 100.0% | | |
| | 72 | 72 | 100.0% | | |
| | 50 | 50 | 100.0% | | |
| | 262 | 251 | 99.6% | | |
| | 832 | 832 | 100.0% | | |
| | 640 | 640 | 100.0% | | |
| 12/16 | 1600 | 1499 | 99.9% | | |
| | 280 | 280 | 100.0% | | |
| | 438 | 438 | 100.0% | | |
| | 179 | 179 | 100.0% | | |
| 12/3 | 50 | 44 | 88.0% | rlcr 6 | |
| | 719 | 645 | 89.7% | cont 2 | rlcr 72 |
| Total | 18939 | 18481 | 97.1% | | |

QUIET DEVICES

* Cup changes:

*Self
discuss
to
discuss*

The Change Checklist is being used to track this change. The D1PFMEA's need to be updated, including the new knowledge of failure modes (vac shift, therm shift, wear shift...); 27713 needs some very minor updates for the sake of clarity; parts lists L3-1, L3-2, L5-2, L6-1 need updates for the -2 cup and -2 env seal. In addition, efforts to verify the -2 cup are still underway. It is known that -2 cups cause disc predeflection, which in turn increases sensor sigma, and pulls down the act & rel pressures. We also know that holed-Kapton shows a "disc float" of about 3 mils, and the force applied to the converter button by the Kapton diaphragm is substantial enough to cause some disc deflection. We are prototyping a reduction of the button height to limit the force applied to the disc, as well as backing off on the cup change from the present .0034" back to about .0025". The concern here is that we're working on minute changes ("m-eye-noor", not "minit") which are quite a bit smaller than the typical print tolerances; any shifts at all will completely wash out any gains we manage to make. We need a much better understanding of the disc envelope, including the design geometry and variability, the process-induced variability, and the balance of forces which come into play (diaphragm versus disc P-d curve). The one thing we might be able to do, to make all the troubles disappear, is to develop a silent disc with larger throw (maybe a thinner material, 455SS ? ...)

* Disc Dept. Automatic Disc Checker II correlation

The new ADC II is in final debug stages, and production discs are being supplied from it. We have 20 individually identified discs with ADC printouts. The goal is to run disc curves on our equipment to attempt correlation with the ADC readings, as well as build into sensors and run curves.

* Complete analysis of Atlanta returns

We still don't know exactly why the devices are open-circuit on the car. Since we know "Vacuum-Dependent" devices open under vac and reset with positive pressure, it follows that vacuum must exist within the master cylinder. We have constructed a test buck and plan to try to replicate the failure on parts known-bad from Atlanta. Following this, we plan to disassemble the devices in order to measure the sensor vacuum-shift, as well as determine the post-assembly preload. Then, some sensors should be opened by hexport-cutting technique which allows diaphragm inspection in the crimped condition. This could be extremely interesting, because the Kapton in vacuum-dependent parts is bi-stable, and actually "snaps" like a disc upon vacuum-reset.

* Preload Measurement Uncertainties Experiment

* Wear shift characterization - per 87PS discovery

* Updates to 77PS ES and internal TI Q.A.S. for quarterly In-Process noise audits

SBO921218/11a PRIORITY-Y

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TI-NHTSA 7345

L3-3
F-SERIES LIGHT TRUCK

* Pelkey high ambient Impulse test

This test was recently run at John Pelkey's request, using the ES 135 C brake fluid temperature but increasing from the ES ambient (121 C) to 149 C = 300 F. We passed 500K successfully and completed a report. However, running to failure would provide potentially valuable diaphragm life information.

* Hank Karzun PN96 Tokico samples; need PIST/PIPC; due Feb 8

Charlie is checking on this - they may have already been shipped.

* Changeover L2-3 and L3-3 snap to L3-3 silent, due 11 Jan 93

Customer-requested validation / ISW work completed. The change involves replacing the snap disc with a silent disc, and updating the customer PIN to CA. The preload target has been determined to be 9.5 - 10.0 mils. Pilots have been run successfully. No vacuum shifts have been detected. No dimensional changes to the cup have been indicated. We must still determine the temperature to run the in-process high-temp consistency audit. mtd
dbr

* Visit from Pelkey, Modi, and sup'v Jim Ritz scheduled for 11 Jan 93

FORD USA BRAKE (77PSL1-1, 77PSL3-1, 77PSL3-2)

* First Cycle Syndrome

The fact that our device requires a couple of cycles to stabilize readings is well-known, even to the point where it is documented in the ES. However, the permanence of the stabilization is a question: apparently there is some storage "reset" taking place which means the stabilization goes away after a while. How much, how long, require characterization. Certain customers only check our device once (w/o stabilization cycles) and report instances where the 160 psi max. acc. reads upwards of 200 psi. We have had RMR's for this. A Band-Aid solution implemented on some products is a non-symmetric print spec, reading 125 psi +75/-35, which accounts for 40 psi worth of first-cycle syndrome.

WIN88 (77PSL3-2)

* Program Issues:

We may owe Ford an envelope drawing - TBD. The drawing with snubber exists. We are trying to back them away from the snubber. Charlie has recently delivered test parts which are actually production L3-1's. We expect they'll find these undetectable in their system. The ISW strategy should be comprehended.

CAPRI (77PSL6-1)

* Spec negotiation (Impulse pressure/temperature) and note on print

We learned at the 11th hour that the vacuum exposure during evac-and-fill is extremely high relative to the NAAO ES. We checked some parts and discovered the diaphragm wrinkling under this vacuum, which indicated a possible life issue. We did a major vacuum-life test, and found the vacuum parts performing worse than the controls but all parts surviving the ES 500K cycles. Ford Australia now wants us to delete the ES Impulse and Vacuum procedures, and replace them with a combined vacuum-Impulse test. They want a note on the envelope drawing explaining this. They have examined the master cylinder ES and field requirements, and determined our ES pressures and temperatures exceed these requirements. I began a campaign to negotiate lower Impulse pressures and temperatures, and they have responded by lowering the pressure from 1450 psi to 1000. I am of the opinion that temperature has a much stronger influence on diaphragm life, but negotiation seems to have stalled. I am withholding their requested print update pending completion of this negotiation.

* Schedule for L6-1 Validation:

| | |
|--|---------------|
| Build val parts (new cup, new O-ring), init char | 18 Jan-22 Jan |
| Approval of similarity claims | TBD |
| Impulse, TC, misc tests, similarity claims | 25 Jan-12 Feb |
| Compl final char | 15 Feb-19 Feb |
| Report writeup | 22 Feb-25 Feb |
| Ship ISR package | 26 Feb 93 |
| ISR MRD @ BCIA | 12 Mar 93 |

FALCON (77PSL4-1)

* Program Issues

The ISW package is due in Australia on 930604. There will be a requirement for approx. 50 VP OTS (Verification Prototype, Off Tool Samples). We need to put an entire system in place to deal with the M10 X 1.0 hexport thread, including production prints, tooling the hexport supplier, obtaining manifolds for Lab and In Process testing, gaging, QC equipment. Status of envelope drawing and parts list should be checked.

THERMAL ISSUES

* High-temperature sensor study

We have not really placed much emphasis on thermal shifts which are sensor-related rather than base-related. One test measuring the ref dim at room and high temp was conducted, which suggested a couple of mils of shift. A better study might be in order. Also, we don't really understand the influence of temperature on the shape of the hatcher curve. It has been proposed that we could characterize the influence of temperature on act and rel by building snap-type devices, and listening for the snap while running the test devices in an environmental chamber.

* Study of low-temp performance using line rejects for high-act

The concern receiving the most focus is the high-temp shifts which tend to make the device go open-circuit, which is an annoyance but is actually failsafe. If low-temp shifts were sufficient to prevent the device from opening on pressure rise, this would be a safety issue. If devices end up pinned statistically too high, they are typically the ones rejected by the pressure tester for high-actuation. Taking some of these and performing low-temperature experiments would help characterize this effect.

* Addition of thermal information to FMEA

DIAPHRAGM LIFE

* Life Test for Tim Andresen w/ 3 mmHg vacuum (ES)

Australia contacted Tim and informed him of the fact that we were concerned about diaphragm life after high-vacuum exposure. Tim asked us the obvious question - what kind of effect did the ES vacuum have? We are running 6 parts w/ ES vac and 6 controls. We told Tim this could be done roughly by the holidays. Presently, 516 vac parts are dead at 913, 1068, 1074, 1194, and 1196 Kcycles. 216 controls are dead at 988 and 1170.

* Rubber diaphragm development

We need to formulate a big-picture strategy in order to justify development efforts. One is to characterize noise with rubber, to work towards snubber elimination. A molded diaphragm supplier, Dia-Com, needs to be contacted. We have prototyped with a lathe-cut design, and produced exemplary diaphragm life results but found the sensor yields are poor due to wide actuation sigma's. This is possibly linked to inconsistent diaphragm compression characteristics.

* Additional diaphragm ideas

Develop experimental material, PEEK (mat'l Andy McKenna - Japan), Dixon polyimide, Allied-Apical competitor to Kapton, Ultem film...

John Brennan's work to characterize film properties under various aging conditions, including saturated brake fluid and trans. fluid...

* Addition of info to DFMEA - leakers begin by going closed-ckt

SBO/921218/file PRIORITY.Y

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TI-NHTSA 7348

PRINTS/DRAFTING

Silent PC P/L chg to 27713-2 and 74247-2; (does not apply yet to 77PSL2-1) ✓
All 77/87 P/L new rivet 74776 ✓
27713 Cup: all updates, silent disc predeflection chg's
36888 Terminal Bassler issues
46515 Base: complete revamp, .083-.095, chg/remove envelope dimension too
?. new radius to address cracking ?
36889 Spring: rivet hole shape, bump dim's and visual, make this print FLAT
36897 Mv term asm: key spring dim's (bent) onto this print
74797 Al cr ring: add wax details
36952 Final asm: correct ht & dia for aluminum crimp ring
36887 Mv term: update cutoff dim
27639 Washer: add radius callout (feeder uses it)

MISCELLANEOUS and CREATIVE BACKLOG (FOR BRAINSTORMING)

- * Obtain Ford factory-fill brake fluid in 55 gal drum
- * Any diff between Ford factory-fill fluid and off the shelf DOT 3 ??
- * F2VC spec - add verbage on prod cyclor like PS spec's
- * Effective area curves - lab crimp vs. production crimp
 - F/d - Pete S. equipment
 - P/d - fixturing for PSM equip rec'd
- * Phone-in cyclor test status ??
- * Stan's stepped hex idea - pinch diaphragm just outside gland
- * Hystat power-steer switch, Chrysler - obtain (show John K)
- * Dale idea for confirmation of correct pin: F/d with continuity signal
- * Silent device: UCON gel to fill cavity for dampening (Norm Freda - source?)
- * Testing of sensor crimping process influence on disc envelope (Mfg Eng)
- * Eliminate environmental seal, chg base to match sensor, elim. cracking
- * Go to larger radius on base flange - elim cracking; better therm stability?

NO M#- 158 FR=VAGS TO=ZIZ SENT=12/21/92 02:10 PM
R#-C P=C DIV=0050 CC=00101 BY=VAGS AT=12/21/92 02:10 PM
TO: 77PS BT MFPC
TOM BURKE MFPC
DICK GARIOPY MFPC

: BILL SWEET WS4
DAVE CZARN ZARN
AZIZ RAHMAN ZIZ
TED BALLARD ETB
TED BREDIKIN TBTV
RUSTY STRUBLE RCS2

FR: MATT SELLERS MTSZ

RE: 36656-35/36656-41 DISC LOTS

FROM NOW ON THE DISC DEPARTMENT WILL BE CHECKING THE 36656 DISC ON A NEW PIECE OF TEST EQUIPMENT CALLED THE AUTOMATIC DISC CHECKER (ADC). FRAN AND I HAVE ALREADY PERFORMED SOME TEST AND HAVE DETERMINED WHAT THE NEW DISC PRESSURES WILL BE WITH THIS NEW ADC SYSTEM. THE PRESSURES MAY HAVE CHANGED SLIGHTLY DUE TO DIFFERENCES BETWEEN THE OLD CHECKER AND THIS NEW ONE. WE FOUND THE FOLLOWING:

| CUP PART NUMBER | DISC PART NUMBER | APPROXIMATE DISC ACTUATION MEAN |
|------------------------|---------------------|---------------------------------------|
| ***** 27713-1 (OLD) | ***** 36656-35 | ***** 22.1 PSI |
| 27713-2 (NEW) | 36656-35 | 26.0 PSI |
| 27288-1 | 36656-41 | 25.5 PSI |

NOTE: RELEASE MEANS ARE "AS REQUIRED" TO MAKE A QUIET DISC.

PLEASE ENSURE THAT THE PROPER KAN BAN CARDS ARE IN PLACE TO ALLOW THESE DISC PRESSURES TO BE ORDERED, AND PLACE ORDERS TO FILL THEM ASAP.

ALWAYS BE AWARE OF WHICH CUP YOU ARE USING OF THE 27713 VARIETY. RIGHT NOW YOU ARE BACK TO USING THE 27713-2 ON THE 77PSL5-2 DEVICE, AND ARE STILL USING THE 27713-1 CUP ON 77PSL3-1'S & 77PSL2-1'S. AS YOU CAN SEE FROM THE CHART ABOVE THE CUP DASH NUMBER CAN HAVE A BIG IMPACT ON ACTUATION MEAN.

REGARDS . . . MATT
11245

TI-NHTSA 7350

-MSG #= 131268 F 005 TO=ZIZ SENT=12/18/92 02:13 PM
R#=077 ST=C DI 050 CC=00101 BY=VAGE AT=12/18/92 02:13 PM

TO: TED BALLARD ETS
TED BREDIKIN TBTV
DAVE VARNEY VRNY

: BILL SWEET PCME
STEVE OFFILER SB01
DAVE CZARN ZARN
AZIZ RAHMAN ZIZ

FR: MATT SELLERS M192

RE: FIRST ISSUE, ADC CHECKED DISC LOTS
=====

WE HAVE COMPLETED PILOTING ONE BOX OF DISC THAT WERE SAMPLED ON THE NEW AUTOMATIC DISC CHECKER, WE USED THIS ONE BOX TO PERFORM PILOTS ON THE LIGHT TRUCK QUIET SWITCH (77PSL3-3), AND THE PASS CAR QUIET SWITCH (77PSL3-1). WE FOUND THE FOLLOWING RESULTS.

| | 77PSL3-1 QUIET PASS CAR ===== | 77PSL3-3 QUIET LIGHT TRUCK ===== |
|---|-------------------------------------|--|
| DISC ACT. MEAN (ADC) | 25.9 | 25.9 |
| DEVICE ACT. MEAN (PROD.) | 149.3 | 253.8 |
| AMPLIFICATION | 5.8 | 9.8 |
| UNDESIRED ACT. MEAN (PROD.) | 127.5 | 250.0 |
| APPX DESIRED DISC ACT. MEAN (ADC) | 22.1 | 25.5 |

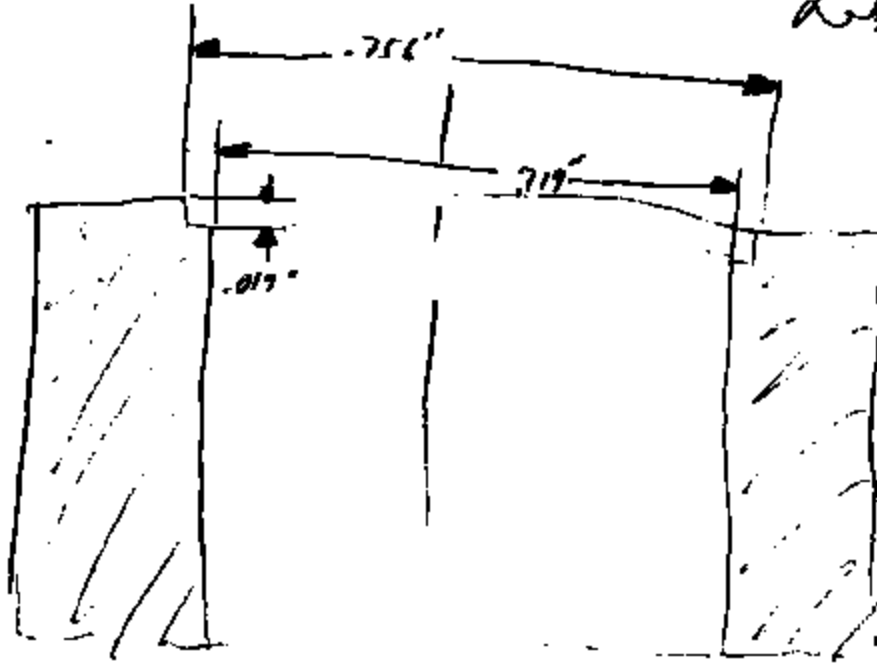
I WILL INSTRUCT THE SMNT TO PLACE ORDERS FOR 36656-35'S WITH AN ACTUATION MEAN OF 22.1 PSI - (RELEASE AS REQUIRED TO MAKE A QUIET SWITCH), AND 36656-41'S WITH AN ACTUATION MEAN OF 25.5 - (RELEASE AS REQUIRED TO MAKE A QUIET SWITCH). NOTE THAT THE DISC WE ALREADY HAVE IN HOUSE WILL MAKE ACCEPTABLE -41'S.

I WOULD ASK THAT YOU MAKE ANY ADJUSTMENTS NECESSARY TO KAN BAN CARDS TO MAKE THESE ACTUATION MEAN ORDERS POSSIBLE.

REGARDS . . . MATT
X1245

TI-NHTSA 7351

Lab Fixture



TI-NHTSA 7352

**DRAWINGS AVAILABLE UPON
REQUEST**

77PSL2-1: Impulse Data Results 11/81 - 12/92

| | | | |
|-----------|-------|----|---|
| 10-Mar-92 | 4,000 | 10 | - |
| 11-Mar-92 | 4,000 | 10 | - |
| 12-Mar-92 | 4,000 | 10 | - |
| 18-Mar-92 | 4,000 | 10 | - |
| 23-Apr-92 | 2,000 | 5 | - |
| 2-May-92 | 2,000 | 5 | - |
| 5-May-92 | 2,000 | 5 | - |
| 6-May-92 | 2,000 | 5 | - |
| 14-Sep-92 | 2,000 | 5 | - |
| 22-Sep-92 | 4,000 | 10 | - |
| 30-Sep-92 | 4,000 | 10 | - |
| 7-Oct-92 | 4,000 | 10 | - |
| 7-Oct-92 | 4,000 | 10 | - |
| 16-Oct-92 | 4,000 | 10 | - |
| 21-Oct-92 | 2,000 | 5 | - |
| 20-Oct-92 | 4,000 | 10 | - |
| 29-Oct-92 | 4,000 | 10 | - |
| 29-Oct-92 | 4,000 | 10 | - |
| 30-Oct-92 | 4,000 | 10 | - |
| 4-Nov-92 | 4,000 | 10 | - |
| 10-Nov-92 | 4,000 | 10 | - |
| 10-Nov-92 | 4,000 | 10 | - |
| 11-Nov-92 | 4,000 | 10 | - |
| 17-Nov-92 | 2,000 | 5 | - |
| 20-Nov-92 | 4,000 | 10 | - |
| 4-Dec-92 | 2,000 | 5 | - |
| 9-Dec-92 | 2,000 | 5 | - |
| 14-Dec-92 | 2,000 | 5 | - |
| 16-Dec-92 | 4,000 | 10 | - |
| 16-Dec-92 | 4,000 | 10 | - |
| 16-Dec-92 | 4,000 | 10 | - |
| 21-Dec-92 | 2,000 | 5 | - |
| 21-Dec-92 | 4,000 | 10 | - |

| | | | |
|---------------|----------------|------------|----------|
| Totals | 268,658 | 668 | - |
|---------------|----------------|------------|----------|

2005 Pre Mark
526 92

| Date | Tested | Good | % | Failure Modes | |
|--------------|--------------|--------------|--------------|---------------|----------|
| Dec-82 | | | | | |
| 12/19 | 19 | 19 | 100.0% | | |
| | 220 | 211 | 95.9% | | |
| | 1685 | 1491 | 88.5% | cont 6 | achi 188 |
| | 50 | 48 | 92.0% | | |
| 12/15 | 1044 | 1042 | 99.8% | | |
| | 708 | 707 | 99.9% | | |
| | 1084 | 1082 | 99.8% | | |
| | 1028 | 1027 | 99.9% | | |
| 12/19 | 409 | 371 | 90.7% | cont 1 | achi 37 |
| | 50 | 50 | 100.0% | | |
| | 1378 | 1258 | 91.3% | cont 7 | achi 113 |
| 12/15 | 540 | 540 | 100.0% | | |
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| | 50 | 50 | 100.0% | | |
| | 932 | 930 | 99.8% | | |
| | 478 | 478 | 100.0% | | |
| | 228 | 228 | 100.0% | | |
| | 72 | 72 | 100.0% | | |
| | 50 | 50 | 100.0% | | |
| | 252 | 251 | 99.6% | | |
| | 632 | 632 | 100.0% | | |
| | 640 | 640 | 100.0% | | |
| 12/15 | 1500 | 1499 | 99.9% | | |
| | 280 | 280 | 100.0% | | |
| | 438 | 438 | 100.0% | | |
| | 179 | 179 | 100.0% | | |
| 12/3 | 50 | 44 | 88.0% | ricr 6 | |
| | 719 | 645 | 89.7% | cont 2 | ricr 72 |
| Total | 15639 | 15481 | 97.1% | | |

77PSL2-1 Yields for 1992

| Date | Tested | Good | % |
|---------------------|---------------|---------------|--------------|
| January-92 | 14341 | 14209 | 99.1% |
| February-92 | 10589 | 10487 | 99.0% |
| March-92 | 26771 | 27980 | 97.5% |
| April-92 | 15827 | 16475 | 97.8% |
| May-92 | 12018 | 11135 | 92.7% |
| June-92 | 23443 | 23133 | 98.7% |
| July-92 | 11835 | 11673 | 98.6% |
| August-92 | 18535 | 18253 | 98.5% |
| September-92 | 11653 | 11582 | 99.0% |
| October-92 | 3838 | 3827 | 99.7% |
| November-92 | 0 | 0 | 0.0% |
| December-92 | 15939 | 15481 | 97.1% |
| Total | 132472 | 128518 | 97.7% |