

EA02025

TEXAS INSTRUMENTS, INC.'S

9/10/03 ATTACHMENT TO ODI

BOX 4, PARTS A - N

PART H

SAMPLE REPORT

(77P5L2-1)

REASON FOR REPORT	VENDOR	P.O.	PART NO.	RE
NEW PART			77P5L2-1	
REPLACEMENT TOOL.	REPORT REQ BY	DATE	INSPECTED BY	DA
CORRECTED TOOL.	E. Rose	4/02/92		4
REPAIRED TOOL.	THE DIMENSIONS INDICATED BELOW REPRESENT TEXAS INSTRUMENTS' FINDINGS REGARDING ACTUAL VALUES FOR ALL CHARACTERISCS MEASURED. IN CASES WHERE ACTUAL VALUES DIFFER FROM THE SPECIFIED DIMENSIONS, THE DISPOSITION MUST INDICATE THE REQUIRED ACTION FOR EACH NON-COMFORMANCE IN THE APPROPRIATE COLUMN.			
REVIEW				
OTHER				

		(CIRCLE ALL OUT OF TOLERANCE DIMENSIONS)				DISPOSITION	
		A	B	C	D		
23	LOW on surface					T.M	
23A	1.80 - 2.212 AX	1 1.651	1.651	1.651	1.651		
23A		2 1.651	1.798	1.651	1.651		
23 24	2.30 - 2.72 AX	1 2.535	2.533	2.494	2.572		
		2 2.726	2.672	2.570	2.519		
24 25	2.15 - 2.42 AX	1 2.213	2.236	2.237	2.271		
25 26	25° ± 2° AX	1 24° 25'	24° 58'	24° 47'	24° 06'		
		2 24° 18'	24° 14'	24° 06'	24° 43'		
26 27	45° ± 2° AX	1 44° 35'	43° 49'	44° 47'	45° 01'		
		2 44° 32'	43° 33'	44° 34'	43° 50'		
27 28	(71.5°) AX	1 72°	71° 31'	71° 20'	72° 01'		
		2 71° 07'	72°	72° 10'	71° 12'		
28 29	1.43 - 1.63 AX	1 1.538	1.538	1.582	1.603		
		2 1.579	1.612	1.602	1.586		
29 30	0.35 - 0.66 AX	1 0.547	0.574	0.571	0.574		
		2 0.592	0.561	0.576	0.558		
		3 0.614	0.574	0.605	0.575		
30 31	0.35 - 0.66 AX	1 0.581	0.571	0.571	0.571		
		2 0.572	0.572	0.572	0.572		
		3 0.572	0.572	0.572	0.572		
31 32	0.86 - 1.12 AX	1 0.975	0.971	0.987	1.041		
		2 1.033	0.978	1.031	1.074		
		3 0.976	0.977	0.981	0.984		
32 33	Team. housing Brown black OK for FLAME Base. TRYING NEW MATERIAL						

REMARKS AND/OR INSTRUCTIONS:

DISPOSITION: TOOL APPROVED FOR PROD.	RESUBMISSION REQ'D
MFG. ENG.:	QRA ENG.:
	PURCH. AGENT:

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- 100. ...

2- COPS QUIET SWITCH

NEXT MEETING:

DATE: MONDAY 4/20
TIME: 9:30
PLACE: CAFETERIA CUBE

P/N	FORD P/N	DESCRIPTION
77PSL3-1	F2AC-9F924-AA	ULTRA-LOW DIFF'L EN53 (CROWN V./GR. MARG.) ~150K/YR
77PSL5-2	F3DC-9F924-AA	ULTRA-LOW DIFF'L W/SNUBBER DN5 (SHO TAURUS) ~20K/YR

DISCUSSION:
1332 77PSL3-1'S GAPPED THROUGH 4/17. HYPOT FREQUENCY
ADJUDGED TO 80 PCS/250. DALE WILL DETERMINE THROUGH
CORRELATION TESTING IF HYPOT TEST IS BEST METHOD TO
DETERMINE LOAD PINS.

17K LOTS NEEDED BY DANA TO REPLACE THEIR L2-1 INVENTORY;
FORD WILL COORDINATE SHIPMENT OF 133K L2-1'S FROM DANA TO
17'S WHO WILL CONTINUE TO SUPPLY L2-1'S ASSEMBLED TO THE
REQUIREMENT FOR THE CAR WHICH HAS 133K.

→ EN53 405 ??

TI-NHTSA 005986

TEST ADD N FACILITIES
ADD IN INTENT SNLZ. HEXS. BY 4/27

10000
JTC MIS MAKING FINALS FROM
ULCO BLANKS 72 80-00

MARKETING/FIELD SALES

PLEASE WITH LIT ON LTR. TEMP ISSUE
AND THEIR BEING FOR UNIT SWITCH

FREEBAY
DOUGLAS

STEIN ENG.

ITEMS:

1. DARE (ADD -S AS NAT'L MORYL/OFFSET)
2. DISC (NEW SET-UP)
3. ENVELOPE DRAWINGS (WHEN REQUESTED)
PARTS LISTS (UPDATE)
1. START W/ HAND MARKED COPY)
WEIBULL TESTING FOR M. SPEARS
CHECK LIT QUIET DISCS
LIT'S BELOW DIFFIC. WITH AND
WITHOUT SNUBBERS TO SENDY BY 4/24
LIT QUIET SWITCHES TO SENDY; 3 W/
AND SWITCHES BY 5/31; DARK MORYL
BASE (NEED TO REASSASS DATE, DETERMINING
IN SENDY EVALYN OF SWITCHES WITH AND
WITHOUT SNUBBERS)

CZARN
SODGE
CZARN
CZARN

OFFILER
SODGE
OFFILER CANCEL

OFFILER EN'S - STYLE; LITE TRIC...
QUIET TRIC DISC W/ NORMAL HEX
100 IN MAY; 100 IN JUNE

MANUFACTURING ENG./MECHANIZATION

PROCESS SPECS
SET-UP SPC FILES
REVIEW PFMEA
PRIORITIZE MECH. WORK
- SOFTWARE CHANGES TO G.A.M.
ADD HYPOT TO P-TESTER ?
MODIFY TRAPPED DISC PROBE FOR EACH
LOT OF SENSORS ?
CHK FOR SOUND ON P-TESTER ?
O PSIG CONTINUITY CHECK

SELLERS
SELLERS
SELLERS
KOURTESIS
KOURTESIS
SELLERS
SELLERS
SELLERS
SELLERS

SO MFG. ENG.

CHK LIT QUIET DISCS

SODGE

MANUFACTURING

AUTTY

REHABING

HAVE ELCO QUOTE SNUBBER W/2nd OPS

KOTCH

ASTING

PRIORITIZE DWG AND P/L CHANGES AS
THEY COME THROUGH

SAVLS,
VE CZARN

TI-NHTSA 005987

CRITICAL ITEMS:

TEST ROOM N FALL 82
PROD N INTENT ENCL. DESAL BY 2407
DATE: 4/20/92 04:12 PM
FROM: DAVID DZARN 00-0001 5742AM 4/20/92 04:12 PM

FROM: 20, 1992
TO: STEVE OFFICER 3801
BILL SWEET WSA
MATT WELLS M322
JIM WATT PCQA
BOB ORLEBY AF70
DALE BOBLE AF01
TOD BALLARD ET9
MIKE DEBATTIA 703
NORM FREDA WMLZ
RUSTY STRUBLE R052
CHARLIE DOUGLAS CMF1
CLAIRE BALHAZAR PCME

CC: TOM CHARBONEAU TC
RAY FOURANGEAU RGT2
ANDY MEGUIRK PCQA
BILL CONNOR MFPC
JOHN NOLRTEGIO MDES
JIM KERN MLDO
STEVE WALTERS MLDG
JEFF GIOMENICO EL3
GARY SNYDER CPPC
STEVE MAJOR SMFH
DICK MULHERN PCTL

FR: DAVE DZARN ZARN

RE: COPS QUIST SWITCH - 4/20 MTG. MINUTES

NEXT MEETING:

DATE: TUESDAY 4/21
TIME: 3:30
PLACE: CAFETERIA CUBE

TI P/N	FORD P/N	DESCRIPTION
77PBL3-1	F2AC-9F924-AA	ULTRA-LOW DIFF'L EN53 (CROWN V./GR. MARQ.) ~150K/YR
77PBL5-2	F3DC-9F924-AA	ULTRA-LOW DIFF'L W/SMUBBER DN5 (SHO TAURUS) ~20K/YR

DISCUSSION:
5206 77PBL3-1'S SHIPPED THROUGH 4/17. (LAST MSG. WAS
INCORRECT.)

PROD'N P-TESTER LIMITS TIGHTENED FOR A FEW DAY TRIAL
PERIOD TO DETERMINE IF PIN EXTREMES CAN BE FOUND
THROUGH PRESSURE READINGS RATHER THAN HYDPT. WILL
REVIEW AGAIN WEDNESDAY.

4/20/92

TI-NHTSA 005986

CRITICAL ITEMS

TEST PROGRAM FAILURES
PROGRAM INTENT BRUB. REXP. BY 4/27 KOTCH

MARKETING/FIELD SALES

CLOSE WITH L/T ON HIGH TEMP ISSUE
AND FIELD NEEDS FOR QUIET SWITCH FREDAY
DOUGLAS

DESIGN ENG.

PRINTS:
P BASE (ADD -3 AS NAT'L NORYL/OFFSET) CZARN
P DISC (NEW SET-UP) SOGGE
- ENVELOPE DRAWINGS (WHEN REQUESTED) CZARN
PARTS LISTS (UPDATE) CZARN
WEIBULL TESTING FOR M. SPEARS OFFILER
CHECK L/T QUIET DISCS SOGGE
100 L/T QUIET SW'S (L3-113) TO SENDIX
- BUILD/CAL BULK NORYL BASES BY 4/27 BALTHAZAR
- DETERMINE FIN TARGET BY 4/24 SOGGE
- BUILD SWITCHES AND SHIP BY 4/30 BALTHAZAR

MANUFACTURING ENG./MECHANIZATION

PROGRESS SPECS BALTHAZAR
SET-UP SPC FILES BALTHAZAR
REVIEW PFMEA SELLERS
COORDINATE MECHANIZATION WORK FOR SELLERS
QUIET SWITCH
O PSIG CONTINUITY CHECK SELLERS

ISO MFG. ENG.

MANUFACTURING

QUALITY

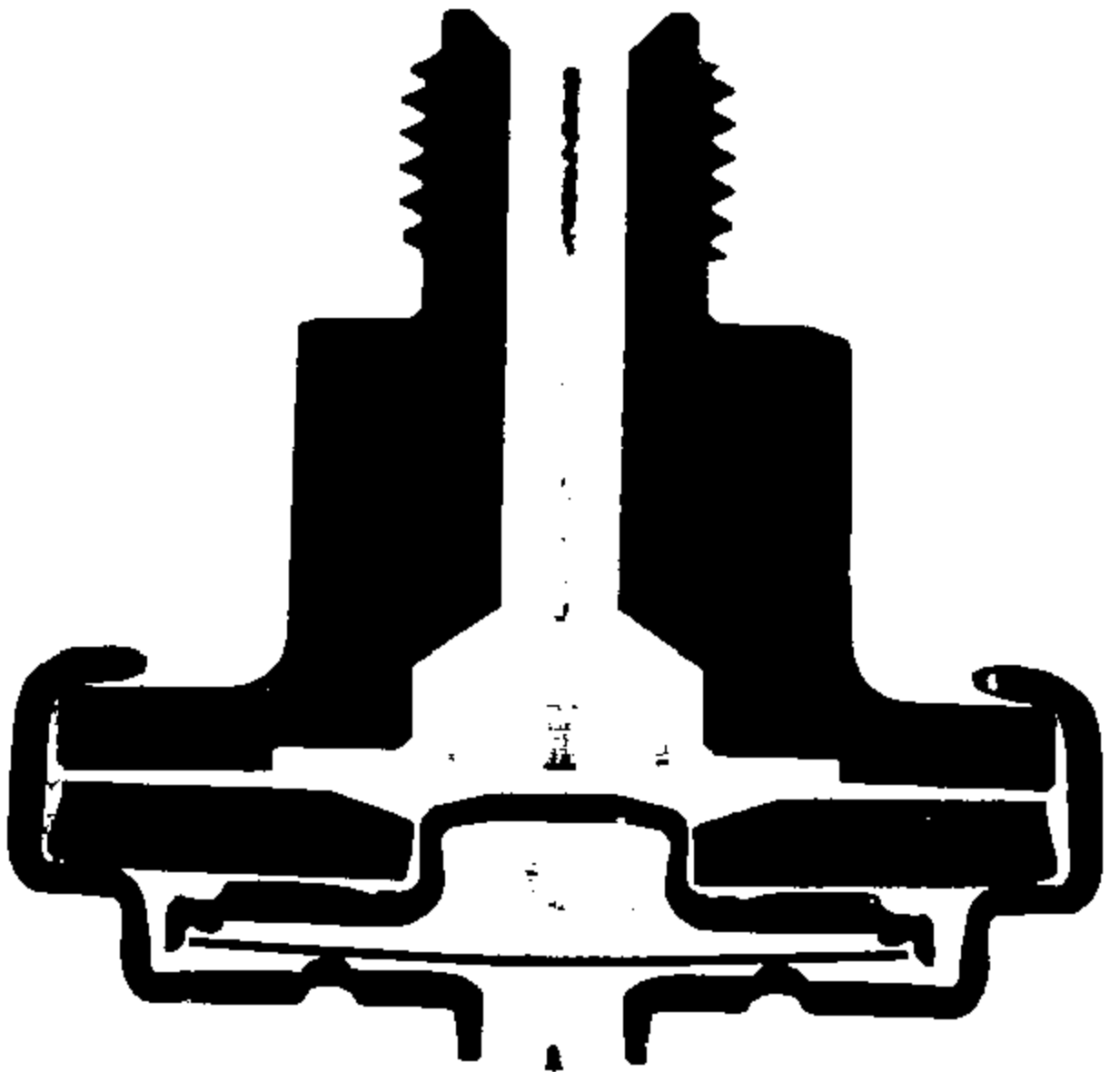
PROCURING

HAVE ELCO QUOTE SNUBBER W/2nd OPS KOTCH

RAFTING

PRIORITIZE DWG AND P/L CHANGES AS
THEY COME THROUGH MULHERN

BOARDS,
AVE CZARN
3-QUIET



4.5 MIL
INCREASED
IRE LOAD

**TEXAS INSTRUMENTS, INC. ISIR SUBMISSION
TO DANA CORPORATION
FOR PART NUMBER F2AC-9F924-AA (77PSL3-1)**

4-21-92

PER CONVERSATION/MATT SELLERS:
REWORK & REMEASURE
2, 3, 4, 6

4-21-92

39

REWORKED + REMEASURED

Dim. # 3

#2 ~~0.278~~ 0.310 mm
~~0.418~~ 0.452 mm

#3
0.641 mm
0.425 mm

#4 0.531 mm
0.591 mm

#6 0.635 mm
0.475 mm

Term. Pos. 0.75 / 0.25 mm

SAMPLE REPORT

REASON FOR REPORT	VENDOR	P.O.	PART NO.	REV.
NEW PART			77P5L3-1	A
REPLACEMENT TOOL.	REPORT REQ. BY	DATE	INSPECTED BY	DATE
CORRECTED TOOL.	Elaine Rose	4/14/92	Sandy Gilbert	4/6
REPAIRED TOOL.	THE DIMENSIONS INDICATED BELOW REPRESENT TEXAS INSTRUMENTS' FINDINGS REGARDING ACTUAL VALUES FOR ALL CHARACTERISTICS MEASURED. IN CASES WHERE ACTUAL VALUES DEVIATE FROM THE SPECIFIED DIMENSIONS, THE DISPOSITION MUST INDICATE THE REQUIRED ACTION EACH NON-CONFORMANCE IN THE APPROPRIATE COLUMN.			
REVIEW				
OTHER <u>Dim analysis</u> <input checked="" type="checkbox"/>				

Dimension	(CIRCLE ALL OUT OF TOLERANCE DIMENSIONS)						DISPOSITION	
	1	2	3	4	5	6	Method of inspection	
1 1.85 - 2.06	1.933	1.933	1.942	1.956	1.900	1.827	Trmic	
2 ϕ 19.05 max	18.657	18.652	18.653	18.733	18.733	18.683	"	
3 .25 - .75	0.593	0.561	0.552	0.522	0.558	0.548	"	reme
4 2.79 - 3.10 2 pks	2.748	2.804	2.752	2.805	2.684	2.807	"	
	2.90	2.90	2.91	2.92	2.91	2.91	Cal	
	2.91	2.92	2.93	2.94	2.92	2.94	"	
5 19.45 - 19.81	19.65	19.70	19.71	19.73	19.75	19.73	"	
6 11.40 - 11.90	11.794	11.797	11.791	11.790	11.784	11.883	Trmic	
7 16.56 - 16.76	16.623	16.652	16.636	16.654	16.626	16.628	"	
8 2.84 - 3.05	2.936	2.948	2.927	2.924	2.910	2.919	"	
ϕ 0.1 ϕ A	0.035	0.017	0.018	0.006	0.043	0.030	"	
9 1.24 - 1.45	1.241	1.242	1.249	1.260	1.270	1.258	"	
10 11.60 - 11.92	11.864	11.719	11.725	11.681	11.682	11.736	"	
11 1.24 - 1.55	1.384	1.397	1.393	1.397	1.425	1.388	"	
12 57.15 max	55.64	55.65	55.69	55.75	55.75	55.71	Cal	
13 12.59 - 13.11	12.824	12.862	12.914	12.933	12.850	12.906	Trmic	
14 11.65 - 12.17	12.023	12.025	12.146	12.126	12.068	12.181	"	
	11.963	11.823	12.056	12.081	12.011	12.055	"	
15 6.60 - 6.81	6.702	6.696	6.690	6.690	6.708	6.722	Trmic	
16 NO Flash or Burs on this surface.	OK	OK	OK	OK	OK	OK	Visual	
17 2.79 - 3.41	3.053	3.164	3.162	3.205	3.187	3.25	Comp	
18 0.68 - 1.30	1.137	1.066	1.153	1.165	1.071	1.117	"	
19 Stamp date code & Ford PA.	OK	OK	OK	OK	OK	OK	Visual	

REMARKS AND/OR INSTRUCTIONS:

DISPOSITION: TOOL APPROVED FOR PROD.	RESUBMISSION REQ'D
MPG. ENG.:	QRA ENG.:
	PURCH. AGENT:

SAMPLE REPORT

F2AC-9E924-AA

REASON FOR REPORT	VENDOR		P.O.	PART NO.	REV.
NEW PART				77PSL3-1	1
REPLACEMENT TOOL.	REPORT REQ BY	DATE	INSPECTED BY		DATE
CORRECTED TOOL.	Elaine Rose	4/14/82	Sandy Gilbert		4/16
REPAIRED TOOL.	THE DIMENSIONS INDICATED BELOW REPRESENT TEXAS INSTRUMENTS' FINDINGS REGARDING ACTUAL VALUES FOR ALL CHARACTERISCS MEASURED. IN CASES WHERE ACTUAL VALUES DEV FROM THE SPECIFIED DIMENSIONS, THE DISPOSITION MUST INDICATE THE REQUIRED ACTION EACH NON-CONFORMANCE IN THE APPROPRIATE COLUMN.				
REVIEW					
OTHER <u>Dim analysis</u> X					

Dimension	(CIRCLE ALL OUT OF TOLERANCE DIMENSIONS)					DISPOSITION		
	1	2	3	4	5	6	METHOD OF INSPECTION	
20 3/8-24 UNF 2A	OK	OK	OK	OK	OK	OK	PSM	
3667-.3739 diam	3715	3725	3710	3715	3705	3710	Cal	
21 1.10-1.40	1.224			section			TIME	
22 .25	OK			section			WATER	
23 \nearrow 0.16 ϕ diam by spec								
24 41°-43°								TIME
25 40°-50° cham								COMP
26 ϕ 7.82-8.03								"
27 1.52-2.04								"
28 9.39-9.66								"
29 8.12 min								"
30 14.23 max								"
31 ϕ 32.51 max	#1							"
32 ϕ 5.58-5.85								"
33 ϕ 7.23-7.37								"
34 ϕ 3.30-3.60	#2							"
35 ϕ 14.0-14.5 H								"
36 0.58-0.68 2p								"
37 2.59-2.80 2 pl	#3							"
ϕ 0.25 ϕ AE	#4							"
38 8.30-8.72 2p								"
39 25° \pm 4 2 p/c	#5							"

Dim #23 \nearrow 0.16 ϕ

#1 .0005" = .0127 mm

#2 .0001 = .00254

#3 .001 = .0254

#4 .0004 = .010

#5 .0005 = .0127

#6 .0006 = .01524

REMARKS AND/OR INSTRUCTION

DISPOSITION: TOOL APPROV

MPG. ENG.:

SAMPLE REPORT

REASON FOR REPORT	VENDOR	P.O.	PART NO.	REV.
NEW PART			77P5L3-1	6
REPLACEMENT TOOL.	REPORT REQ. BY	DATE	INSPECTED BY	DATE
CORRECTED TOOL.	Elaine Rose	4/14/92	Sandy Gilbert	4/2
REPAIRED TOOL.	THE DIMENSIONS INDICATED BELOW REPRESENT TEXAS INSTRUMENTS' FINDINGS REGARDING ACTUAL VALUES FOR ALL CHARACTERISTICS MEASURED. IN CASES WHERE ACTUAL VALUES DEVIATE FROM THE SPECIFIED DIMENSIONS, THE DISPOSITION MUST INDICATE THE REQUIRED ACTION EACH NON-CONFORMANCE IN THE APPROPRIATE COLUMN.			
REVIEW				
OTHER <u>Dim analysis</u> <input checked="" type="checkbox"/>				

Dimension	(CIRCLE ALL OUT OF TOLERANCE DIMENSIONS)						DISPOSITION	
	1	2	3	4	5	6	number of features	
39 cont	24° 21'	23° 36'	23° 42'	22° 49'	24° 28'	23° 26'	1	comp
40 Housing to be natural in color	OK	OK	OK	OK	OK	OK	1	visual
41 [71.5°] 2 pics	71° 49'	71° 25'	72° 21'	71° 45'	71° 43'	71° 44'	1	comp
	72° 37'	72° 21'	72° 14'	72° 30'	72° 5'	72° 36'	1	

REMARKS AND/OR INSTRUCTIONS:

DISPOSITION: TOOL APPROVED FOR PROD.	RESUBMISSION REQ'D
MFG. ENG.:	QRA ENG.:
	PURCH. AGENT:

**DRAWINGS AVAILABLE UPON
REQUEST**

TEXAS INSTRUMENTS INCORPORATED
CONTROL PRODUCTS DIVISION
ATTLEBORO, MASSACHUSETTS 02703

QUALITY ASSURANCE WORK ORDER

* INDICATE TYPE OF SERVICE REQUESTED:

NOTICE: TWO COPIES OF THE DRAWING MUST
BE INCLUDED WITH YOUR REQUEST.

IMPORTANT: SUPPLIER F.A.I. INCLUDED WITH
THIS REQUEST: YES/NO ? _____

FIRST ARTICLE INSPECTION
 PARTIAL "FAI"
 TOOLPROOF
 DIMENSIONAL ANALYSIS
 MACHINE CAPABILITY
 PROCESS CAPABILITY

* INDICATE ONE OF THE FOLLOWING REASONS:

(F2AC-9F934-AA)

NEW PART / NEW TOOL / MOLD
 CORRECTED TOOL / MOLD
 OTHER _____

* PART NUMBER: 77PSL3-1

DRAWING REVISION: A

NUMBER OF CAVITIES / STATIONS

6 TOOL ID: _____

TYPE OF MATERIAL: Noryl

PART DESCRIPTION: PRESSURE SWITCH

SUPPLIER: _____

SAMPLE / MOLD DATE: _____

* DATE SUBMITTED: 4-14-92 DATE REQUIRED: 4/24/92

REQUESTED BY: ELAINE ROSE M/S: 12-27

COST CENTER: 149 PRODUCT CODE: 88 EXT: 1907

PRIORITY (INDICATE ONE): URGENT * AS DATED

** "URGENT" PRIORITY REQUIRES MANAGERS APPROVAL

APPROVED BY (IF REQUIRED): M. D. Watts

ENGINEERING SPECIAL INSTRUCTIONS

NOTES

- 1.) A "FIRST ARTICLE INSPECTION", "PARTIAL F.A.I.", OR A "TOOLPROOF", ALL REQUIRE A "DISPOSITION" FROM THE MATERIALS REVIEW BOARD, INCLUDING ALL APPROPRIATE SIGNATURES. ALSO, THE DISPOSITIONED COPY MUST BE RETURNED TO RECEIVING INSPECTION CC146 FOR PROPER RECORDING.
- 2.) RECORDS: A) COPIES OF ALL "FIRST ARTICLE INSPECTIONS" (INCLUDING PARTIALS) WILL BE RETAINED BY RECEIVING INSPECTION FOR SEVEN YEARS.
B) RECORDS OF ALL OTHER ANALYSIS WILL NOT BE RETAINED BY RECEIVING INSPECTION.
- 3.) "DIMENSIONAL ANALYSIS": ANY REQUEST FOR A DIMENSIONAL ANALYSIS THAT INCLUDES ALL DIMENSIONS, OR ALL "CRITICAL" & "MAJOR" DIMENSIONS, WILL BE CONSIDERED A "FIRST ARTICLE INSPECTION" OR A "TOOLPROOF", AND WILL REQUIRE DISPOSITION BY THE MATERIALS REVIEW BOARD. THE APPROVED COPY MUST BE RETURNED TO RECEIVING INSPECTION CC146.

QUALITY ASSURANCE

DATE REC. I: _____

EST. HRS. I: _____

COMPLETED: _____

BY: _____

RECEIVING INSPECTION

77PSL3-1

Oct. 90 - 160 psi

6-29-92

Data obtained Apr. 16 '92

pg. 1 of 2

1	129.2	125.9	131.4	* 178.0	127.6	141.4
2	139.4	127.2	132.6	139.2		140.5
3	129.7	123.3	138.2	129.4		130.8
4	134.0	131.2	125.9	131.6		138.7
5	140.5	122.5	140.4	132.5		133.4
6	134.7	133.5	133.8	136.1		131.7
7	130.7	138.9	132.4	130.4		134.6
8	123.3	138.0	139.1	134.1		129.9
9	139.4	120.8	127.6	125.0		128.4
10	124.9	122.5	137.5	130.4		126.5
11	132.4	128.1	131.3	133.2		132.9
12	127.8	135.3	129.0	131.0		126.0
13	143.6	137.1	125.3	127.2		129.8
14	124.1	135.8	133.2	133.2		133.3
15	134.7	136.9	130.4	137.2		136.9
16	137.3	129.3	124.3	129.3		127.2
17	131.0	140.6	132.4	126.7		133.4
18	136.8	135.5	123.1	125.3		125.0
19	136.8	131.3	119.8	122.3		139.7
20	133.3	132.8	132.4	126.5		125.3
21	139.0	134.0	135.2	127.1		134.7
22	128.2	127.4	130.6	123.6		127.5
23	131.6	130.4	128.2	134.0		126.6
24	141.3	122.0	* (177.8)	143.6	142.9	133.8
25	120.7	122.7	128.5	135.9		132.5
26	133.6	125.9	129.4	134.5		129.9
27	131.7	127.0	125.4	132.2		133.5
28	127.5	126.0	131.2	128.0		126.6
29	132.1	129.3	134.4	131.7		124.9
30	128.3	138.6	131.3	126.3		127.2
31	126.9	127.3	129.5	131.7		126.3
32	132.6	121.7	128.2	128.5		130.8
33	134.5	129.2	137.2	133.1		119.2
34	130.5	131.6	128.7	131.7		128.9
35	128.3	131.6	129.1	123.3		129.3
36	126.7	117.2	127.3	135.3		128.7
37	135.6	130.4	128.1	129.9		126.6
38	131.7	119.2	130.7	132.6		132.4
39	137.6	128.0	132.8	135.8		132.4
40	133.5	133.9	129.9	125.0		126.9
41	124.9	126.1	127.7	128.7		135.2
42	128.4	126.1	118.7	122.4		131.0
43	125.9	132.5	124.4	136.0		126.5
44	131.9	129.3	131.7	133.3		136.0
45	129.9	137.2	138.3	130.6		138.9
46	126.3	125.6	126.6	122.1		130.4
47	129.2	132.4	131.5	138.4		126.4
48	134.0	132.9	128.0	129.8		139.3
49	131.2	123.6	132.2	133.1		126.4
50	133.2	124.6	131.0	132.7		137.5

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Oct.

6-21-12

Data obtained Apr. 16 '92

pg. 2 of 2

1	131.7								
2	128.2								
3	131.7								
4	134.4								
5	137.1								
6	120.5								
7	130.3								
8	133.4								
9	124.2								
10	133.9								
11	133.7								
12	130.6								
13	128.1								
14	128.9								
15	130.9								
16	133.3								
17	127.2								
18	130.8								
19	129.5								
20	130.3								
21	142.8								
22	126.1								
23	127.1								
24	130.7								
25	134.7								
26	127.6								
27	127.2								
28	123.1								
29	129.9								
30	125.2								
31	130.5								
32	123.6								
33	131.3								
34	134.2								
35	131.5								
36	137.6								
37	125.6								
38	129.1								
39	133.1								
40	136.6								
41	129.4								
42	137.5								
43	129.9								
44	125.2								
45	134.0								
46	122.9								
47	131.0								
48	123.2								
49	123.2								
50	126.9								

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Rel. 20-120 psi

6-27-72

Data obtained Apr. 16 '92

pg. 140

1	100.0	87.1	95.9	*	140.7	89.5	111.0
2	104.0	95.2	90.2		97.1		111.0
3	88.1	92.4	103.8		95.8		106.3
4	98.6	93.5	91.4		99.9		104.0
5	111.6	85.6	113.1		99.9		98.3
6	102.0	98.4	100.6		102.3		102.2
7	98.1	103.9	94.4		96.6		102.2
8	84.2	107.9	105.9		97.8		100.9
9	105.3	87.1	100.8		91.8		97.6
10	90.2	88.1	107.9		96.6		95.1
11	97.1	94.5	100.8		92.4		96.3
12	99.8	101.8	97.0		97.0		94.2
13	100.0	104.8	92.2		93.3		97.4
14	92.6	103.3	102.1		95.7		97.4
15	106.4	104.6	98.2		102.3		104.1
16	105.3	90.9	93.6		98.3		93.7
17	95.9	104.6	104.7		93.2		102.5
18	106.1	104.6	89.9		86.7		92.7
19	107.7	93.6	88.7		98.1		108.2
20	98.2	94.5	98.2		90.9		90.3
21	108.9	102.1	107.8		94.4		103.5
22	98.4	92.4	93.8		96.7		94.6
23	93.6	100.1	* 96.0	112.8	100.3		94.6
24	106.5	94.1	92.6		112.3		101.1
25	85.3	89.4	96.1		105.3		98.0
26	98.1	89.4	89.6		100.3		90.3
27	97.0	91.8	94.1		101.0		105.4
28	97.0	91.8	94.1		98.4		89.3
29	99.6	100.7	107.6		97.2		92.3
30	100.9	107.5	100.8		92.3		93.5
31	91.0	93.3	97.1		97.7		90.0
32	95.8	89.8	94.6		96.4		97.1
33	103.7	94.5	106.1		101.5		82.4
34	99.5	99.6	96.9		101.1		95.0
35	99.5	96.7	99.5		90.4		95.0
36	88.6	83.0	91.8		104.0		96.3
37	104.5	99.4	103.5		97.6		93.8
38	98.1	90.8	97.1		102.6		98.7
39	105.9	96.4	102.5		106.3		99.9
40	101.9	99.9	93.5		90.4		92.6
41	94.7	93.8	96.6		95.2		101.3
42	103.4	92.6	87.2		100.0		99.3
43	93.4	97.4	88.5		102.9		93.9
44	100.9	94.9	104.6		98.0		103.0
45	97.2	103.8	108.9		100.4		104.2
46	93.8	90.2	95.8		90.6		100.2
47	96.3	96.9	97.3		102.9		96.4
48	100.1	102.2	92.4		95.5		108.1
49	101.4	87.2	102.1		104.1		92.3
50	98.8	89.7	98.3		101.6		109.2

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Cal.

Data obtained Apr. 16 '92

pg. 2 of 2

1	102.4
2	92.3
3	100.8
4	99.5
5	100.8
6	87.5
7	95.2
8	100.1
9	98.8
10	101.2
11	101.4
12	102.8
13	92.7
14	101.4
15	95.9
16	101.0
17	92.5
18	95.9
19	93.7
20	98.5
21	107.8
22	94.9
23	91.1
24	97.2
25	104.8
26	97.2
27	93.6
28	89.0
29	96.1
30	88.0
31	100.6
32	93.2
33	96.8
34	100.6
35	99.6
36	103.6
37	89.8
38	99.6
39	98.5
40	101.0
41	99.6
42	103.6
43	95.5
44	93.0
45	104.4
46	87.3
47	99.7
48	99.6
49	97.5
50	91.8

17-APR-1992 09:43:52.33 OPER DOOR DID NOT CLOSE 1

17-APR-1992 09:44:12.33 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 09:44:29.55 TOOL CYCLE TIMEOUT 1

77PS PRESSURE TESTER LOT REPORT

RATING: 77PSL2-1

LOT ID: MASTERS

LOT STARTED: 17-APR-1992 09:43:29.56

LOT FINISHED: 17-APR-1992 10:11:04.07

SETUP DATA:

DISC LOT ID: 0.00

DISC MEAN ACT: 23.4 MEAN REL: 12.7

LIMIT (NC)

ACTUATION: 90.0 TO 160.0 PSI

RELEASE: 20.0 TO 120.0 PSI

DIFFERENTIAL: 0.0 TO 160.0 PSI

MAX MILLIVOLT: 500.0 PSI

ACT CREEP TIME: 25.0 PSI

REL CREEP TIME: 150.0 PSI

PRECYCLE PRESS: 800.0 PSI

PRECYCLE COUNT: 2

NOT ENOUGH PARTS FOR REPORT ON FIXTURE 0

SER 1; FIX 1; C= 000000; SIN=8000; WRLU=43.7; WRRD=47.4; LEAK RATE= 2.0
ACT= 129.2; REL= 100.0; DIF= 29.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 2; FIX 2; C= 000000; SIN=8000; WRLU=43.7; WRRD=47.4; LEAK RATE= 2.0
ACT= 139.4; REL= 104.0; DIF= 35.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 3; FIX 3; C= 000000; SIN=8000; WRLU=43.7; WRRD=47.4; LEAK RATE= 2.0
ACT= 129.7; REL= 88.1; DIF= 41.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 4; FIX 4; C= 000000; SIN=8000; WRLU=43.7; WRRD=47.4; LEAK RATE= 2.0
ACT= 134.0; REL= 98.6; DIF= 35.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:11:26.79 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:11:46.79 OPER DOOR STILL DID NOT CLOSE 1

SER 5; FIX 1; C= 000000; SIN=8000; WRLU=44.1; WRRD=48.2; LEAK RATE= 2.0
ACT= 140.5; REL= 111.6; DIF= 28.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 6; FIX 2; C= 000000; SIN=8000; WRLU=44.1; WRRD=48.2; LEAK RATE= 2.0
ACT= 134.7; REL= 102.0; DIF= 32.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 7; FIX 3; C= 000000; SIN=8000; WRLU=44.1; WRRD=48.2; LEAK RATE= 2.0
ACT= 138.7; REL= 98.1; DIF= 32.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 8; FIX 4; C= 000000; SIN=8000; WRLU=44.1; WRRD=48.2; LEAK RATE= 2.0
ACT= 123.5; REL= 84.2; DIF= 39.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:12:34.38 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:12:54.38 OPER DOOR STILL DID NOT CLOSE 1

SER 9; FIX 1; C= 000000; SIN=8000; WRLU=44.1; WRRD=48.1; LEAK RATE= 2.0
ACT= 139.4; REL= 105.3; DIF= 34.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

10 SER 10; FIX 2; C= 000000; SIN=8000; WRLU=44.1; WRRD=48.1; LEAK RATE= 2.0
ACT= 124.9; REL= 90.2; DIF= 34.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 11; FIX 3; C= 000000; SIN=8000; WRLU=44.1; WRRD=48.1; LEAK RATE= 2.0

ACT= 157.8; REL= 99.8; DIF= 28.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:22:25.46 OPER DOOR DID NOT CLOSE 1

SER 13; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.3; LEAK RATE= 1.9
ACT= 132.6; REL= 100.0; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 14; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.3; LEAK RATE= 1.9
ACT= 129.1; REL= 92.6; DIF= 36.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 15; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.3; LEAK RATE= 1.9
ACT= 134.7; REL= 106.4; DIF= 28.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 16; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.3; LEAK RATE= 1.9
ACT= 137.3; REL= 105.3; DIF= 32.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:23:09.05 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:23:29.05 OPER DOOR STILL DID NOT CLOSE 1

SER 17; FIX 1; C= 0000000; BIN=GOOD; MRRU=43.7; MRRD=48.1; LEAK RATE= 1.7
ACT= 131.0; REL= 95.9; DIF= 35.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 18; FIX 2; C= 0000000; BIN=GOOD; MRRU=43.7; MRRD=48.1; LEAK RATE= 1.7
ACT= 136.8; REL= 106.1; DIF= 30.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 19; FIX 3; C= 0000000; BIN=GOOD; MRRU=43.7; MRRD=48.1; LEAK RATE= 1.7
ACT= 136.8; REL= 107.7; DIF= 29.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

20 SER 20; FIX 4; C= 0000000; BIN=GOOD; MRRU=43.7; MRRD=48.1; LEAK RATE= 1.7
ACT= 133.3; REL= 98.2; DIF= 35.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 21; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.2; LEAK RATE= 1.9
ACT= 139.0; REL= 108.9; DIF= 30.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 22; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.2; LEAK RATE= 1.9
ACT= 128.6; REL= 98.4; DIF= 36.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

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SER 24; FIX 4; C= 000000; BIN=8000; MFRU=44.1; MFRD=47.2; LEAK RATE= 1.9
ACT= 141.3; REL= 106.5; DIF= 34.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 25; FIX 1; C= 000000; BIN=8000; MFRU=44.4; MFRD=48.5; LEAK RATE= 2.2
ACT= 120.7; REL= 85.3; DIF= 35.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 26; FIX 2; C= 000000; BIN=8000; MFRU=44.4; MFRD=48.5; LEAK RATE= 2.2
ACT= 130.0; REL= 98.1; DIF= 35.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 27; FIX 3; C= 000000; BIN=8000; MFRU=44.4; MFRD=48.5; LEAK RATE= 2.2
ACT= 131.7; REL= 97.0; DIF= 34.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 28; FIX 4; C= 000000; BIN=8000; MFRU=44.4; MFRD=48.5; LEAK RATE= 2.2
ACT= 127.5; REL= 97.0; DIF= 30.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 29; FIX 1; C= 000000; BIN=8000; MFRU=44.2; MFRD=47.9; LEAK RATE= 2.2
ACT= 132.1; REL= 99.6; DIF= 32.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

30 SER 30; FIX 2; C= 000000; BIN=8000; MFRU=44.2; MFRD=47.9; LEAK RATE= 2.2
ACT= 128.3; REL= 100.9; DIF= 27.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 31; FIX 3; C= 000000; BIN=8000; MFRU=44.2; MFRD=47.9; LEAK RATE= 2.2
ACT= 126.9; REL= 91.0; DIF= 35.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 32; FIX 4; C= 000000; BIN=8000; MFRU=44.2; MFRD=47.9; LEAK RATE= 2.2
ACT= 132.6; REL= 95.5; DIF= 36.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:25:28.45 GPER DOOR DID NOT CLOSE 1

SER 33; FIX 1; C= 000000; BIN=8000; MFRU=44.2; MFRD=48.6; LEAK RATE= 1.9
ACT= 134.5; REL= 103.7; DIF= 30.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 34; FIX 2; C= 000000; BIN=8000; MFRU=44.2; MFRD=48.6; LEAK RATE= 1.9
ACT= 130.5; REL= 95.5; DIF= 31.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 36; FIX 4; C= 000000; BIN=GOOD; MRRL=44.2; MRRD=46.6; LEAK RATE= 1.9
ACT= 123.7; REL= 88.6; DIF= 35.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 37; FIX 1; C= 090000; BIN=GOOD; MRRL=44.1; MRRD=46.4; LEAK RATE= 2.0
ACT= 135.6; REL= 104.5; DIF= 31.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 38; FIX 2; C= 000000; BIN=GOOD; MRRL=44.1; MRRD=46.4; LEAK RATE= 2.0
ACT= 131.7; REL= 98.1; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 39; FIX 3; C= 000000; BIN=GOOD; MRRL=44.1; MRRD=46.4; LEAK RATE= 2.0
ACT= 139.6; REL= 105.9; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

40 SER 40; FIX 4; C= 000000; BIN=GOOD; MRRL=44.1; MRRD=46.4; LEAK RATE= 2.0
ACT= 133.3; REL= 101.9; DIF= 31.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:26:35.20 OPER DOOR DID NOT CLOSE 1

SER 41; FIX 1; C= 000000; BIN=GOOD; MRRL=44.1; MRRD=47.7; LEAK RATE= 1.9
ACT= 124.9; REL= 94.7; DIF= 30.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 42; FIX 2; C= 000000; BIN=GOOD; MRRL=44.1; MRRD=47.7; LEAK RATE= 1.9
ACT= 128.4; REL= 103.4; DIF= 24.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 43; FIX 3; C= 000000; BIN=GOOD; MRRL=44.1; MRRD=47.7; LEAK RATE= 1.9
ACT= 125.5; REL= 93.4; DIF= 32.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 44; FIX 4; C= 000000; BIN=GOOD; MRRL=44.1; MRRD=47.7; LEAK RATE= 1.9
ACT= 131.9; REL= 100.9; DIF= 31.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:27:06.17 OPER DOOR DID NOT CLOSE 1

SER 45; FIX 1; C= 000000; BIN=GOOD; MRRL=44.2; MRRD=47.5; LEAK RATE= 2.0

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SER 46; FIX 4; C= 0000000; BIN=8000; MRRL=44.2; MRRO=47.5; LEAK RATE= 2.0
ACT= 128.3; REL= 95.8; DIF= 32.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 47; FIX 3; C= 0000000; BIN=8000; MRRL=44.2; MRRO=47.5; LEAK RATE= 2.0
ACT= 129.2; REL= 96.3; DIF= 32.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 48; FIX 4; C= 0000000; BIN=8000; MRRL=44.2; MRRO=47.5; LEAK RATE= 2.0
ACT= 134.0; REL= 100.1; DIF= 33.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:27:52.52 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:28:12.52 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 10:28:26.15 TUGL CYCLE TIMEOUT 1

SER 49; FIX 1; C= 0000000; BIN=8000; MRRL=44.3; MRRO=48.1; LEAK RATE= 1.9
ACT= 131.8; REL= 101.4; DIF= 30.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

P SER 50; FIX 2; C= 0000000; BIN=8000; MRRL=44.3; MRRO=48.1; LEAK RATE= 1.9
ACT= 133.2; REL= 98.8; DIF= 34.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 51; FIX 3; C= 0000000; BIN=8000; MRRL=44.3; MRRO=48.1; LEAK RATE= 1.9
ACT= 125.9; REL= 87.1; DIF= 38.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 52; FIX 4; C= 0000000; BIN=8000; MRRL=44.3; MRRO=48.1; LEAK RATE= 1.9
ACT= 127.2; REL= 95.2; DIF= 32.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:31:52.41 OPER DOOR DID NOT CLOSE 1

SER 53; FIX 1; C= 0000000; BIN=8000; MRRL=44.0; MRRO=47.7; LEAK RATE= 1.9
ACT= 123.3; REL= 92.4; DIF= 30.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 54; FIX 2; C= 0000000; BIN=8000; MRRL=44.0; MRRO=47.7; LEAK RATE= 1.9
ACT= 131.2; REL= 93.5; DIF= 27.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 55; FIX 3; C= 0000000; BIN=8000; MRRL=44.0; MRRO=47.7; LEAK RATE= 1.9
ACT= 122.5; REL= 85.4; DIF= 36.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 56; FIX 4; C= 0000000; BIN=8000; MRRL=44.0; MRRO=47.7; LEAK RATE= 1.9
ACT= 133.5; REL= 98.4; DIF= 35.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

NO: 138.7; REL= 107.4; DIF= 30.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 58; FIX 2; C= 000000; BIN=GOOD; MRRU=44.2; MRRD=47.5; LEAK RATE= 1.9
ACT= 138.0; REL= 107.4; DIF= 30.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 59; FIX 3; C= 000000; BIN=GOOD; MRRU=44.2; MRRD=47.5; LEAK RATE= 1.9
ACT= 120.8; REL= 87.1; DIF= 32.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

60 SER 60; FIX 4; C= 000000; BIN=GOOD; MRRU=44.2; MRRD=47.5; LEAK RATE= 1.9
ACT= 122.5; REL= 88.1; DIF= 34.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:32:33.71 OPER DOOR DID NOT CLOSE 1

SER 61; FIX 1; C= 000000; BIN=GOOD; MRRU=44.3; MRRD=48.0; LEAK RATE= 2.1
ACT= 128.1; REL= 94.5; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 62; FIX 2; C= 000000; BIN=GOOD; MRRU=44.3; MRRD=48.0; LEAK RATE= 2.1
ACT= 135.3; REL= 101.8; DIF= 33.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 63; FIX 3; C= 000000; BIN=GOOD; MRRU=44.3; MRRD=48.0; LEAK RATE= 2.1
ACT= 137.1; REL= 104.8; DIF= 32.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 64; FIX 4; C= 000000; BIN=GOOD; MRRU=44.3; MRRD=48.0; LEAK RATE= 2.1
ACT= 135.8; REL= 103.3; DIF= 32.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:33:00.40 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:33:20.40 OPER DOOR STILL DID NOT CLOSE 1

SER 65; FIX 1; C= 000000; BIN=GOOD; MRRU=43.7; MRRD=47.2; LEAK RATE= 1.7
ACT= 136.9; REL= 104.6; DIF= 32.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 66; FIX 2; C= 000000; BIN=GOOD; MRRU=43.7; MRRD=47.2; LEAK RATE= 1.7
ACT= 129.3; REL= 90.9; DIF= 38.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 67; FIX 3; C= 000000; BIN=GOOD; MRRU=43.7; MRRD=47.2; LEAK RATE= 1.7
ACT= 140.6; REL= 104.6; DIF= 36.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 68; FIX 4; C= 000000; BIN=GOOD; MRRU=43.7; MRRD=47.2; LEAK RATE= 1.7
ACT= 135.5; REL= 104.6; DIF= 30.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

TI-NHTSA 000010

SER 69; FIX 1; C= 0000000; BIN=GOOD; NRRU=44.2; MRRD=47.8; LEAK RATE= 1.9
ACT= 131.9; REL= 93.4; DIF= 37.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

70

SER 70; FIX 2; C= 0000000; BIN=GOOD; NRRU=44.2; MRRD=47.8; LEAK RATE= 1.9
ACT= 132.8; REL= 94.5; DIF= 38.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 71; FIX 3; C= 0000000; BIN=GOOD; NRRU=44.2; MRRD=47.8; LEAK RATE= 1.9
ACT= 134.0; REL= 102.1; DIF= 32.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 72; FIX 4; C= 0000000; BIN=GOOD; NRRU=44.2; MRRD=47.8; LEAK RATE= 1.9
ACT= 127.4; REL= 92.4; DIF= 35.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:34:29.53 OPER DOOR DID NOT CLOSE 1

SER 73; FIX 1; C= 0000000; BIN=GOOD; NRRU=44.1; MRRD=47.5; LEAK RATE= 2.0
ACT= 130.4; REL= 100.1; DIF= 30.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 74; FIX 2; C= 0000000; BIN=GOOD; NRRU=44.1; MRRD=47.5; LEAK RATE= 2.0
ACT= 122.0; REL= 94.1; DIF= 27.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 75; FIX 3; C= 0000000; BIN=GOOD; NRRU=44.1; MRRD=47.5; LEAK RATE= 2.0
ACT= 122.7; REL= 89.4; DIF= 33.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 76; FIX 4; C= 0000000; BIN=GOOD; NRRU=44.1; MRRD=47.5; LEAK RATE= 2.0
ACT= 125.9; REL= 89.4; DIF= 36.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 77; FIX 1; C= 0000000; BIN=GOOD; NRRU=44.8; MRRD=47.3; LEAK RATE= 2.0
ACT= 127.0; REL= 91.8; DIF= 35.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 78; FIX 2; C= 0000000; BIN=GOOD; NRRU=44.8; MRRD=47.3; LEAK RATE= 2.0
ACT= 126.0; REL= 91.8; DIF= 34.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 79; FIX 3; C= 0000000; BIN=GOOD; NRRU=44.8; MRRD=47.3; LEAK RATE= 2.0
ACT= 129.3; REL= 100.7; DIF= 28.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

80

SER 80; FIX 4; C= 0000000; BIN=GOOD; NRRU=44.8; MRRD=47.3; LEAK RATE= 2.0
ACT= 138.6; REL= 107.5; DIF= 31.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 81; FIX 1; C= 0000000; BIN=GOOD ; NFRU=44.3; NFRD=46.8; LEAK RATE= 2.0
ACT= 127.3; REL= 93.3; DIF= 34.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 82; FIX 2; C= 0000000; BIN=GOOD ; NFRU=44.3; NFRD=46.8; LEAK RATE= 2.0
ACT= 121.7; REL= 89.8; DIF= 31.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 83; FIX 3; C= 0000000; BIN=GOOD ; NFRU=44.3; NFRD=46.8; LEAK RATE= 2.0
ACT= 129.2; REL= 94.5; DIF= 34.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 84; FIX 4; C= 0000000; BIN=GOOD ; NFRU=44.3; NFRD=46.8; LEAK RATE= 2.0
ACT= 131.8; REL= 97.8; DIF= 32.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:23:46.00 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:36:06.00 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 10:36:22.20 TOOL CYCLE TIMEOUT 1

SER 85; FIX 1; C= 0000000; BIN=GOOD ; NFRU=43.9; NFRD=47.8; LEAK RATE= 2.1
ACT= 131.6; REL= 96.7; DIF= 34.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 86; FIX 2; C= 0000000; BIN=GOOD ; NFRU=43.9; NFRD=47.8; LEAK RATE= 2.1
ACT= 117.2; REL= 83.0; DIF= 34.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 87; FIX 3; C= 0000000; BIN=GOOD ; NFRU=43.9; NFRD=47.8; LEAK RATE= 2.1
ACT= 130.4; REL= 99.4; DIF= 31.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 88; FIX 4; C= 0000000; BIN=GOOD ; NFRU=43.9; NFRD=47.8; LEAK RATE= 2.1
ACT= 119.8; REL= 70.8; DIF= 28.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:39:56.83 OPER DOOR DID NOT CLOSE 1

SER 89; FIX 1; C= 0000000; BIN=GOOD ; NFRU=44.2; NFRD=47.8; LEAK RATE= 1.9
ACT= 128.0; REL= 96.4; DIF= 31.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

90 SER 90; FIX 2; C= 0000000; BIN=GOOD ; NFRU=44.2; NFRD=47.8; LEAK RATE= 1.9
ACT= 133.9; REL= 99.9; DIF= 34.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 91; FIX 3; C= 0000000; BIN=GOOD ; NFRU=44.2; NFRD=47.8; LEAK RATE= 1.9
ACT= 126.1; REL= 97.8; DIF= 32.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

ACT= 126.1; REL= 72.0; DIF= 33.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:40:40.32 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:41:00.32 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 10:41:17.81 TOOL CYCLE TIMEOUT 1

SER 93; FIX 1; C= 0000000; BIN=GOOD ; MRRU=44.4; MRRD=47.8; LEAK RATE= 2.0
ACT= 132.5; REL= 97.4; DIF= 35.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 94; FIX 2; C= 0000000; BIN=GOOD ; MRRU=44.4; MRRD=47.8; LEAK RATE= 2.0
ACT= 129.3; REL= 94.9; DIF= 34.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 95; FIX 3; C= 0000000; BIN=GOOD ; MRRU=44.4; MRRD=47.8; LEAK RATE= 2.0
ACT= 138.2; REL= 103.8; DIF= 34.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 96; FIX 4; C= 0000000; BIN=GOOD ; MRRU=44.4; MRRD=47.8; LEAK RATE= 2.0
ACT= 125.6; REL= 90.2; DIF= 35.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:44:39.52 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:44:59.52 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 10:45:17.91 TOOL CYCLE TIMEOUT 1

SER 97; FIX 1; C= 0000000; BIN=GOOD ; MRRU=43.8; MRRD=47.4; LEAK RATE= 1.9
ACT= 132.4; REL= 96.9; DIF= 35.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 98; FIX 2; C= 0000000; BIN=GOOD ; MRRU=43.8; MRRD=47.4; LEAK RATE= 1.9
ACT= 132.9; REL= 102.2; DIF= 30.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 99; FIX 3; C= 0000000; BIN=GOOD ; MRRU=43.8; MRRD=47.4; LEAK RATE= 1.9
ACT= 123.6; REL= 87.2; DIF= 36.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

100 SER 100; FIX 4; C= 0000000; BIN=GOOD ; MRRU=43.8; MRRD=47.4; LEAK RATE= 1.9
ACT= 124.6; REL= 89.7; DIF= 35.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

ACT= 130.4; REL= 95.9; DIF= 34.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 102; FIX 2; C= 0000000; BIN=8000; MRRU=44.1; MRRD=47.8; LEAK RATE= 1.9
ACT= 132.6; REL= 90.2; DIF= 42.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 103; FIX 3; C= 0000000; BIN=8000; MRRU=44.1; MRRD=47.8; LEAK RATE= 1.9
ACT= 138.2; REL= 103.8; DIF= 34.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 104; FIX 4; C= 0000000; BIN=8000; MRRU=44.1; MRRD=47.4; LEAK RATE= 1.9
ACT= 125.9; REL= 91.4; DIF= 34.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 105; FIX 1; C= 0000000; BIN=8000; MRRU=44.1; MRRD=47.2; LEAK RATE= 1.8
ACT= 140.4; REL= 113.1; DIF= 27.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 106; FIX 2; C= 0000000; BIN=8000; MRRU=44.1; MRRD=47.2; LEAK RATE= 1.8
ACT= 133.8; REL= 100.6; DIF= 33.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 107; FIX 3; C= 0000000; BIN=8000; MRRU=44.1; MRRD=47.2; LEAK RATE= 1.8
ACT= 132.4; REL= 94.4; DIF= 38.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 108; FIX 4; C= 0000000; BIN=8000; MRRU=44.1; MRRD=47.2; LEAK RATE= 1.8
ACT= 139.1; REL= 105.9; DIF= 33.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:49:40.16 OPER DOOR DID NOT CLOSE 1

SER 109; FIX 1; C= 0000000; BIN=8000; MRRU=44.4; MRRD=47.9; LEAK RATE= 2.0
ACT= 127.6; REL= 100.8; DIF= 26.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

110 SER 110; FIX 2; C= 0000000; BIN=8000; MRRU=44.4; MRRD=47.9; LEAK RATE= 2.0
ACT= 137.5; REL= 104.9; DIF= 32.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 111; FIX 3; C= 0000000; BIN=8000; MRRU=44.4; MRRD=47.9; LEAK RATE= 2.0
ACT= 131.3; REL= 100.8; DIF= 30.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 112; FIX 4; C= 0000000; BIN=8000; MRRU=44.4; MRRD=47.9; LEAK RATE= 2.0
ACT= 129.0; REL= 97.0; DIF= 32.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 113; FIX 1; C= 0000000; BIN=8000; MRRU=44.2; MRRD=47.2; LEAK RATE= 2.0
ACT= 125.3; REL= 92.2; DIF= 33.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 114; FIX 2; C= 0000000; BIN=8000; MRRU=44.2; MRRD=47.2; LEAK RATE= 2.0
ACT= 133.2; REL= 102.1; DIF= 31.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

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ACT= 130.4; REL= 96.2; DIF= 22.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 116; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.2; LEAK RATE= 2.0
ACT= 124.3; REL= 93.6; DIF= 30.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 117; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.9; LEAK RATE= 2.1
ACT= 132.4; REL= 104.7; DIF= 27.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 118; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.9; LEAK RATE= 2.1
ACT= 123.1; REL= 89.9; DIF= 33.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 119; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.9; LEAK RATE= 2.1
ACT= 119.8; REL= 88.7; DIF= 31.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

120 SER 120; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.9; LEAK RATE= 2.1
ACT= 132.4; REL= 98.2; DIF= 34.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 121; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.8; LEAK RATE= 2.0
ACT= 135.2; REL= 107.8; DIF= 27.4 PSI; ACTCR= 200.0ms; RELCR= 122.3

SER 122; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.8; LEAK RATE= 2.0
ACT= 130.6; REL= 93.8; DIF= 36.7 PSI; ACTCR= 200.0ms; RELCR= 15.0

SER 123; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.8; LEAK RATE= 2.0
ACT= 128.2; REL= 96.0; DIF= 32.2 PSI; ACTCR= 200.0ms; RELCR= 38.4

24 SER 124; FIX 4; C= 0020000; BIN=CONT; MRRU=44.1; MRRD=47.8; LEAK RATE= 2.0
ACT= 177.8; REL= 92.5; DIF= 85.2 PSI; ACTCR= 200.0ms; RELCR= 0.6

17-APR-1992 10:51:29.38 OPER DOOR DID NOT CLOSE 1

SER 125; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.3; LEAK RATE= 2.4
ACT= 128.5; REL= 96.1; DIF= 32.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 126; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.3; LEAK RATE= 2.4
ACT= 123.4; REL= 39.6; DIF= 33.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 127; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.3; LEAK RATE= 2.4
ACT= 125.4; REL= 34.1; DIF= 31.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 128; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.3; LEAK RATE= 2.4
ACT= 131.2; REL= 71.1; DIF= 37.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

TI-NHTSA 006015

17-APR-1992 10:52:25.66 OPER DOOR STILL DID NOT CLOSE 1

SER 129; FIX 1; C= 0000000; BIN=GOOD; MFRU=44.1; MFRD=47.6; LEAK RATE= 2.2
ACT= 134.9; REL= 107.6; DIF= 26.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

130

SER 130; FIX 2; C= 0000000; BIN=GOOD; MFRU=44.1; MFRD=47.6; LEAK RATE= 2.2
ACT= 151.3; REL= 100.8; DIF= 30.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 131; FIX 3; C= 0000000; BIN=GOOD; MFRU=44.1; MFRD=47.6; LEAK RATE= 2.2
ACT= 129.5; REL= 97.1; DIF= 32.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 132; FIX 4; C= 0000000; BIN=GOOD; MFRU=44.1; MFRD=47.6; LEAK RATE= 2.2
ACT= 126.2; REL= 94.6; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

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17-APR-1992 10:53:00.20 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:53:20.20 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 10:53:37.62 TOOL CYCLE TIMEOUT 1

SER 133; FIX 1; C= 0000000; BIN=GOOD; MFRU=44.5; MFRD=47.1; LEAK RATE= 1.8
ACT= 137.2; REL= 106.1; DIF= 31.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 134; FIX 2; C= 0000000; BIN=GOOD; MFRU=44.5; MFRD=47.1; LEAK RATE= 1.8
ACT= 128.7; REL= 96.9; DIF= 31.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 135; FIX 3; C= 0000000; BIN=GOOD; MFRU=44.5; MFRD=47.1; LEAK RATE= 1.8
ACT= 129.1; REL= 99.5; DIF= 29.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 136; FIX 4; C= 0000000; BIN=GOOD; MFRU=44.5; MFRD=47.1; LEAK RATE= 1.8
ACT= 127.3; REL= 91.8; DIF= 35.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:54:52.26 OPER DOOR DID NOT CLOSE 1

REL= 120.1; REL= 103.5; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 138; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.2; LEAK RATE= 2.0
ACT= 130.7; REL= 97.1; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 139; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.2; LEAK RATE= 2.0
ACT= 132.8; REL= 103.5; DIF= 29.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

140 SER 140; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.2; LEAK RATE= 2.0
ACT= 129.9; REL= 93.5; DIF= 36.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 141; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.5; LEAK RATE= 2.0
ACT= 127.7; REL= 96.6; DIF= 31.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 142; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.5; LEAK RATE= 2.0
ACT= 118.7; REL= 87.2; DIF= 31.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 143; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.5; LEAK RATE= 2.0
ACT= 124.4; REL= 88.5; DIF= 35.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 144; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.5; LEAK RATE= 2.0
ACT= 131.7; REL= 104.6; DIF= 27.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 145; FIX 1; C= 0000000; BIN=GOOD; MRRU=43.6; MRRD=47.1; LEAK RATE= 2.2
ACT= 138.3; REL= 108.9; DIF= 29.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 146; FIX 2; C= 0000000; BIN=GOOD; MRRU=43.8; MRRD=47.1; LEAK RATE= 2.2
ACT= 126.6; REL= 95.8; DIF= 30.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 147; FIX 3; C= 0000000; BIN=GOOD; MRRU=43.2; MRRD=47.1; LEAK RATE= 2.2
ACT= 131.5; REL= 97.3; DIF= 34.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 148; FIX 4; C= 0000000; BIN=GOOD; MRRU=43.8; MRRD=47.1; LEAK RATE= 2.2
ACT= 128.0; REL= 92.4; DIF= 35.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 149; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.1; LEAK RATE= 2.2
ACT= 132.2; REL= 102.1; DIF= 30.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

150 SER 150; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.1; LEAK RATE= 2.2
ACT= 131.0; REL= 98.3; DIF= 32.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 151; FIX 3; C= 0020012; BIN=GOOD; MRRU=44.2; MRRD=47.1; LEAK RATE= 2.2
ACT= 176.0; REL= 140.7; DIF= 37.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 152; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.1; LEAK RATE= 2.2
ACT= 139.2; REL= 97.1; DIF= 42.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 153; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.5; LEAK RATE= 1.9
ACT= 129.4; REL= 95.8; DIF= 33.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 154; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.5; LEAK RATE= 1.9
ACT= 131.4; REL= 97.9; DIF= 31.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 155; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.5; LEAK RATE= 1.9
ACT= 132.5; REL= 99.9; DIF= 32.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 156; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.5; LEAK RATE= 1.9
ACT= 136.1; REL= 102.9; DIF= 33.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 157; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.5; MRRD=47.6; LEAK RATE= 1.9
ACT= 130.4; REL= 96.4; DIF= 33.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 158; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.5; MRRD=47.6; LEAK RATE= 1.9
ACT= 134.1; REL= 97.8; DIF= 36.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 159; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.5; MRRD=47.6; LEAK RATE= 1.9
ACT= 125.0; REL= 91.8; DIF= 33.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

160 SER 160; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.5; MRRD=47.6; LEAK RATE= 1.9
ACT= 130.4; REL= 96.6; DIF= 33.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:57:25.89 OPER GOOD DID NOT CLOSE 1

SER 161; FIX 1; C= 0000000; BIN=GOOD; MRRU=43.9; MRRD=47.8; LEAK RATE= 1.9
ACT= 133.2; REL= 99.4; DIF= 35.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 162; FIX 2; C= 0000000; BIN=GOOD; MRRU=43.9; MRRD=47.8; LEAK RATE= 1.9
ACT= 131.0; REL= 97.0; DIF= 34.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 163; FIX 3; C= 0000000; BIN=GOOD; MRRU=43.9; MRRD=47.8; LEAK RATE= 1.9

TI-NHTSA 006018

ACT= 133.2; REL= 95.7; DIF= 37.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 165; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.7; LEAK RATE= 2.0
ACT= 137.2; REL= 102.3; DIF= 34.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 166; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.7; LEAK RATE= 2.0
ACT= 129.3; REL= 98.3; DIF= 31.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 167; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.7; LEAK RATE= 2.0
ACT= 126.7; REL= 93.2; DIF= 33.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 168; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.7; LEAK RATE= 2.0
ACT= 125.3; REL= 86.7; DIF= 38.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 10:58:22.59 OPER DOOR DID NOT CLOSE 1

17-APR-1992 10:58:42.59 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 10:59:00.61 TOOL CYCLE TIMEOUT 1

SER 169; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.7; LEAK RATE= 2.1
ACT= 128.3; REL= 96.1; DIF= 30.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

170

SER 170; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.7; LEAK RATE= 2.1
ACT= 126.5; REL= 90.3; DIF= 35.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 171; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.7; LEAK RATE= 2.1
ACT= 127.1; REL= 94.4; DIF= 32.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 172; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.7; LEAK RATE= 2.1
ACT= 123.0; REL= 96.7; DIF= 26.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:00:53.08 OPER DOOR DID NOT CLOSE 1

17-APR-1992 11:01:13.08 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 11:01:29.18 TOOL CYCLE TIMEOUT 1

SER 173; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.0; MRRD=47.0; LEAK RATE= 2.2
ACT= 134.0; REL= 100.3; DIF= 33.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 174; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.0; MRRD=47.0; LEAK RATE= 2.2
ACT= 142.9; REL= 112.3; DIF= 30.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 175; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.0; MRRD=47.0; LEAK RATE= 2.2

TI-NHTSA 006019

ACT= 134.5; REL= 100.3; DIF= 34.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:03:27.56 OPER DOOR DID NOT CLOSE 1

SER 177; FIX 1; C= 0000000; BIN=GOOD; MRSL=43.7; MRSD=47.4; LEAK RATE= 1.9
ACT= 132.2; REL= 101.0; DIF= 31.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 178; FIX 2; C= 0000000; BIN=GOOD; MRSL=43.7; MRSD=47.4; LEAK RATE= 1.9
ACT= 128.0; REL= 98.4; DIF= 29.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 179; FIX 3; C= 0000000; BIN=GOOD; MRSL=43.7; MRSD=47.4; LEAK RATE= 1.9
ACT= 131.7; REL= 97.2; DIF= 34.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

180 SER 180; FIX 4; C= 0000000; BIN=GOOD; MRSL=43.7; MRSD=47.4; LEAK RATE= 1.9
ACT= 126.3; REL= 92.3; DIF= 33.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:03:52.53 OPER DOOR DID NOT CLOSE 1

SER 181; FIX 1; C= 0000000; BIN=GOOD; MRSL=44.3; MRSD=47.5; LEAK RATE= 2.0
ACT= 131.7; REL= 97.7; DIF= 34.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 182; FIX 2; C= 0000000; BIN=GOOD; MRSL=44.3; MRSD=47.5; LEAK RATE= 2.0
ACT= 128.5; REL= 96.4; DIF= 32.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 183; FIX 3; C= 0000000; BIN=GOOD; MRSL=44.3; MRSD=47.5; LEAK RATE= 2.0
ACT= 133.1; REL= 101.5; DIF= 31.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 184; FIX 4; C= 0000000; BIN=GOOD; MRSL=44.3; MRSD=47.5; LEAK RATE= 2.0
ACT= 131.7; REL= 101.1; DIF= 30.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:04:18.31 OPER DOOR DID NOT CLOSE 1

TI-NHTSA 006020

MRU= 122.3; REL= 70.9; DIF= 32.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 186; FIX 2; C= 000000; BIN=GOOD; MRU=44.2; MRD=47.6; LEAK RATE= 2.0
ACT= 135.3; REL= 104.0; DIF= 31.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 187; FIX 3; C= 000000; BIN=GOOD; MRU=44.2; MRD=47.6; LEAK RATE= 2.0
ACT= 129.9; REL= 97.6; DIF= 32.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 188; FIX 4; C= 000000; BIN=GOOD; MRU=44.2; MRD=47.6; LEAK RATE= 2.0
ACT= 132.6; REL= 102.6; DIF= 30.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:04:44.23 OPER DOOR DID NOT CLOSE 1

SER 189; FIX 1; C= 000000; BIN=GOOD; MRU=44.5; MRD=48.5; LEAK RATE= 1.6
ACT= 135.8; REL= 106.3; DIF= 29.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

190 SER 190; FIX 2; C= 000000; BIN=GOOD; MRU=44.5; MRD=48.5; LEAK RATE= 1.8
ACT= 125.0; REL= 90.4; DIF= 34.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 191; FIX 3; C= 000000; BIN=GOOD; MRU=44.5; MRD=48.5; LEAK RATE= 1.6
ACT= 128.7; REL= 95.2; DIF= 33.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 192; FIX 4; C= 000000; BIN=GOOD; MRU=44.5; MRD=48.5; LEAK RATE= 1.8
ACT= 132.4; REL= 100.0; DIF= 32.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 193; FIX 1; C= 000000; BIN=GOOD; MRU=44.3; MRD=47.7; LEAK RATE= 2.0
ACT= 132.0; REL= 102.5; DIF= 33.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 194; FIX 2; C= 000000; BIN=GOOD; MRU=44.3; MRD=47.7; LEAK RATE= 2.0
ACT= 133.3; REL= 96.0; DIF= 35.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 195; FIX 3; C= 000000; BIN=GOOD; MRU=44.3; MRD=47.7; LEAK RATE= 2.0
ACT= 130.6; REL= 100.4; DIF= 30.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 196; FIX 4; C= 000000; BIN=GOOD; MRU=44.3; MRD=47.7; LEAK RATE= 2.0
ACT= 122.1; REL= 90.6; DIF= 31.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

TI-NHTSA 006021

ACT= 128.4; REL= 101.9; DIF= 30.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 198; FIX 2; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=47.5; LEAK RATE= 2.2
ACT= 129.8; REL= 95.5; DIF= 34.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 199; FIX 3; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=47.5; LEAK RATE= 2.2
ACT= 133.1; REL= 104.1; DIF= 29.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

200 SER 200; FIX 4; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=47.5; LEAK RATE= 2.2
ACT= 132.7; REL= 101.6; DIF= 31.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 201; FIX 1; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=46.2; LEAK RATE= 2.3
ACT= 141.4; REL= 111.0; DIF= 30.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 202; FIX 2; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=46.2; LEAK RATE= 2.3
ACT= 140.5; REL= 111.0; DIF= 29.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 203; FIX 3; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=46.2; LEAK RATE= 2.3
ACT= 130.8; REL= 100.3; DIF= 30.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 204; FIX 4; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=46.2; LEAK RATE= 2.3
ACT= 138.7; REL= 104.0; DIF= 34.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:06:27.81 OPER DOOR DID NOT CLOSE 1

SER 205; FIX 1; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=48.0; LEAK RATE= 2.1
ACT= 123.4; REL= 98.3; DIF= 35.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 206; FIX 2; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=48.0; LEAK RATE= 2.1
ACT= 131.7; REL= 102.2; DIF= 29.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 207; FIX 3; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=48.0; LEAK RATE= 2.1
ACT= 134.6; REL= 102.2; DIF= 32.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 208; FIX 4; C= 000000; BIN=GOOD; NFRU=44.2; NFRD=48.0; LEAK RATE= 2.1
ACT= 129.9; REL= 100.9; DIF= 29.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:07:09.67 OPER DOOR DID NOT CLOSE 1

17-APR-1992 11:07:29.87 OPER DOOR STILL DID NOT CLOSE 1

SER 209; FIX 1; C= 000000; BIN=8000; MRU=44.2; MRD=47.4; LEAK RATE= 1.9
ACT= 128.4; REL= 97.6; DIF= 30.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

210 SER 210; FIX 2; C= 000000; BIN=8000; MRU=44.2; MRD=47.4; LEAK RATE= 1.9
ACT= 126.5; REL= 95.1; DIF= 31.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 211; FIX 3; C= 000000; BIN=8000; MRU=44.2; MRD=47.4; LEAK RATE= 1.9
ACT= 132.9; REL= 96.3; DIF= 36.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 212; FIX 4; C= 000000; BIN=8000; MRU=44.2; MRD=47.4; LEAK RATE= 1.9
ACT= 126.0; REL= 94.2; DIF= 31.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 213; FIX 1; C= 000000; BIN=8000; MRU=44.5; MRD=47.5; LEAK RATE= 2.1
ACT= 129.8; REL= 97.4; DIF= 32.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 214; FIX 2; C= 000000; BIN=8000; MRU=44.5; MRD=47.5; LEAK RATE= 2.1
ACT= 133.3; REL= 97.4; DIF= 35.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 215; FIX 3; C= 000000; BIN=8000; MRU=44.5; MRD=47.5; LEAK RATE= 2.1
ACT= 136.9; REL= 104.0; DIF= 32.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 216; FIX 4; C= 000000; BIN=8000; MRU=44.5; MRD=47.5; LEAK RATE= 2.1
ACT= 127.2; REL= 93.7; DIF= 33.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:15:06.63 SUPER DOOR DID NOT CLOSE 1

SER 217; FIX 1; C= 000000; BIN=8000; MRU=44.3; MRD=47.6; LEAK RATE= 2.0
ACT= 133.4; REL= 102.5; DIF= 30.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 218; FIX 2; C= 000000; BIN=8000; MRU=44.3; MRD=47.6; LEAK RATE= 2.0
ACT= 125.0; REL= 92.7; DIF= 32.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 219; FIX 3; C= 000000; BIN=8000; MRU=44.3; MRD=47.6; LEAK RATE= 2.0
ACT= 139.7; REL= 108.2; DIF= 31.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

220 SER 220; FIX 4; C= 000000; BIN=8000; MRU=44.3; MRD=47.6; LEAK RATE= 2.0
ACT= 125.3; REL= 90.3; DIF= 35.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:16:31.42 OPER DOOR DID NOT CLOSE 1

SER 221; FIX 1; C= 0000000; BIN=GOOD ; MRRU=44.1; MRRD=47.7; LEAK RATE= 1.9
ACT= 134.1; REL= 133.5; DIF= 31.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 222; FIX 2; C= 0000000; BIN=GOOD ; MRRU=44.1; MRRD=47.7; LEAK RATE= 1.9
ACT= 127.5; REL= 94.6; DIF= 32.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 223; FIX 3; C= 0000000; BIN=GOOD ; MRRU=44.1; MRRD=47.7; LEAK RATE= 1.9
ACT= 126.6; REL= 94.6; DIF= 32.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 224; FIX 4; C= 0000000; BIN=GOOD ; MRRU=44.1; MRRD=47.7; LEAK RATE= 1.9
ACT= 133.8; REL= 101.1; DIF= 32.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:16:56.88 OPER DOOR DID NOT CLOSE 1

SER 225; FIX 1; C= 0000000; BIN=GOOD ; MRRU=44.3; MRRD=46.7; LEAK RATE= 1.9
ACT= 132.5; REL= 98.0; DIF= 34.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 226; FIX 2; C= 0000000; BIN=GOOD ; MRRU=44.3; MRRD=46.7; LEAK RATE= 1.9
ACT= 129.9; REL= 90.3; DIF= 39.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 227; FIX 3; C= 0000000; BIN=GOOD ; MRRU=44.3; MRRD=46.7; LEAK RATE= 1.9
ACT= 133.5; REL= 105.4; DIF= 28.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 228; FIX 4; C= 0000000; BIN=GOOD ; MRRU=44.3; MRRD=46.7; LEAK RATE= 1.9
ACT= 126.6; REL= 89.3; DIF= 37.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:17:28.27 OPER DOOR DID NOT CLOSE 1

SER 229; FIX 1; C= 0000000; BIN=GOOD ; MRRU=44.2; MRRD=47.5; LEAK RATE= 1.6
ACT= 124.9; REL= 92.3; DIF= 32.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

230 SER 230; FIX 2; C= 0000000; BIN=GOOD ; MRRU=44.2; MRRD=47.5; LEAK RATE= 1.6
ACT= 127.2; REL= 73.5; DIF= 33.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

TI-NHTSA 006024

ACT= 126.3; REL= 90.0; DIF= 36.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 232; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.5; LEAK RATE= 1.6
ACT= 130.8; REL= 97.1; DIF= 33.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:17:52.80 OPER DOOR DID NOT CLOSE 1

SER 233; FIX 1; C= 0000000; BIN=GOOD; MRRU=45.8; MRRD=47.4; LEAK RATE= 1.9
ACT= 117.2; REL= 82.4; DIF= 34.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 234; FIX 2; C= 0000000; BIN=GOOD; MRRU=43.8; MRRD=47.6; LEAK RATE= 1.9
ACT= 128.9; REL= 95.0; DIF= 33.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 235; FIX 3; C= 0000000; BIN=GOOD; MRRU=43.8; MRRD=47.6; LEAK RATE= 1.9
ACT= 129.3; REL= 95.0; DIF= 34.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 236; FIX 4; C= 0000000; BIN=GOOD; MRRU=43.8; MRRD=47.6; LEAK RATE= 1.9
ACT= 128.7; REL= 96.3; DIF= 32.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 237; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.9; LEAK RATE= 1.7
ACT= 126.6; REL= 93.8; DIF= 32.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 238; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.9; LEAK RATE= 1.7
ACT= 132.4; REL= 96.7; DIF= 33.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 239; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.9; LEAK RATE= 1.7
ACT= 132.4; REL= 99.9; DIF= 32.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

240 SER 240; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=47.9; LEAK RATE= 1.7
ACT= 126.9; REL= 92.6; DIF= 34.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 241; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.5; MRRD=47.5; LEAK RATE= 1.8
ACT= 135.2; REL= 102.3; DIF= 26.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

TI-NHTSA 006026

17-APR-1992 11:19:07.88 OPER DOOR DID NOT CLOSE 1

SER 243; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.5; MRRD=47.5; LEAK RATE= 1.8
ACT= 126.5; REL= 93.9; DIF= 32.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 244; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.5; MRRD=47.5; LEAK RATE= 1.8
ACT= 136.0; REL= 103.0; DIF= 33.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:19:07.88 OPER DOOR DID NOT CLOSE 1

17-APR-1992 11:19:27.88 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 11:19:46.19 TOOL CYCLE TIMEOUT 1

SER 245; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.4; LEAK RATE= 1.8
ACT= 138.9; REL= 104.2; DIF= 34.7 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 246; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.4; LEAK RATE= 1.8
ACT= 130.4; REL= 100.2; DIF= 30.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 247; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.4; LEAK RATE= 1.8
ACT= 124.4; REL= 96.4; DIF= 30.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 248; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.4; LEAK RATE= 1.8
ACT= 139.3; REL= 108.1; DIF= 31.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 249; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.6; LEAK RATE= 2.1
ACT= 126.4; REL= 92.3; DIF= 34.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

250 SER 250; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.6; LEAK RATE= 2.1
ACT= 137.5; REL= 109.2; DIF= 28.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 251; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.6; LEAK RATE= 2.1
ACT= 131.7; REL= 102.4; DIF= 29.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 252; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.6; LEAK RATE= 2.1
ACT= 128.2; REL= 92.3; DIF= 35.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:22:27.92 OPER DOOR DID NOT CLOSE 1

17-APR-1992 11:22:47.92 OPER DOOR STILL DID NOT CLOSE 1

SER 253; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.0; LEAK RATE= 2.0
ACT= 131.7; REL= 100.8; DIF= 30.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 254; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.0; LEAK RATE= 2.0
ACT= 134.4; REL= 99.5; DIF= 34.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

REL= 120.5; REL= 87.5; DIF= 30.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 256; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.0; LEAK RATE= 2.0
ACT= 120.5; REL= 87.5; DIF= 30.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:23:22.47 OPER DOOR DID NOT CLOSE 1

17-APR-1992 11:23:42.47 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 11:23:59.21 TQDL CYCLE TIMEOUT 1

SER 257; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.6; MRRD=47.8; LEAK RATE= 1.8
ACT= 130.3; REL= 95.2; DIF= 35.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 258; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.6; MRRD=47.8; LEAK RATE= 1.8
ACT= 133.4; REL= 100.1; DIF= 33.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 259; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.6; MRRD=47.8; LEAK RATE= 1.8
ACT= 124.2; REL= 98.8; DIF= 25.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

260 SER 260; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.6; MRRD=47.8; LEAK RATE= 1.8
ACT= 133.9; REL= 101.2; DIF= 32.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:30:18.24 OPER DOOR DID NOT CLOSE 1

SER 261; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=48.1; LEAK RATE= 2.1
ACT= 133.7; REL= 101.4; DIF= 32.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 262; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=48.1; LEAK RATE= 2.1
ACT= 130.6; REL= 102.8; DIF= 27.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 263; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=48.1; LEAK RATE= 2.1
ACT= 128.1; REL= 92.7; DIF= 35.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 264; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=48.1; LEAK RATE= 2.1
ACT= 128.9; REL= 101.4; DIF= 27.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 265; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.7; LEAK RATE= 2.3
ACT= 130.8; REL= 95.9; DIF= 35.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 266; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.7; LEAK RATE= 2.3
ACT= 133.3; REL= 101.0; DIF= 32.3 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 267; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.7; LEAK RATE= 2.3
ACT= 127.2; REL= 92.5; DIF= 34.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 268; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.4; MRRD=47.7; LEAK RATE= 2.3
ACT= 130.8; REL= 95.9; DIF= 35.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

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SER 269; FIX 1; C= 000000; BIN=GOOD; NRRU=44.0; MRRD=47.3; LEAK RATE= 2.0
ACT= 129.5; REL= 93.7; DIF= 35.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

270 SER 270; FIX 2; C= 000000; BIN=GOOD; NRRU=44.0; MRRD=47.3; LEAK RATE= 2.0
ACT= 130.3; REL= 95.5; DIF= 31.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 271; FIX 3; C= 000000; BIN=GOOD; NRRU=44.0; MRRD=47.3; LEAK RATE= 2.0
ACT= 142.8; REL= 107.8; DIF= 34.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 272; FIX 4; C= 000000; BIN=GOOD; NRRU=44.0; MRRD=47.3; LEAK RATE= 2.0
ACT= 126.1; REL= 94.9; DIF= 31.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 273; FIX 1; C= 000000; BIN=GOOD; NRRU=44.2; MRRD=47.7; LEAK RATE= 1.5
ACT= 127.1; REL= 91.1; DIF= 36.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 274; FIX 2; C= 000000; BIN=GOOD; NRRU=44.2; MRRD=47.7; LEAK RATE= 1.5
ACT= 139.7; REL= 97.2; DIF= 33.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 275; FIX 3; C= 000000; BIN=GOOD; NRRU=44.2; MRRD=47.7; LEAK RATE= 1.5
ACT= 134.7; REL= 104.8; DIF= 29.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 276; FIX 4; C= 000000; BIN=GOOD; NRRU=44.2; MRRD=47.7; LEAK RATE= 1.5
ACT= 127.6; REL= 97.2; DIF= 30.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:32:08.07 OPER DOOR DID NOT CLOSE 1

SER 277; FIX 1; C= 000000; BIN=GOOD; NRRU=44.4; MRRD=48.0; LEAK RATE= 1.8
ACT= 127.2; REL= 93.6; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 278; FIX 2; C= 000000; BIN=GOOD; NRRU=44.4; MRRD=48.0; LEAK RATE= 1.8
ACT= 123.1; REL= 89.0; DIF= 34.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 279; FIX 3; C= 000000; BIN=GOOD; NRRU=44.4; MRRD=48.0; LEAK RATE= 1.8
ACT= 129.9; REL= 96.1; DIF= 33.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

280 SER 280; FIX 4; C= 000000; BIN=GOOD; NRRU=44.4; MRRD=48.0; LEAK RATE= 1.8
ACT= 127.2; REL= 93.6; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:32:53.64 OPER DOOR DID NOT CLOSE 1

SER 281; FIX 1; C= 0000000; BIN=GOOD; MRU=44.1; MRD=47.7; LEAK RATE= 1.9
ACT= 130.5; REL= 100.6; DIF= 29.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 282; FIX 2; C= 0000000; BIN=GOOD; MRU=44.1; MRD=47.7; LEAK RATE= 1.9
ACT= 123.6; REL= 93.2; DIF= 30.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 283; FIX 3; C= 0000000; BIN=GOOD; MRU=44.1; MRD=47.7; LEAK RATE= 1.9
ACT= 131.3; REL= 96.8; DIF= 34.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 284; FIX 4; C= 0000000; BIN=GOOD; MRU=44.1; MRD=47.7; LEAK RATE= 1.9
ACT= 134.2; REL= 100.6; DIF= 33.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:33:01.25 OPER DOOR DID NOT CLOSE 1

17-APR-1992 11:33:21.28 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 11:33:57.15 TOOL CYCLE TIMEOUT 1

SER 285; FIX 1; C= 0000000; BIN=GOOD; MRU=44.3; MRD=48.7; LEAK RATE= 2.1
ACT= 131.5; REL= 99.6; DIF= 32.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 286; FIX 2; C= 0000000; BIN=GOOD; MRU=44.3; MRD=48.7; LEAK RATE= 2.1
ACT= 137.6; REL= 103.6; DIF= 34.0 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 287; FIX 3; C= 0000000; BIN=GOOD; MRU=44.3; MRD=48.7; LEAK RATE= 2.1
ACT= 125.6; REL= 89.8; DIF= 35.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 288; FIX 4; C= 0000000; BIN=GOOD; MRU=44.3; MRD=48.7; LEAK RATE= 2.1
ACT= 129.1; REL= 99.6; DIF= 29.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:42:46.51 OPER DOOR DID NOT CLOSE 1

17-APR-1992 11:43:06.51 OPER DOOR STILL DID NOT CLOSE 1

SER 289; FIX 1; C= 0000000; BIN=GOOD; MRU=44.1; MRD=48.0; LEAK RATE= 2.0
ACT= 133.1; REL= 98.5; DIF= 34.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

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SER 291; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=48.0; LEAK RATE= 2.0
ACT= 129.4; REL= 99.6; DIF= 29.8 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 292; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.1; MRRD=48.0; LEAK RATE= 2.0
ACT= 137.5; REL= 103.6; DIF= 33.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:43:52.41 OPER DOOR DID NOT CLOSE 1

SER 293; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.6; LEAK RATE= 2.0
ACT= 129.9; REL= 95.5; DIF= 34.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 294; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.6; LEAK RATE= 2.0
ACT= 125.2; REL= 93.0; DIF= 32.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 295; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.6; LEAK RATE= 2.0
ACT= 134.0; REL= 104.4; DIF= 29.5 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 296; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.6; LEAK RATE= 2.0
ACT= 122.9; REL= 87.3; DIF= 35.6 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:44:31.03 OPER DOOR DID NOT CLOSE 1

SER 297; FIX 1; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.2; LEAK RATE= 1.9
ACT= 131.0; REL= 99.1; DIF= 31.9 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 298; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.2; LEAK RATE= 1.9
ACT= 123.8; REL= 90.6; DIF= 33.2 PSI; ACTCR= 200.0ms; RELCR= 200.0

SER 299; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.2; LEAK RATE= 1.9
ACT= 123.8; REL= 97.5; DIF= 28.4 PSI; ACTCR= 200.0ms; RELCR= 200.0

300
*** SER 300; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.2; MRRD=47.2; LEAK RATE= 1.9
ACT= 126.9; REL= 91.6; DIF= 35.1 PSI; ACTCR= 200.0ms; RELCR= 200.0

17-APR-1992 11:45:11.54 OPER DOOR DID NOT CLOSE 1

17-APR-1992 11:45:31.54 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 11:45:46.25 TOOL CYCLE TIMEOUT 1

124 ACT= 143.6; REL= 112.8; DIF= 30.8 PSI; ACTCR= 200.0mm; RELCR= 200.0

51 SER 302; FIX 2; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.7; LEAK RATE= 1.9
ACT= 127.6; REL= 89.5; DIF= 38.1 PSI; ACTCR= 200.0mm; RELCR= 200.0

SER 303; FIX 3; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.7; LEAK RATE= 1.9
ACT= 129.8; REL= 103.2; DIF= 26.7 PSI; ACTCR= 200.0mm; RELCR= 200.0

SER 304; FIX 4; C= 0000000; BIN=GOOD; MRRU=44.3; MRRD=47.7; LEAK RATE= 1.9
ACT= 133.4; REL= 101.8; DIF= 31.6 PSI; ACTCR= 200.0mm; RELCR= 200.0

17-APR-1992 11:46:16.12 OPER DOOR DID NOT CLOSE 1

7798 PRESSURE TESTER LOT REPORT

RATING: 77PSL2-1

LOT ID: A-2107

LOT STARTED: 17-APR-1992 10:11:04.06

TIME PRINTED: 17-APR-1992 11:46:42.95

SETUP DATA:

DISC LOT ID: 0.00

DISC MEAN ACT: 23.4 MEAN REL: 12.7

LIMIT (NC)

ACTUATION: 90.0 TO 160.0 PSI

RELEASE: 20.0 TO 120.0 PSI

DIFFERENTIAL: 0.0 TO 160.0 PSI

MAX MILLIVOLT: 500.0 PSI

ACT CREEP TIME: 25.0 PSI

REL CREEP TIME: 150.0 PSI

PRECYCLE PRESS: 800.0 PSI

PRECYCLE COUNT: 2

NUMBER OF PIECES TESTED: 304

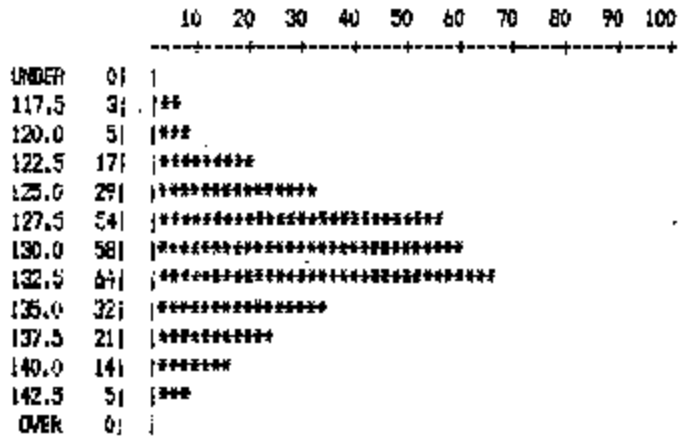
PERCENT OF PIECES GOOD: 100

TI-NHTSA 006031

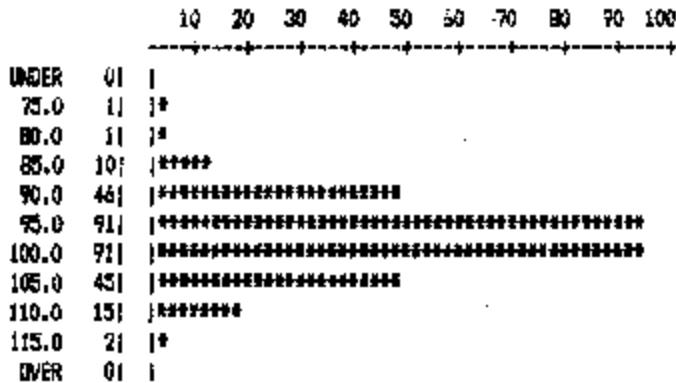
DEF	COUNT	% OF RECORDS
LEAK	0	0.00 %
CONT	2	100.00 %
ACCR	0	0.00 %
ACLD	0	0.00 %
ACHI	0	0.00 %
RLHI	0	0.00 %
RLLS	0	0.00 %
DFLO	0	0.00 %
RLEK	0	0.00 %
DFHI	0	0.00 %

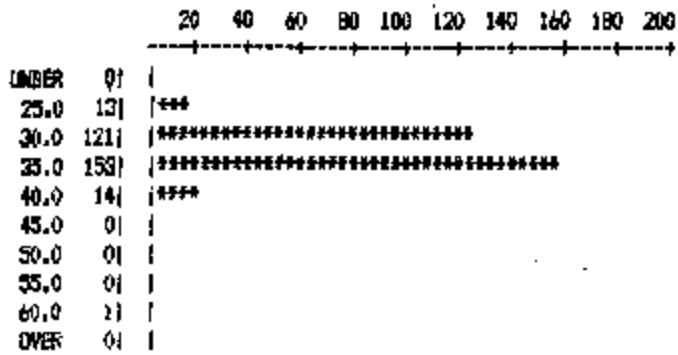
STATISTICS	MEAN	SIGMA	CPK
ACTUATION:	130.6	4.85	2.00
RELEASE:	97.7	5.36	1.25
MILLIVOLT:	0.0	0.00	0.00
DIFFERENTIAL:	32.9	3.19	3.44

HISTOGRAM OF ACTUATION PRESSURE

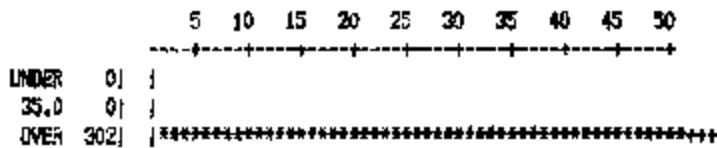


HISTOGRAM OF RELEASE PRESSURE

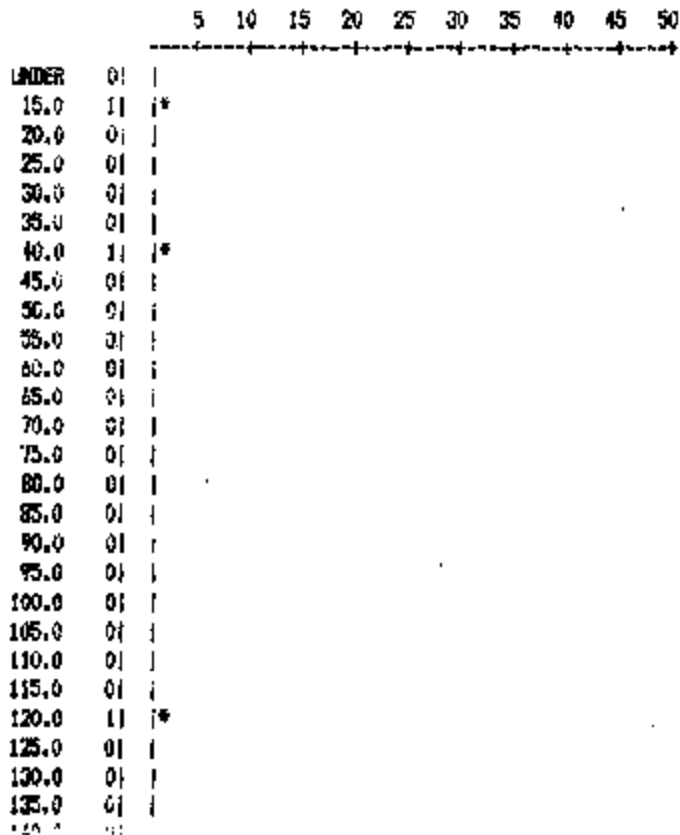




HISTOGRAM OF ACTUATION CREEP



HISTOGRAM OF RELEASE CREEP



150.0 01 |
160.0 01 |
165.0 01 |
170.0 01 |
175.0 01 |
180.0 01 |
185.0 01 |
OVER 2991 |*****

17-APR-1992 11:46:54.31 OPER DOOR DID NOT CLOSE 1

17-APR-1992 11:47:14.31 OPER DOOR STILL DID NOT CLOSE 1

17-APR-1992 11:47:30.04 TDA CYCLE TIMEOUT 1

TI-NHTSA 006034

Plans for Noise Control in Volume Production

(Please note that these plans are still under development and subject to change, pending receipt of the necessary transducer hardware, actual construction of test equipment, and performance of various comparative tests of switch designs previously confirmed by in-car tests to be "quiet" or "noisy".)

Bruce Maeroff, Supv. of Pass. Car Brake Systems Eng. Dept., has instructed TI to develop a method of testing pressure switch devices which will allow comparative measurement of the audible noise and tactile pedal feel phenomenon.

The system under development is composed of a Kistler high-resolution hydraulic pressure transducer with range 0-300 psi and resolution to .005 psi; a manifold to mount this transducer in close proximity to the device under test; a means of evacuating and filling the setup; and a means of applying a carefully controlled and reasonably noise-free pressure signal, using an air-over-oil intensifier unit fed by a feedback controlled air pressure regulator. Suitable isolation from the environment, possibly including shock mounting and/or acoustic protection, is to-be-determined.

Once suitable test equipment exists, the next phase is to characterize "known" devices including: normal snap-action; reduced snap devices found to be quiet in air but noisy in the actual application; and devices found suitable by Ford. This will allow establishment of control parameters. These parameters will be included in an addition to the ES, which will include PV, IP-1, and IP-2 tests.

Once the update to the ES is mutually agreed upon by Ford and TI, a partial ISR test will be conducted of this specific parameter; or, alternately, this will be included in the full ISR if time permits.

For the purpose of switch manufacturing process control, above studies will be correlated with disc (pressure-sensing element) characteristics which are controlled in the disc manufacturing process. The IP-2 testing for the noise parameter will be conducted on a quarterly basis per inputs from Bruce Maeroff.

As 9/24/72

TI-NHTSA 006035

Interim Containment Actions

Pressure and force vs. deflection characteristic curves are routinely plotted as a development tool for the pressure sensing elements. Generally speaking, these curves are indispensable for the information they provide, yet they are somewhat time- and labor-intensive, not easily automatable, and require interpretation.

The nature of the curves describing the parts which have been deemed acceptable for DH5 are well-known from testing during development.

In order to control the manufacturing process in the short-term, the above curves are re-run on every lot, under the direction of a TI Member of Technical Staff, and compared with the curves for the parts which are known to be acceptable.

To date, seven separate lots have been produced and tested as above with very good correlation and repeatability, indicating the disc manufacturing process is presently under control.

This interim process control strategy will remain in effect until such time as a more suitable strategy, using hydraulic-disturbance equipment which is under development, can be implemented; in conjunction with development and correlation of a simple static pressure-deflection check, which will obtain a few of the key points on the characteristic curve and can be used for manufacturing process control.

So 92022

TI-NHTSA 006036

FINAL INSPECTION 779211-1

DATE: 4-23-92

CUSTOMER P.O. #200-99024-88

TEST LOT 4-10

MATERIAL: 779211-1

REEL LOT

MATERIAL

REEL #1

CUP LOT # 11

REEL #

CUP LOT #

LOT # 2

CONNECT 150

LOT #

CONNECT LOT

WASHER LOT 140 1-CUT

QTY: 1000

WASHER LOT

QTY:

TEST	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
1A ACTUATION	146	137	139	134	132	140	137	142	135									
RELEASE	67	66	69	62	67	60	67	65	62									
2 VISUAL	OK	OK	OK	OK	OK	OK	OK	OK	OK									
3 DIMENSION						OK	OK	OK	OK									
4B VOLT DROP						OK	OK	OK	OK									
5C CUR. LEAK						OK	OK	OK	OK									
6D PROOF						OK	OK	OK	OK									
7 IMPULSE	OK	OK	OK	OK	OK													
A ACTUATION	140	130	140	146	140	140	140	145	135									
RELEASE	60	60	60	65	60	70	70	65	60									
B VOLT DROP	OK	OK	OK	OK	OK													
C CUR. LEAK	OK	OK	OK	OK	OK													
D PROOF	OK	OK	OK	OK	OK													
8J TERL. STR						OK	OK	OK	OK									
R ACTUATION						145	145	150	140									
RELEASE						70	70	65	65									
B VOLT DROP						OK	OK	OK	OK									
C CUR. LEAK						OK	OK	OK	OK									
D PROOF						OK	OK	OK	OK									
9 BURST						OK	OK	OK	OK									

TI-NHTSA 006037

FINISHED PRODUCTION

WHITE CANARY
PINK

Route to Finished Goods
Route to Dept. Supervisor

APPSL-2-1

SPECIAL REQUIREMENT
20

TOTAL QUANTITY
9

MAAL ORDER NUMBER

NO SUBTOTALS

Lot 4-10

QUALITY CONTROL APPROVAL

IN PROCESS	IN PROGRESS	FINAL
		NOTED BY ACCEPT APR 24 1982

Form 1800
DATE 4-22-82 DEPARTMENT 294

PRESSURE SWITCH DATA

FORM 21605

TEST NO. 438-01-60

DEVICE 77A5L3-1	DATE REQUESTED	REQUESTED BY	REQUESTED COMPL. DATE
PERFORMED BY LUTIS	DATE STARTED 4-26-77	DATE COMPLETED	APPROVED BY

PROJECT TITLE:

E199424

CUSTOMER:

PURPOSE OF TEST:

PROCEDURE:

ACT : 90-200 PSIG
REL : 20 PSIG MIN

SWITCH #	ACT	REL	DIF	ACT CR	REL CR	MVD
438-01-01	129.2	105.3	23.9	3234.2	1103.5	.54
02	131.9	93.4	38.5	3009.5	666.2	.42
03	128.6	85.8	42.8	3176.5	355.0	.44
04	129.1	82.3	46.8	3207.0	206.8	.44
05	125.5	78.8	46.7	3321.5	211.0	.45
06	128.2	86.3	41.9	3121.8	527.5	.39
07	132.3	89.9	42.4	2829.8	683.5	.48
08	123.9	80.7	43.2	3432.5	296.0	.46
09	125.7	90.8	44.9	2742.8	572.0	.49
10	128.9	88.8	40.1	3010.8	518.0	.57
11	124.6	89.9	34.7	3332.3	578.0	.47
12	125.6	81.5	44.1	3257.3	204.8	.48
13	127.4	86.6	40.8	3090.5	722.3	.40
14	127.2	84.2	43.0	3097.5	627.5	.44
15	119.4	75.0	44.4	3632.0	201.8	.41
16	124.1	78.2	45.9	3527.8	351.5	.42
17	114.4	76.4	38.0	3970.5	208.8	.41
18	122.5	78.6	44.0	3475.2	306.5	.40
19	124.6	80.6	44.0	2770.0	287.5	.44
20	128.3	81.5	46.8	3036.0	448.8	.42
21	126.5	80.7	45.8	3170.5	210.5	.42
22	125.9	91.6	44.3	2772.0	665.5	.41
23	130.0	85.1	44.9	2914.3	392.0	.42
24	125.0	81.8	43.2	3271.0	254.5	.46
25	132.6	91.8	40.8	2829.2	822.0	.46
26	121.0	82.4	38.6	3539.0	476.8	.40
27	126.5	77.2	49.3	3142.5	201.8	.43
28	117.2	81.4	35.8	3796.0	402.0	.42

TI-NHTSA 006039

SWITCH #	ACT	REL	DIF	ACT CR	REL CR	MVD
29	122.4	77.3	45.1	3078.0	208.3	.47
30	135.0	89.7	45.3	2773.0	748.0	.48
31	123.1	78.7	44.4	3242.8	275.5	.42
32	125.1	83.7	41.3	3194.0	500.0	.43
33	129.4	83.9	45.6	3125.8	218.3	.47
34	134.3	85.2	49.1	2702.3	1729.3	.48
35	125.2	77.9	47.3	3220.5	1407.3	.49
36	128.7	93.8	34.9	2976.0	2073.5	.45
37	124.9	81.9	43.1	3237.0	273.3	.45
38	124.6	80.3	44.3	3272.0	287.0	.39
39	133.4	94.7	38.7	2840.8	811.0	.42
40	133.0	92.7	40.3	2802.8	730.8	.45
41	123.0	84.9	38.1	3481.0	375.5	.54
42	133.0	90.9	42.1	2813.8	619.8	.42
43	134.4	89.4	45.1	2778.5	558.5	.42
44	124.8	81.2	43.6	3286.8	202.8	.42
45	118.3	84.5	33.8	3747.0	554.3	.47
46	125.3	81.1	44.2	3260.5	409.0	.43
47	121.2	79.9	41.3	3557.3	359.3	.46
48	116.6	76.6	40.0	3875.8	283.8	.52
49	127.7	88.8	38.8	3122.5	492.8	.49
50	126.2	85.4	40.8	3224.0	349.5	.47
51	128.9	82.0	46.9	3019.0	207.3	.47
52	132.1	96.7	35.3	2838.3	809.5	.40
53	122.5	75.9	46.8	3424.0	209.8	.46
54	132.8	90.3	39.5	2822.0	944.3	.44
55	124.3	83.0	41.4	3299.8	520.8	.50
56	124.5	86.4	38.1	3304.3	661.8	.48
57	123.2	83.5	39.7	3403.3	210.0	.51
58	129.6	84.4	45.2	2923.5	249.3	.46
59	131.2	87.5	43.7	2860.5	372.3	.44
60	128.8	88.2	40.6	2985.0	404.0	.39

TI-NHTSA 006040

-MSG M#- 115981 FR=QCBJ TO=PCQA SENT=04/27/92 09:33 AM
R#-217 ST=C DIV=0050 CC=00666 BY=QCBJ AT=04/27/92 09:33 AM

To: Jim Watt PCQA Elaine Rose PCQA
Copy: Norm Roy NLDG Bill Sweet PCME
Bill Archibald AFCQ Matt Sellers PCME
Jim Kern KERN Steve Offiler SBO1

From: James Frericha JPF

Subj: 46412 Dimensions MSG #32290.

Date: 04-27-92.

The two dimensions referenced in your message were measured on two different historical samples of the 46412-2.

1. Dimension 0.461/0.465

Historical data taken 1-4-89 to Rev R.

Cav P	Cav U	Cav V	Cav X
.4665	.4688	.4683	.4681

From production runs on 3-6-92 and 3-26-92 on the 46412-2.

Cav P	Cav Z	Cav O	Cav Blank
.4682	.4683	.4682	.4679
.4682	.4684	.4672	.4685

(Tool makers microscope looking down into part)

This dimension is controlled by the stack up of the terminal slots and their separation. The spec. for the T/S is 0.180/0.184 2x and web 0.096/0.103. Adding these up the tolerance would be 0.456/0.471. Changing the steel for 0.461/0.465 would also change the T/S and web.

2. Dimension 0.531/0.543

Historical data taken 1-4-89 to Rev R.

Cav P	Cav U	Cav V	Cav X
.5276	.5302	.5282	.5258

From production runs on 3-6-92 and 3-26-92 on the 46412-2.

Cav P	Cav Z	Cav O	Cav Blank
.5294	.5272	.5255	.5331
.5329	.5259	.5270	.5271

(Tool makers microscope to the ends of the radii)

Steel could be modified to increase this.

Regards,

James x-3078

TI-NHTSA 006041

-MSG N#- 115981 FR-QCBI TO-PCQA SENT-04/27/92 09:33 AM
R#-218 ST-C DIV-0050 CC-00666 BY-QCBI AT-04/27/92 09:33 AM

To: Jim Watt PCQA Elaine Rose PCQA
Copy: Norm Roy MLDG Bill Sweet PCME
Bill Archibald AFCQ Matt Sellers PCME
Jim Kern KERN Steve Offiler SBO1
From: James Frerichs JPF
Subj: 46412 Dimensions MSG #32290.
Date: 04-27-92.

with data ship

The two dimensions referenced in your message were measured on two different historical samples of the 46412-2.

1. Dimension 0.461/0.465

Historical data taken 1-4-89 to Rev R.

Cav P	Cav U	Cav V	Cav X
.4665	.4688	.4683	.4681

From production runs on 3-6-92 and 3-26-92 on the 46412-2.

Cav P	Cav Z	Cav O	Cav Blank
.4682	.4683	.4682	.4678
.4682	.4684	.4672	.4685

(Tool makers microscope looking down into part)

This dimension is controlled by the stack up of the terminal slots and their separation. The spec. for the T/S is 0.180/0.184 2x and web 0.096/0.103. Adding these up the tolerance would be 0.456/0.471. Changing the steel for 0.461/0.465 would also change the T/S and web.

2. Dimension 0.531/0.543

Historical data taken 1-4-89 to Rev R.

Cav P	Cav U	Cav V	Cav X
.5276	.5302	.5282	.5258

From production runs on 3-6-92 and 3-26-92 on the 46412-2.

Cav P	Cav Z	Cav O	Cav Blank
.5294	.5272	.5255	.5331
.5329	.5359	.5270	.5271

(Tool makers microscope to the ends of the radii)

Steel could be modified to increase this.

Regards,

James x-3078

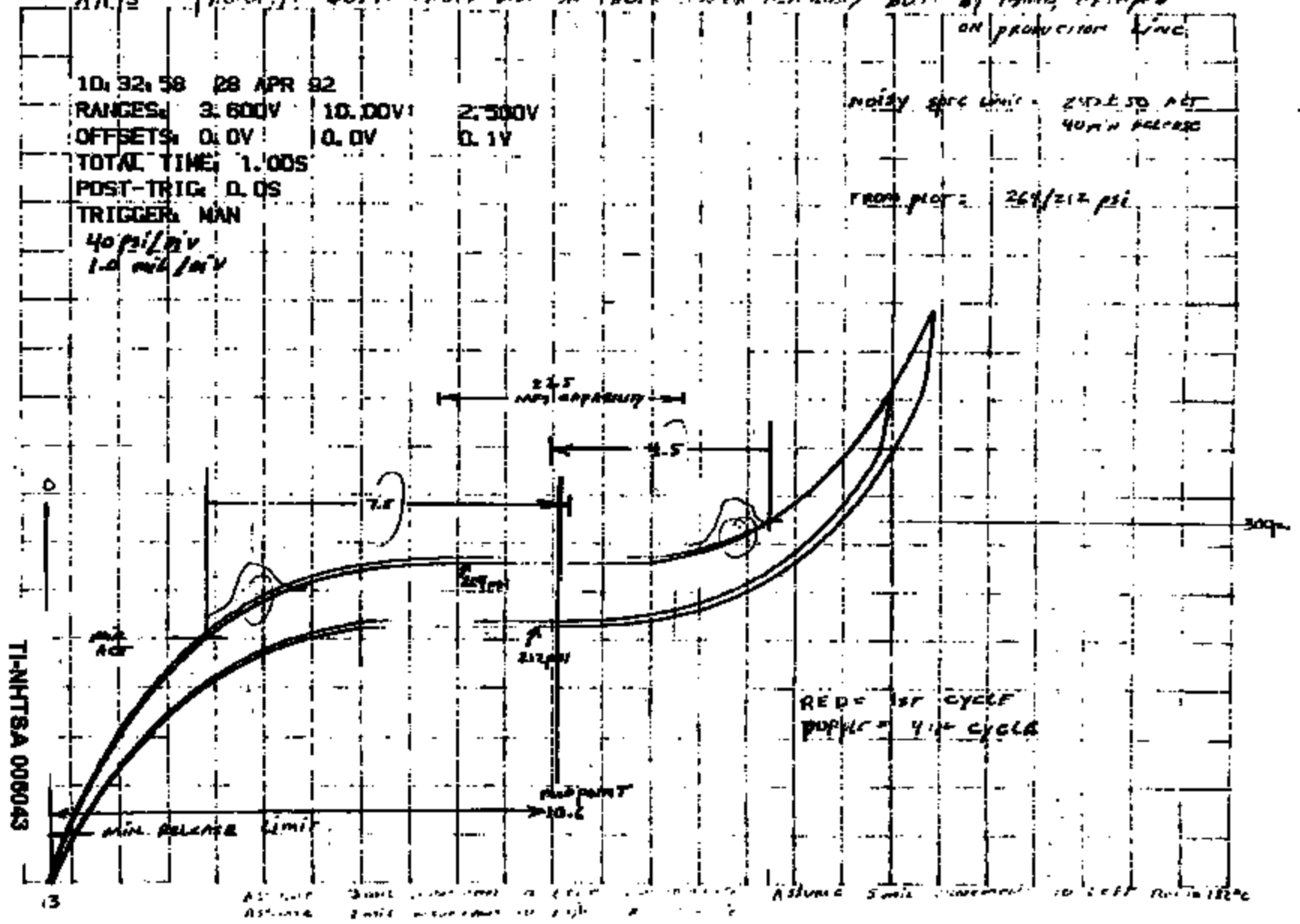
TI-NHTSA 006042

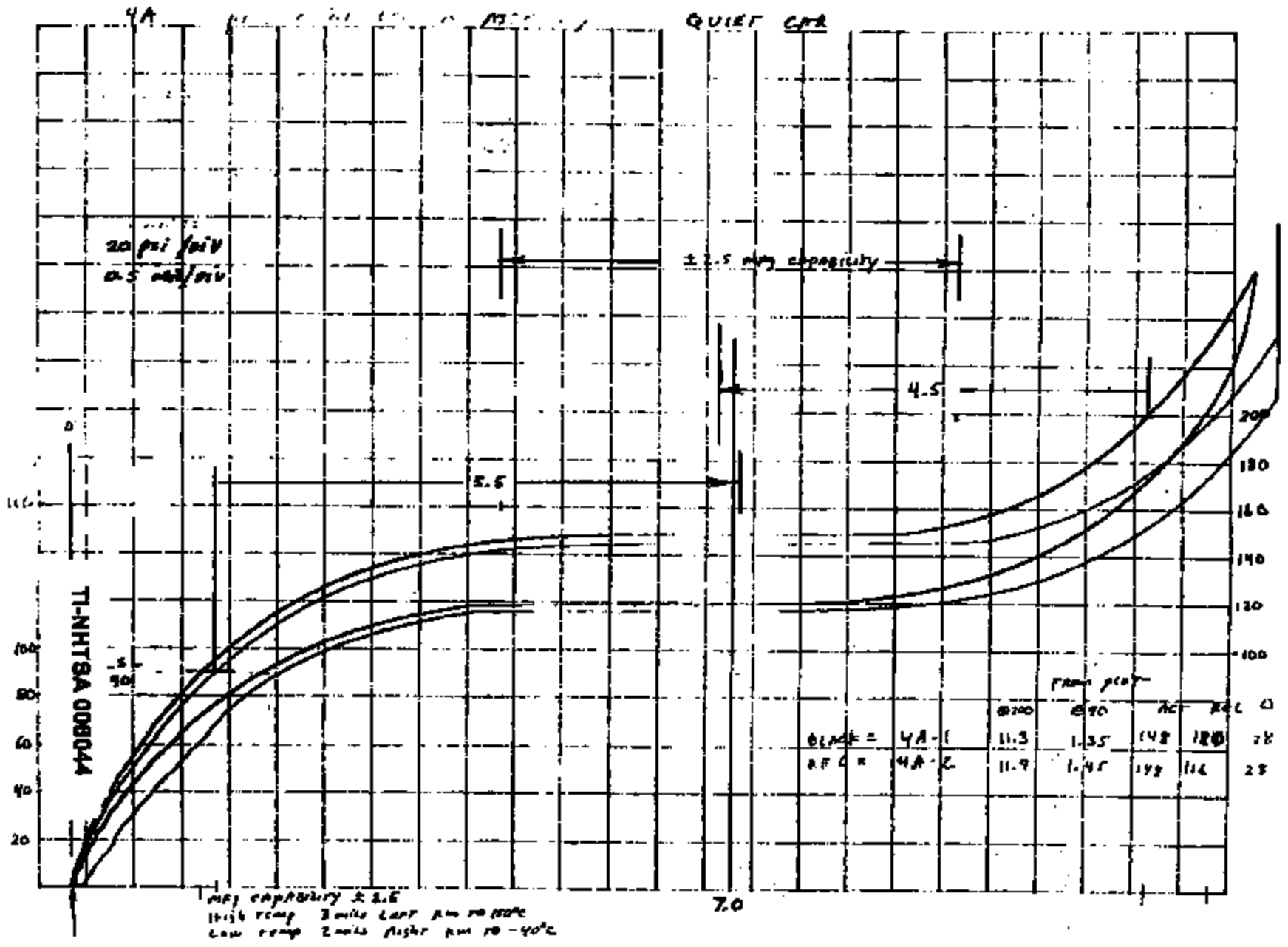
"AAJ3"

10.00V/100ns. QUOTE: CHECK PRESS IN TRUCK UNDER REPAIRS/ BUT BY HAND, CLIMBED ON PRODUCTION LINE

10:32:58 28 APR 92
 RANGES: 3.600V 10.00V 2.500V
 OFFSETS: 0.0V 0.0V 0.1V
 TOTAL TIME: 1.00S
 POST-TRIG: 0.0S
 TRIGGER: MAN
 40psi/div
 1.0 mil/div

noisy spec limit = 250 ± 50 psi
 40psi/div
 room floor = 269/212 psi





-MSG #=- 212787 FR-ZARN TO-GAMY SENT=04/29/92 04:22 PM
R#-180 ST=C DIV=0050 CC=00101 BY-ZARN AT=04/29/92 04:22 PM

TO: RUSTY STRUBLE RCS2
MIKE DeMATTIA MD3
CHARLIE DOUGLAS CNP1
DICK GARIOPY NFPC
PAUL KOTCH PRK1
JOE LAZARE JNLS
STEVE OFFILER SBO1
MATT SELLERS PCNE
BILL SWEET PCNE
JIM WATT PCQA

CC: TOM CHARBONEAU TC
JOHN KOURTESIS NDES
STEVE MAJOR SMFH
ANDY McGUIRK PCQA
ED O'NEILL EJON
NORM FREDA WHEE
GARY SNYDER CPPC
MARTHA SULLIVAN CPPC
RAY TOURANGEAU PCNE
BILL CONGDON NFPC
STEVE MCCOZEY NDES
ELAINE ROSE GAMY

FR: DAVE CZARN ZARN

SJ: FORD CRUISE CONTROL PRESSURE SWITCH START-UP MEETING
MINUTES OF 3/26/92 MEETING

THE FOLLOWING IS A RESEND OF THE LAST MEETING MINUTES - PRIOR TO THE DAILY CCPS QUIET SWITCH MEETINGS. I WOULD LIKE THE TEAM TO REVIEW THESE AFTER/DURING THE QUIET SWITCH MEETING ON 4/30. I WILL BE UNABLE TO ATTEND THE MEETING AND WILL ASK CHARLIE - BY WAY OF THIS MESSAGE - TO RUN THE MEETING. THANK YOU.

MEETING

THE NEXT MEETING IS SCHEDULED FOR:

DATE: 04/30/92 (THURSDAY)
TIME: 3:30 PM
PLACE: CAFET. CUBE

77PS

Hexport:

Elco is still 100% sorting hexports for slivers/stringers. Elco c/a indicates that Elco and TI will evaluate a modification to the length and diameter of the bore closest to the internal gland side of the hexport. We don't know what Elco is doing at the moment; Paul, please champion the effort to get this resolved.

* REPORT ON ELCO'S PROGRESS IN RESOLVING KOTCH ONGOING
SLIVER/STRINGER ISSUE
. HAVE ELCO RETURN J512 GAGE FOR STUDY KOTCH T-B-D
. ELCO J512 GAGE R&R STUDY SELLERS T-B-D
* ADD SLIVER/STRINGER INSPECTION TO IQP ROSE 03/19 COMP.
FOR P/N 36900

Production/Quality Issues:

DIAPHRAGM LIFE

HIGH TEMP LOSS OF CONTINUITY

(Separate mtgs are being held daily)

* LOCK OUT "CREEP CHK DISABLE" FUNCTION SELLERS 03/26 ORIG.
FROM P-TESTER? 04/02 REV.

TI-NHTSA 006045

RMR's

4 L/T switches returned; system reportedly inoperable - "no continuity" is probable cause. It's possible (...and maybe even probable) that the switches were not at fault. However, I still believe this is not an issue that we should let drop, as it may indicate a switch, system, or Ford assembly problem. Jim agreed to pursue further.

- * F/U WITH THE APPROPRIATE INDIVIDUAL TO DETERMINE IF THESE SWITCHES FUNCTION CORRECTLY IN THE SYSTEM. FREDA 03/26 no conclusions

EASTERN AUTOMATION RIVETING OPERATION

(Mid-May targeted for changeover to new rivet operation)

- . PROVIDE D. CZARN W/NEW RIVETS SELLERS 03/19 COMP.
- . SEND TO FORD/GET SREA APPROVAL OFFILER 03/26 COMP.
- * F/U WITH PEASE AND PELKEY RE: RIVET SREA SIGN-OFF FREDA 04/02

FLAKING/CLEANLINESS

Jim proposed an alternate approach to maintaining tote cleanliness whereby a recyclable liner is used in the totes for a T-B-D period of time and parts are transferred between totes by hand (rather than "dumping" from one tote to another). Pilot run will be conducted next week.

Matt's received a proposal for vacuuming sensors and final switches after crimping, to remove metal flakes and other particulate. Cost is \$5k/station x 2 stations.

- . LONG TERM C/A SELLERS/ ONGOING
- . ADD PM'S TO QC INSPECTION - ALL 77PS WATT
- OP'S PLUS 52PS SENSOR ASM. WATT/ 03/19 COMP.

DANA PRESSURE TEST CORRELATION

- * CALL DANA TO REQUEST THAT CAL'M DATA BE PROVIDED FOR 42 SWITCHES; DISCUSS SPECIFICS OF TEST PROCEDURE WATT 03/13 COMP.
- * PROVIDE TEST PLAN TO BRUCE PEASE OFFILER 03/13 COMP.
- * COMPLETE TESTING AND REPORT TO BRUCE OFFILER/ 04/16

Sensor Assembly Machine:

- . PRIORITIZE REMAINING UPGRADE ITEMS SELLERS ONGOING

Base Assembly Machine:

Ultrasonic welder is in-house until 4/03. Evaluation plan needs to be defined ASAP.

- * DEFINE PLAN FOR EVALUATING U-S WELDER SELLERS/ 03/27
- OFFILER/
- * BUILD PARTS MCCOY 04/03

Final Assembly Machine:

ISR:

Issues: Taves pkg. not approved because SPC data is needed onthread Pd and J51

2 chamfer OD (SC's on print). The latter is not measure directly; rather, the J512 gage procedure is used which measures a dimension that defines the angle and chamfer depth. Jim will propose to Teves that this not be defined as a Significant Characteristic.

* GET HEXPORT CONTROL PLAN FROM MATT AND REVW TO SEE IF SPC DATA IS COLLECTED	WATT	03/16	COMP.
* UNDERSTAND REASON FOR TEVES' REQUEST AND RESPOND	WATT	03/20	COMP.
* PROPOSE ELIMINATION OF CHAMFER OD AS A SIGNIF. CHARACTERISTIC (TEVES)	WATT	04/02	
. PROVIDE QUARTERLY Cpk REPORT	WATT	start 03/31	
* SUBMIT DANA/PITTS PKGS	WATT	01/23	ORIG.
		04/02	REV.

Ultra-Low Differential Switch NY93

Dale Hodge will champion ultra-low differential switch efforts; items will be covered at separate meetings.

Miscellaneous:

* BUILD 35 L/T SWITCHES WITH 3A GAGED 10B21 HEXPORTS TO BE SUPPLIED BY ELAINE	ROSE/ RODRIGUEZ	03/19	COMP.
* DISCUSS IDEA OF POSTING PFMEA'S AT PROD'N OPERATIONS W/ TEVES; GET SAMPLE (discussed; will send sample)	WATT	03/26	ORIG.
* HOW DO WE PREPARE FOR A CLEANLINESS AUDIT FROM TEVES?	WATT	04/02	REV.
(Audit would look at cleanliness of switch only; i.e., not audit of production line cleanliness. No audit planned.)			
* TEVES CRITERIA FOR CONTAMINATION	WATT	03/26	
* RE-USABLE PACKAGING FROM TEVES?	WATT	04/09	

Production Plan:

. MAINTAIN RUNNING TOTAL OF L/T (L2-3) SWITCHES LEADING TO 100K FOR AMORTISATION	STRUBLE	ONGOING
Status Date Total Shipped		
Rusty, need update.....		
. UPDATE PRODUCTION PLANS	STRUBLE	ONGOING

	P/C	L/T
	77PSL2-1	77PSL2-3
	-----	-----
MAR	64.7	22.6

REGARDS,
DAVE CZARN \55-FORD

#27639



TOLLWAY STEEL CORPORATION
25th Ave. & Main St.
Melrose Park, IL 60160
Phone (708) 681-3190

Customer DIEMASTERS MFG.

ANALYSIS REPORT

ITEM #	ORDER #	PART #	SIZE	GRADE	TEMPER
1.	033632	CROSSAD 1375C	.0985 x 1.375 x cl	C1050	ANNLD
2.					
3.					

QUALITY CONTROL
APR 30 1976

ITEM #	ID#	C	Mn	P	S	SI	NI	Cr	Al
1.	664332	.51	.69	.013	.002	.27			
2.									
3.									

ITEM #	ROCKWELL	TENSILE	YIELD	ELONGATION	OTHER
1.	RB 78				
2.					
3.					

CERTIFIED BY: Thomas Bulman
THOMAS BULMAN

TEXAS INSTR
27639-1

3/76

TI-NHTSA 008048

PROPOSED SPEC FOR QUIET DISC 36656-35

VALUES ARE FOR DISC AFTER FINAL HEAT TREATMENT

MATERIAL PART # 75525-2
BLANK STRIP # 74371-2

- A ACTUATION MEAN : AS REQUIRED BY MFG ENGINEERING
(NOMINAL TARGET : 22 psi)
- B ACT MEAN TOLERANCE : ± 1.0 psi
- C ACT SIGMA MAX : 1.0^5 psi
- D MAXIMUM MEAN DIFFERENTIAL : 5.5 psi
- E DIFFERENTIAL SIGMA MAX : 1.0 psi
- F MINIMUM MEAN TRAVEL TO
14 psi ON ACTUATION : 0.0035 inches
- G MAX SIGMA, TRAVEL TO
14 psi ON ACTUATION : TO BE DETERMINED
- H MINIMUM MEAN TRAVEL TO
32 psi ON ACTUATION : 0.0240 inches
- I MAXIMUM SIGMA, TRAVEL TO
32 psi ON ACTUATION : TO BE DETERMINED
- MINIMUM $\Delta H-F$ = 0.0125 inches

PRESSURE CALIBRATION

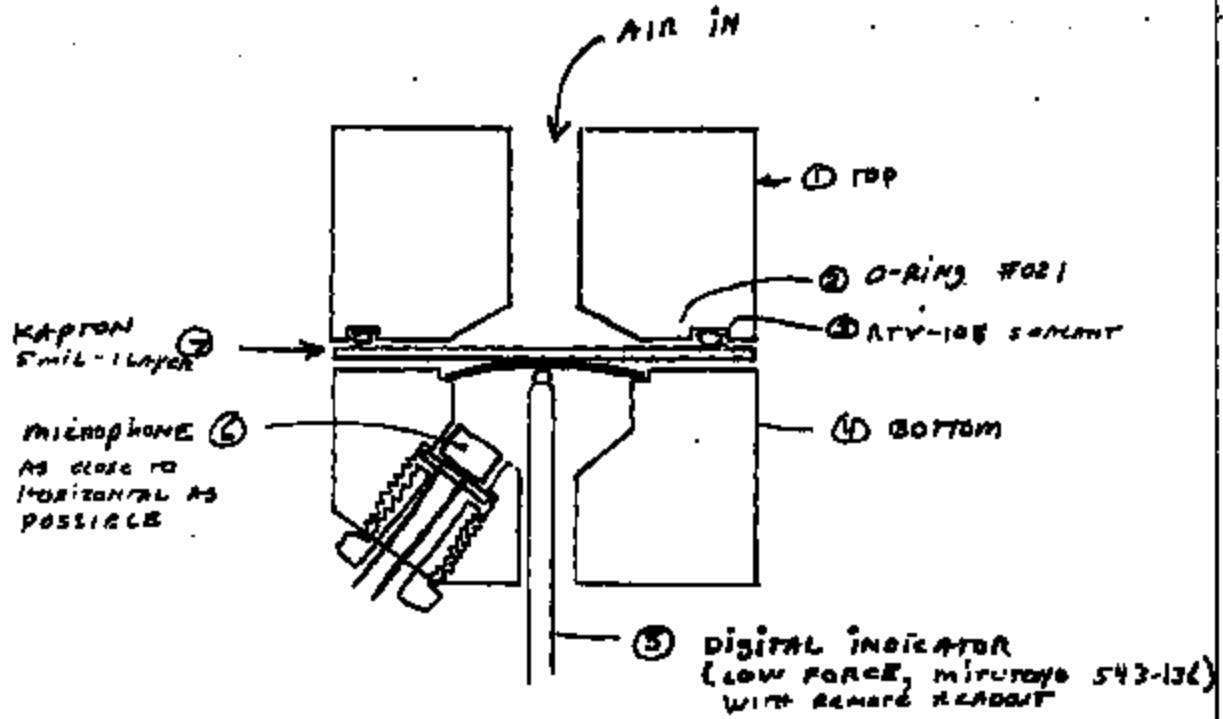
1) METHOD

MEASUREMENT TO BE TAKEN IN A STANDARD FIXTURE
PRINT # XXX, USING THE FOLLOWING MEASUREMENT
PROCEDURE;

- A. CYCLE DISC THREE TIMES ACTUATION TO RELEASE
- B. FROM RELEASE INCREASE PRESSURE TO 14 psi \pm 0.5 psi
AND RECORD DISC TRAVEL.
- C. CONTINUE PRESSURE INCREASE UNTIL ACTUATION.
RECORD ACTUATION PRESSURE.
- D. INCREASE PRESSURE TO 32 psi \pm 0.5 psi AND
RECORD DISC TRAVEL.

E. DECREASE PRESSURE TO RELEASE AND RECORD
RELEASE PRESSURE

ALL RAMP RATES SHALL BE LESS THAN 0.5 PSI/SEC.

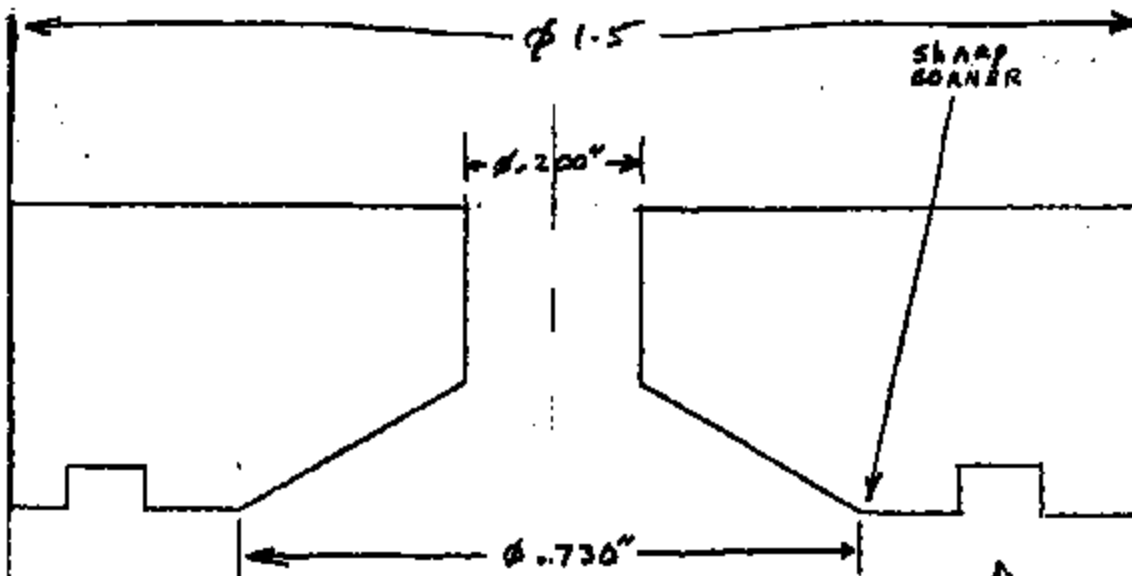


DATE: 12-20-92 BY: GLENN S. BROWN

TOP

DATE 3006

4-30-92

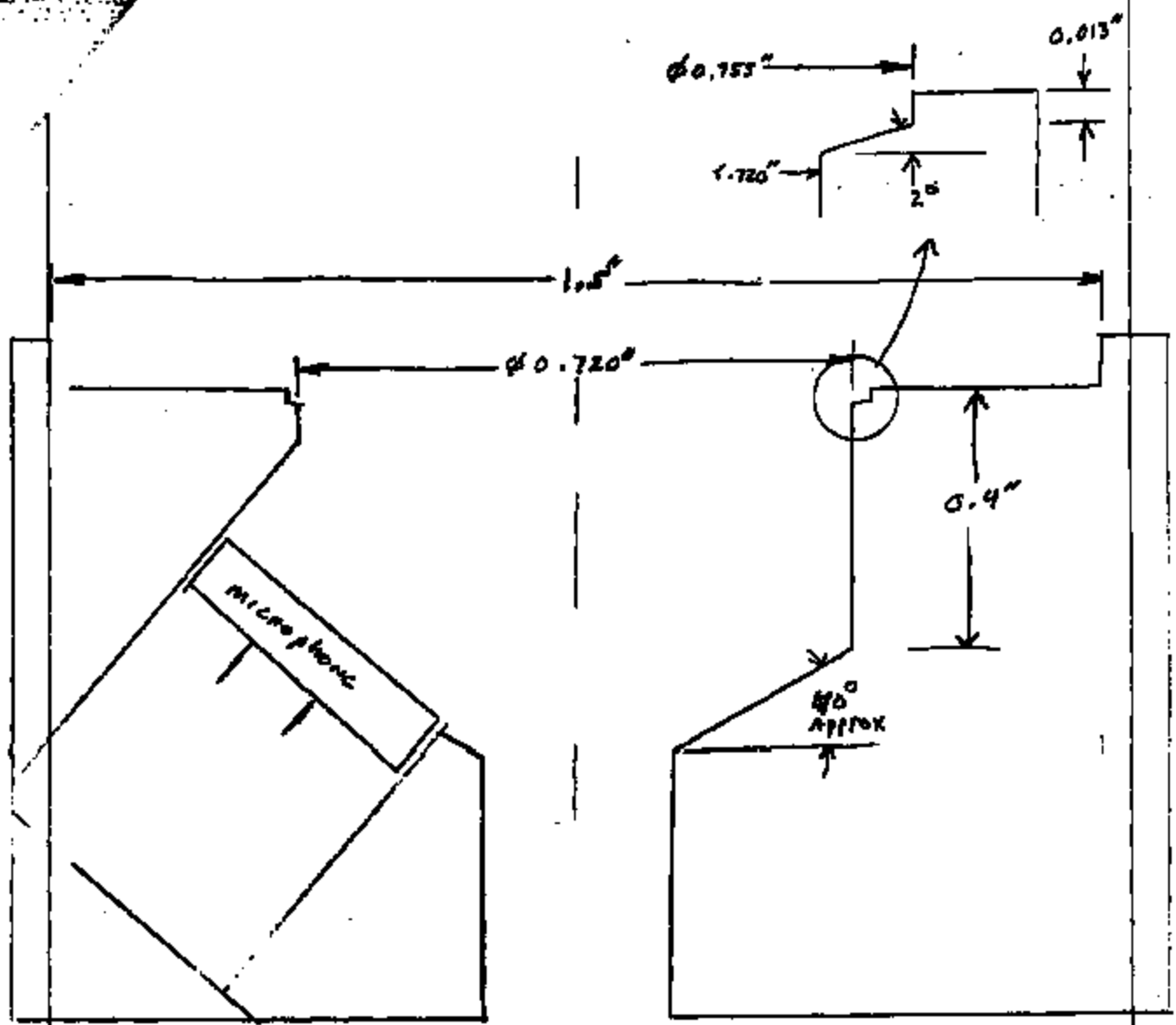


↑
LAND FOR
O-RING
↓
RTV-108

BOTTOM

DRAWN BY: 11-20-92

SCALE: 1/2" = 1" AND 1/8" = 1/4" DIA.



IN NEEDED FOR DIAL INDICATOR
APPROX .250"